

Appendix C Geomorphology Target Notes



Target Note	Ordnance Survey Grid Reference	Description	Photographs
001	254597, 610035	Looking generally west from the proposed site entrance to Peat Hill.	
002	254687, 610210	Looking generally west along the northern slope of Peat Hill. Note the dominance of grasses and grazing pasture.	
003	254789, 609760	Looking generally north along the western slope of Peat Hill across BP-A and towards the proposed route of the access track.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
004	254937, 609759	Looking generally northwest along the northern slope of Peat Hill within BP-A at an exposure of igneous bedrock. Note the mineral grasses and grazing pasture.	
005	255086, 609758	Looking generally northwest to Peat Hill across BP-A and across the proposed access route of the hill.	
006	255239, 609959	Looking generally north from Peat Hill to the B741. Note the mineral grasses indicating the absence of significant depths of peat.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
007	255189, 609708	Looking generally west from adjacent to the access track.	
008	255489, 609660	Looking generally south towards Barbeys Hill and across Blood Moss and the proposed locations of the temporary compound and the substation.	
009	255383, 609426	Looking generally north towards Peat Hill across a flush in the foreground.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
010	255090, 609307	Looking generally north towards the proposed location of T16.	
011	255429, 609224	Looking generally southeast towards Chang Hill and Benty Cowan Hill from the access track. Note the steep valley in the distance.	
012	255434, 609020	Looking generally east towards Rigg Hill from the temporary construction compound.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
013	255467, 609045	Looking north to Peat Hill across Blood Moss showing a potential peat pipe in the foreground, denoted by a line of rushes.	
014	255490, 609011	Looking generally south from the temporary construction compound towards Enoch Hill (right summit), High Chang Hill (left of Enoch Hill) and Barbeys Hill (in foreground).	
015	255419, 608896	Looking generally southeast from the temporary construction compound towards Chang Hill showing the steep sided valleys of Catlock Burn (left) and Littlechange Burn (right).	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
016	255385, 608804	Looking generally northeast over the proposed location of the temporary construction compound and substation towards Peat Hill (left summit).	
017	256096, 608694	Looking southeast from Rigg Hill down in to the steep sided valley of the Crocradie Burn and the confluence with the Catlock Burn (right).	
018	255690, 608502	A peat substrate exposure along near the banks of the Knockburnie Burn. Note the thin organic soils overlying Glacial Till, denoted by the red line.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
019	255450, 608333	Looking north over a flush adjacent to the Knockburnie Burn.	
020	255187, 608205	Looking north across the proposed location of T16 towards Barbeys Hill (foreground) and Enoch Hill in the distance.	
021	256291, 608508	An example of a recent translational failure of the mineral soils along the steep sided valley of the Catlock Burn.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
022	256085, 608436	Looking downslope from the head of a translational failure on the steep north facing slope of Littlechang Hill.	
023	256092, 608405	Looking generally northeast along the steep sided valley of the Crocradie Burn. Note the numerous translational failures along the valley.	
024	255944, 608345	Looking in a downstream direction along the Littlechang Burn. Note the steepness of the streams gradient and further evidence of translational failures.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
025	255991, 608297	Evidence of translational failure along the valley of the Littlechang Burn.	
026	255991, 608302	Bedrock exposures along the steep sided valley of the Littlechang Burn.	
027	255990, 608203	Exposed superficial deposits along the Littlechang Burn. Note the granular nature of the soils which include course gravels, cobbles and boulders.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
028	255947, 608161	Looking generally southeast at a potential peat pipe and pipe collapses extending upslope to the northeast of T2.	
029	255910, 608045	Looking generally north- northwest towards Rigg Hill from T2.	
030	255667, 608060	Looking generally west towards Carsphairn Forest and Lethans Hill to the west of the site. In the foreground is an example of one of the many drainage ditches.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
031	255788, 607806	An example of the peat profile taken on the northern slope of Barbeys Hill. Note the low water content and the relatively high fibrosity of the sample and the present of sandy clayey substrate at the base of the sample (right).	
032	255847, 607290	Looking generally northeast across Barbeys Hill and the route of the access track to T17 which avoids the hagging in the distance.	
033	256090, 606698	Looking generally north from Enoch Hill along the western site boundary.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
034	256405, 606162	Potential evidence of tension cracking and slope creep of the peat around the location of T19.	
035	256291, 607210	Looking generally south towards High Chang Hill. Note the exposure in the foreground which indicates granular soils.	
036	256484, 606900	Looking generally southeast across the source of Bitch Burn with evidence of hagging and flushes.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
037	256685, 606866	Looking generally southwest towards an area of hagging (in the distance) to the northeast of T7 which is over the horizon.	
038	256687, 606802	A closer example of the haggs shown in target note 037.	
039	256784, 606682	A peat exposure at a hagg to the northeast of T7. Note the granular nature of the peat substrate.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
040	256575, 606536	Looking generally southeast across a flush adjacent to the micrositing allowance for T17.	
041	256885, 608904	Looking generally north towards Dalleagles from the northern slope of Chang Hill.	
042	256787, 608403	Looking across Chang Hill towards Benty Cowan Hill and the location of T14.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
043	256687, 608003	An example of the shallow soil profile on Chang Hill comprising an organic horizon of <0.5m depth over gleyed sandy clay.	
044	257487, 608606	Looking generally northwest towards High Chang Hill across Trough Burn.	
045	255395, 607909	A potential peat pipe collapse to the south of BP-C.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
046	257661, 607965	A pond formed in shallow peat in the col between Benty Cowan Hill and High Chang Hill located adjacent to the proposed track to T18.	
047	257364, 607808	Looking generally northwest along the route of the tracks to T14 and T18.	
048	257266, 607283	Peat pipe collapses to the north of T10 near the source of the Polga Burn. Collapses are present in front and behind of the person.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
049	257225, 607280	A peat pipe collapse on the Polga Burn. The form of the collapse may indicate that surface water may surcharge into the collapse during heavy rainfall causing scour when flows subside.	
050	257386, 606706	Looking northeast along the Connel Burn from adjacent to T12.	
051	257409, 606692	Evidence of gully formation in the mineral soils to the north of T12.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
052	257849, 607542	Looking across the micrositing allowance for T15 up towards High Change Hill.	
053	258685, 609008	Looking generally northeast across the source of the Blarene Burn. Note the dominance of mineral soils in this area.	
054	259007, 608401	Looking along the steep sided valley of the Connel Burn.	

Target Note	Ordnance Survey Grid Reference	Description	Photographs
055	256108, 607908	Looking southwest towards Barbeys Hill over an area of hagging near T17.	
056	255786, 608211	Looking northeast along the valley of the Crocradie Burn with Rigg Hill to the left and Chang Hill on the right.	
057	257512, 608112	An example of a moss filled grip within the micrositing allowance of T14.	



Target Note	Ordnance Survey Grid Reference	Description	Photographs
058	256128, 606922	A peat slump on the northern slope of Enoch Hill to the northeast of T4.	



Appendix 6.C Carbon Balance – Average Peat Depth Calculations Spreadsheet



3,013

TOTAL (m3) Average 0.34

. <mark>(m3)</mark> 0.92

TOTAL

		New Ac	cess Traci	6.15km	n but less tha		
	d	Peat lepths	Tarat	0	T	-	
Volume m3	ati	along rack (m)	Track length (m)	Cumulative Count	Track width (m)	Excavated area (m2)	Volumes
1,814 378	-	0.5 0.5	50 50	50 100	6 6	300 300	150 150
869 643	_	0.5	50 50	150 200	6	300 300	150 150
1,890 378	-	0.5	50 50	250 300	6	300 300	150 150
529 378	-	0.5	50 50	350 400	6	300 300	150 150
756 869	-	0.5	50 50	450 500	6	300 300	150 150
832	_	0.5	50	550	6	300	150
1,814 1,134	_	0.5	50 50	600 650	6	300 300	150 150
12,285	_	0.5 0.5	50 50	700 750	6	300 300	150 150
	-	0.5	50 50	800 850	6	300 300	150 150
Volume	- 1	0.52	50	900	6	300	156
m3 1,625		0.52	50 50	950 1000	6	300 300	156 162
750 750		0.54 0.54	50 50	1050 1100	6	300 300	162 162
625 1.250		0.56	50 50	1150 1200	6	300 300	168 171
938		0.58	50	1250	6	300 300	174
625		0.6	50	1350	6	300	180
625		0.6	50	1400	6	300	180
1,063 2,875	-	0.6 0.6	50 50	1450 1500	6 6	300 300	180 180
1,688	-	0.6 0.6	50 50	1550 1600	6 6	300 300	180 180
13,813	-	0.6 0.6	50 50	1650 1700	6 6	300 300	180 180
	-	0.6 0.6	50 50	1750 1800	6	300 300	180 180
	-	0.6 0.6	50 50	1850 1900	6	300 300	180 180
	-	0.6 0.6	50 50	1950 2000	6	300 300	180 180
	-	0.6	50 50	2050 2100	6	300 300	180 180
	-	0.61	50 50	2150 2200	6	300 300	183
	-	0.61	50 50	2250 2300	6	300 300	183 186
	-	0.64	50 50	2350 2400	6	300	192 192
	_	0.64	50	2400 2450 2500	6	300	192
	_	0.65	50 50 50	2500 2550 2600	6	300	192 195 195
	_	0.65	50	2650	6	300	195
	_	0.65	50 50	2700 2750	6	300 300	195 198
	-	0.66	50 50	2800 2850	6 6	300 300	198 207
	_	0.69	50 50	2900 2950	6	300 300	207 207
	-	0.7	50 50	3000 3050	6 6	300 300	210 210
	_	0.7	50 50	3100 3150	6	300 300	210 210
	_	0.7 0.7	50 50	3200 3250	6	300 300	210 210
	-	0.7	50 50	3300 3350	6 6	300 300	210 210
	-	0.7	50 50	3400 3450	6	300 300	210 213
	-	0.71	50 50	3500 3550	6	300 300	213 225
	-	0.75	50 50	3600 3650	6	300 300	225 231
	-	0.79	50 50	3700 3750	6	300 300	237 240
	-	0.8	50 50	3800 3850	6	300 300	240 240
	-	0.8	50 50	3900 3950	6	300 300	240 246
	-	0.82	50 50	4000 4050	6	300 300	246 246
	-	0.82	50 50	4100 4150	6	300 300	246 246
	-	0.83	50 50	4200 4250	6	300 300	249 252
	-	0.84 0.85	50 50	4300 4350	6	300 300	252 255
	-	0.85 0.85	50 50	4400 4450	6	300 300	255 255
	-	0.85	50 50	4500 4550	6	300 300	255 255
	-	0.86 0.86	50 50	4600 4650	6	300 300	258 258
	-	0.86	50 50	4700 4750	6	300 300	258 258
	-	0.86 0.87	50 50	4800 4850	6	300 300	258 261
	-	0.87 0.88	50 50	4900 4950	6	300 300	261 264
	-	0.9 0.9	50 50	5000 5050	6	300 300	270 270
	-	0.9 0.9	50 50	5100 5150	6	300 300	270 270
	-	0.9	50 50	5200 5250	6	300 300	270 270
	-	0.9	50 50	5300 5350	6	300 300	270
	-	0.9	50 50	5400 5450	6	300 300	270
	-	0.9	50 50	5500	6	300 300	270 270
	-	0.9	50	5600 5650	6	300 300 300	270 270 270
	-	0.9	50	5700	6	300	270 270 270
	-	0.9	50 50 50	5750 5800 5850	6	300 300 300	270 270 273
	-	0.91	50 50 50	5900 5950	6	300	273 276 276
	-	0.92 0.93 0.94	50 50 50	6000	6	300 300 300	276 279 282
	-	0.94	50	6050 6100	6	300	282
	Ľ	0.94	50 6,150	6150	6	300 TOTAL	282 26,286
		0.71	0,150			IOTAL	20,200



1,900 TOTAL

Peat			
depths		Note - peat probe	
along		locations are not	
track		sequential along tracks	
(m)	Track length (m)	for all locations	Yellow - floating road
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0.00	50		
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0.12	50		
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0.12	50		
0.13	50		
0.17	50		
0.18	50		
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0.21	50		
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0.44 0.44 0.45 0.45 0.45	50 50		

-			
Peat			
depths		Note - peat probe	
along		locations are not	
track	—	sequential along tracks	
(m)	Track length (m)	for all locations	Yellow - floating road
0.49	50		
0.49	50		
0.50	50		
0.50	50		
0.50	50		
0.50	50		
0.50	50		
0.50	50		
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0.50	50		
0.50	50		
0.50	50		
0.50	50		
0.50	50		
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0.52	50		
0.52	50		
0.54	50		
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0.54 0.56	50 50		
0.57	50		
0.58 0.59	50		
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0.70	50		
0.70	50		
0.71	50		
0.71	50		
0.75	50		
0.75	50		
0.77	50		
0.79	50		
0.80	50		
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0.80	50		
0.82	50		
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	50		
0.82			
0.82 0.82 0.83	50 50		

Peat depths		Note - peat probe	
along		locations are not	
track		sequential along tracks	
(m)	Track length (m)	for all locations	Yellow - floating road
0.84	50		
0.84	50		
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0.91	50		
0.92	50 50		
	50		
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0.94	50		
1.00	50		
1.00	50		
1.02	50		
1.02	50		
1.00	50		
1.07	50		
1.00	50		
1.10	50		
1.10	50		
1.12	50		
1.25	50		
1.20	50		
1.20	50		
1.30	50		
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1.65 1.70 1.70 1.72 1.72 1.80 1.80 1.80 1.82 1.84	50 50 50 50 50 50 50 50 50 50 50		
1.65 1.70 1.70 1.72 1.72 1.80 1.80 1.80 1.82 1.84 1.85	50 50 50 50 50 50 50 50 50 50 50 50		
1.65 1.70 1.72 1.72 1.80 1.80 1.80 1.82 1.84 1.85 1.90	50 50 50 50 50 50 50 50 50 50 50 50 50		
1.65 1.70 1.72 1.72 1.72 1.80 1.80 1.82 1.84 1.85 1.90 1.90	50 50 50 50 50 50 50 50 50 50 50 50 50 5		
1.65 1.70 1.72 1.72 1.72 1.80 1.80 1.80 1.82 1.84 1.85 1.90 1.90 2.10	50 50 50 50 50 50 50 50 50 50 50 50 50 5		
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1.65 1.70 1.72 1.72 1.72 1.80 1.80 1.80 1.82 1.84 1.85 1.90 1.90 2.10 2.20 2.22	50 50 50 50 50 50 50 50 50 50 50 50 50 5		
1.65 1.70 1.72 1.72 1.72 1.80 1.80 1.80 1.82 1.84 1.85 1.90 1.90 2.10 2.20	50 50 50 50 50 50 50 50 50 50 50 50 50 5		

Wind Turbines on peat <0.5m Area of	Wind Turbines on peat >0.5m		cess Tracks	Upgraded access track (Not used for this project) Peat Width of Volume	Construction compound
restoratio Depth of Turbine n rest. Total Vol.	Area of Depth of Turbine restoration restoration Total Vol.	Peat depth track resto	th of Depth of Volume of pration restoration restoration	depths Track restoratio Depth of of along length (m) n rest. restoratio	Compound Total Areas Peat Depth Volume m3
1 1500 0.3 450 6 1500 0.4 600	2 2362.5 0.5 1,181 3 2362.5 0.5 1,181	0.00 50 0.00 50	6 0.00 0 6 0.00 0		Primary 10000 0.51 5100
10 1500 0.44 660 11 1500 0.22 330	4 2362.5 0.5 1,181 5 2362.5 0.5 1,181	0.00 50 0.00 50	6 0.00 0 6 0.00 0		5100
14 1500 0.15 225 18 1500 0.26 390	7 2362.5 0.5 1,181 8 2362.5 0.5 1,181	0.00 50 0.00 50	6 0.00 0 6 0.00 0		Borrow Pits
Total 2,655	9 2362.5 0.5 1,181 12 2362.5 0.5 1,181	0.00 50 0.00 50	6 0.00 0 6 0.00 0		Number Total Area Peat depth Volume A 30000 0.33 9900 0 restoration as <0.5m
	13 2362.5 0.5 1,181 15 2362.5 0.5 1,181	0.00 50 0.00 50	6 0.00 0 6 0.00 0		B 10000 0.34 3400 0 restoration as <0.5m C 10000 1.05 10500
	16 2362.5 0.5 1,181 17 2362.5 0.5 1,181	0.00 50 0.00 50	6 0.00 0 6 0.00 0		
	19 2362.5 0.5 1,181	0.00 50 0.10 50	6 0.00 0 6 0.00 0		TOTAL 10500
	Total 15,356	0.12 50 0.12 50	6 0.00 0 6 0.00 0		
25m square hole with 2.5m batter	25m square hole with 2.5m batter	0.15 50	6 0.00 0		TOTAL RESTORATION VOLUMES
2011 Square Hole Wait 2.011 Datter	2011 Square note with 2.011 baller	0.17 50	6 0.00 0		
		0.18 50 0.20 50	6 0.00 0 6 0.00 0		Turbines on peat 0 excavated New access tracks 26,286
27.5		0.21 50 0.21 50	6 0.00 0 6 0.00 0		Upgraded access track 0 Up Construction compounds 5100
		0.22 50 0.22 50	6 0.00 0 6 0.00 0		Borrow pits 10500 TOTAL 41,886
		0.22 50 0.23 50	6 0.00 0 6 0.00 0		
		0.23 50 0.25 50	6 0.00 0 6 0.00 0		
50		0.25 50 0.25 50	6 0.00 0 6 0.00 0		
		0.26 50 0.26 50	6 0.00 0 6 0.00 0		
		0.26 50	6 0.00 0 6 0.00 0		
road		0.27 50 0.28 50 0.28 50	6 0.00 0 6 0.00 0		
		0.29 50 0.30 50	6 0.00 0 6 0.00 0		
25		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
Perimeter - can only restore in 2 sides of crane pad as		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
road and foundations take up 2 sides		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
		0.30 50 0.30 50	6 0.00 0 6 0.00 0		
		0.32 50 0.32 50	6 0.00 0 6 0.00 0		
		0.32 50 0.34 50 0.34 50	6 0.00 0 6 0.00 0		
		0.35 50 0.35 50	6 0.00 0 6 0.00 0		
		0.35 50 0.36 50	6 0.00 0 6 0.00 0		
		0.37 50 0.38 50	6 0.00 0 6 0.00 0		
		0.38 50 0.38 50 0.38 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.39 50 0.39 50	6 0.00 0 6 0.00 0		
		0.39 50 0.39 50 0.40 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.40 50 0.40 50 0.40 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.40 50 0.40 50 0.40 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.40 50 0.40 50	6 0.00 0 6 0.00 0		
		0.40 50 0.40 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.40 50 0.41 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.41 50 0.41 50 0.41 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.43 50	6 0.00 0		
		0.44 50	6 0.00 0 6 0.00 0		
		0.44 50 0.44 50	6 0.00 0 6 0.00 0 6 0.00 0		
		0.44 50 0.45 50	6 0.00 0		
		0.45 50 0.45 50	6 0.00 0		
		0.45 50 0.47 50	6 0.00 0 6 0.00 0		
		0.48 50	6 0.00 0		

6666666666666666666

12,285 26,286 0 5,100 12,276 332 10,500 13,813



1	All peat depths roads	Average peat	depths at turbine locations
	0.00	2.40	

All peat depths roads	Average peat	depths at
0.00	2.40	
0.00	0.50	
0.00	1.15	
0.60	0.85	
0.30	2.50	
0.21	0.50	
0.10	0.70	
0.44	0.50	
0.75	1.00	
0.32	1.15	
0.25	1.10	
1.72	2.40	
0.85	1.50	
0.82	0.3	
0.50	0.4	
0.35	0.44	
0.47	0.22	
0.44	0.15	Ì
0.44	0.26	Ì
0.84		Average
0.86		
0.86		
0.86		
0.49		
0.90		
0.90		
0.82	•	
0.93	•	
1.34	•	
1.65	•	
0.71		
0.83		
0.91		
2.10		
0.25		
0.12		
0.86		
1.82		
0.70		
0.12		
0.35		
0.37	l.	
0.15		
0.54		
0.22		
0.41		
0.17		
0.69		
0.25		
0.34		
0.65		
0.30		
0.50		
0.30		
0.40		
0.00		
0.00		
0.00		
0.30		
0.60		
0.30		
1.40		

Track length	m Total	
Floating	1,900	
New tracks	11,000	
Upgrade	0	
Total Length	12,900	

Extra peat excavation	Volume m3 A	rea m2
Primary compound	5,100	10,000
Passing Places	2,550	
Control building	12,276	19,800
Met masts	332	425
Borrow Pit	10,500	30,000
Totals	30,758	60,225

Floating road not requiring drainage 1,900

1.40	
0.60	1
0.30	
0.40	
0.85	
0.40	
0.60	
0.45	4
0.40	4
0.70	+
0.30	
0.30	
0.90	
0.50	1
0.60	1
0.50	4
0.30	
0.50	
0.45	
0.00	
0.30	
0.00	4
0.60	1
0.90	1
0.60	
1.10	t
0.40	
0.90	
1.00	
0.90	1
0.30	1
0.30	
0.50	
0.80	
0.80	
0.60	1
0.60	4
0.90	+
0.30	
0.30	
0.60	
0.00	4
0.00	
<u> </u>	
0.50	+
1.80	
0.30	
0.30	
0.40	4
0.40	
0.50	
1.30	
0.90	
0.00	
0.50	Į
0.70	
0.70	
0.85	
0.40	
1.40	
0.80	1
1.90	
1.70	

All peat depths roads Average peat depths at turbine locations
0.90
1.80
0.90
0.70
0.70
0.45
0.40
0.90
0.90
0.90
0.00

0.00 1.10 0.40 0.00 0.60 0.90 0.32 0.87 0.59 0.26 0.60

 1.85

 1.02

 0.43

 1.44

 0.50

 0.52

 0.70

 0.50

0.34 0.52 0.50

0.66 0.29 0.88

0.64 0.87 2.22 1.26

0.65 0.94 0.92 0.50 0.23 0.39 0.36 0.44 0.26 0.48 0.22 0.23 0.21 0.69 0.22 0.27 0.39 0.17 0.77 0.41 0.77 0.41 0.41 0.99 0.49

0.44 2.27 1.12 0.86

1.08 1.28 1.02

0.65 1.58 0.38 0.60 0.71 1.84 0.84 0.57

0.58 0.56 0.70 0.50

0.62 0.28 0.35 0.79 0.61 0.90 0.61 0.82 0.64 0.82 0.64 0.75 0.38 0.64 1.07 0.69 1.41 1.72

1.72	
0.64	
0.66	
0.18	
0.26	
0.45	
0.54	
0.94	
0.85	
0.65	
0.94	
1.03	
0.28	
0.70	
0.20	
0.80	
1.25	-
2.30	•
0.90	1
1.90	l l
1.70	
1.40	<u> </u>
2.20	<u> </u>
2.25	<u>.</u>

	Track length	Track	Excavated	
	(m)	width (m)		Volumes
1.00	50	6	300	300
1.02	50	6	300	306
1.02	50	6	300	306
1.03	50	6	300	309
1.07	50	6	300	321
1.08	50	6	300	324
1.10	50	6	300	330
1.10	50	6	300	330
1.12	50	6	300	336
1.25	50	6	300	375
1.26	50	6	300	378
1.28	50	6	300	384
1.30	50 50	6	300	390
1.30	<u>50</u> 50	6	300	390 402
1.34 1.40	50 50	6 6	<u>300</u> 300	402
1.40	50 50	6	300	420
1.40	50	6	300	420
1.40	50	6	300	420
1.41	50	6	300	423
1.58	50	6	300	474
1.65	50	6	300	495
1.70	50	6	300	510
1.70	50	6	300	510
1.70	50	6	300	516
1.72	50	6	300	516
1.80	50	6	300	540
1.80	50	6	300	540
1.84	50	6	300	552
1.85	50	6	300	555
1.90	50	6	300	570
1.90	50	6	300	570
2.10	50	6	300	630
2.20	50	6	300	660
2.22	50	6	300	666
2.25	50	6	300	675
2.27	50	6		681
2.30	50	6	300	690
1.55	1,900			17,646



Appendix 6.D Carbon Calculator Spreadsheet

Due to the number of pages the full carbon spreadsheet has been provided in digital format only. If a paper copy is required, it is available from Eon on request.



Scottish Government Windfarm Carbon Assessment Tool - Version 2.9.0 26/03/2014	
This spreadsheet calculates payback time for windfarm sited on peatlands using methods given in	¹ D.Nayak, ¹ J.U. Smith , ¹ P. Smith,
Nayak et al, 2008 (<u>http://www.scotland.gov.uk/Publications/2008/06/25114657/0</u>)	¹ P.Graves
and revised equations for GHG emissions (Nayak, D.R., Miller, D., Nolan, A., Smith, P. and Smith, J.U., 2010, Calculating carbon budgets of wind	
farms on Scottish peatland. Mires and Peat 4: Art. 9. Online: (http://www.mires-and-peat.net/map04/map_04_09.htm)	
Version 2.0.0 - Adapted to include detail of forestry management, Smith et al., 2011.	
http://www.scotland.gov.uk/WindFarmsAndCarbon	OF ABERDEEN
Version 2.9.0 - Includes multiple regions for forestry and construction (access to calculation worksheets protected for planning purposes).	
Revised by J.U.Smith to correct forestry and resotration sheets	² P Millor ² A Nolan ² L Morrico
Version 2.9.1 - Equivalent to version 2.8.0 but with worksheets unprotected for your own use. Do not use this version in planning applications.	2 The James
	Hutton
	Institute
INSTRUCTIONS	
A There are 6 worksheets giving instructions, data entry and outputs,	204 Decks 2D Construct
Instructions	3 CA Forestry Commission
Do I need to use this tool?Click here to find out Click here	Car rolesity commission
Core input data Data needed in all calculations Click here	40.00
Forestry input data Extra details sometimes needed for forestry calculations	4 THE UNIVERSITY of EDINBURGH
Construction input data Extra details sometimes needed for construction calculations	THE UNIVERSITE OF EDINBURGH
Payback time and CO2 emissions Click here	
and 8 numbered worksheets showing calculations:	5 Inivorcity
1. Windfarm CO ₂ emission saving	University
2. CO2 loss due to turbine life	Set Glasgow
3. CO2 loss due to backup	
4. Loss of CO ₂ Fixing Pot.	
5. Loss of soil CO2	
5a. Volume of peat removed	Note on official version number
5b. CO2 loss from removed peat	Note on official version number
5c. Volume of peat drained	
5d. CO_2 loss from drained peat	Version X.Y.Z
5e. Emission rates	
6. CO ₂ loss by DOC & POC loss	X refers to the release number
7i. Forestry CO_2 loss - simple	Y refers to released updates on
7ii. Forestry CO_2 loss - detailed	release X Z refers to unreleased updates on
7a. C sequest. in trees (3PG)	release X.Y
7b. C seq. in soil under trees	
7c. Average stand data	Officially released versions will
7d. Windspeed ratios	always have Z=0
8. CO_2 gain - site improvement	
In addition, there are spreadsheets containing references and requesting feedback. References	If you make changes of your own,
	please do not refer to your modified
Frequently asked questions	spreadsheet using the official version
	number.
Notes on calculations are given in pale green text boxes Click here to see example of Notes Box	The latest version is published at
Protocols for measurements are given in pale yellow comment boxes Click here to see example of Protocol Box	www.scotland.gov.uk/WindFarmsAn
Assumptions are given in pale blue text boxes Click here to see example of Assumptions Box	dCarbon
	Please check you are using the latest
	official version with Z=0 before
	submitting a planning application.


Do I need to use this tool?			
1. Will the site be drained on construction of the windfarm?	No 🔻		
2. Is the soil at the site highly organic? i.e. is the soil organo-mineral or organic, (i.e. a peaty gley or peat)?	Yes 🔻		
3. Does windfarm construction require a significant amount of deforestation? i.e. is removal in excess of keyholing the turbines within the forest boundary?	No		
You should use this tool because the soil is highly organic. Please move to the Core input data sheet and complete the form	1 to obtain an estim	ate of C payback time	
		Click here to return to Instructions sheet	Click her
		Click here to move on to Core input data sheet	Click h

Core input data ENTER INPUT DATA HERE! VALUES SHOULD ONLY BE CHANGED ON THIS SHEET. DO NOT USE EXAMPLE VALUES AS DEFAULTSIENTER YOUR OWN VALUES THAT ARE SPECIFIC TO YOUR PARTICULAR SITE. Note: The input parameters include some variables that can be specified by default values, but others that must be site specific. Variables that can be taken from defaults are marked v purple tags on left hand side.

Click here to move to Payback Time Click here Click here to return to Instructions

	Expected values		Pos		nge of values	_	
Input data	Enter expected value here	Record source	Enter minimum value here	Record source	Enter maximum value here	Record source	
		of data		of data		of data	Note: Capacity factor. The capacity factor of any power plant is the proportion of energy produced
Windfarm characteristics	*		¥		*		Note: <u>Capacity relator</u> . The capacity factor or any power plant is the proportion or energy produced during a given period with respect to the energy that would have been produced had the wind farm been running continually and at maximum output (DECC (2004); see also
<u>Dimensions</u> No. of turbines	19		19		19		www.bwea.com/ref/capacity/actors.html). Capacity Factor = Electricity generated during the period [kWh]/ (Installed capacity [kW] x
Lifetime of windfarm (years)	25	Fixed	25		25		number of hours in the period [h]) The average capacity factor between 1998 and 2004 for Scotland was 30% (DTI, 2006, Energy
Performance Power rating of turbines (turbine capacity) (MW)	3.3		3.3		3.3		Trends, March 2006). We recommend that a site-specific capacity factor site should be used (as measured during planning stage). The average capacity factor for the United Kinodom, in 2009.
Capacity factor	Direct input of capacity factor		Direct input of capacity factor		Direct input of capacity factor		was 27%, and 28% for Scotland (Energy Trends, September 2010)
Enter estimated capacity factor (percentage efficiency)	27.0		21.8		33.6		Note: Extra capacity required for backup . If 20% of national electricity is generated by wind energy, the extra capacity required for backup is 5% of the rated capacity of the wind plant (Dale
Backup Extra capacity required for backup (%)	5		0		5 🗲		et al 2004, Energy Policy, 32, 1949-56). We suggest this should be 5% of the actual output. If it is assumed that less than 20% of national electricity is generated by wind energy, a lower
Additional emissions due to reduced thermal efficiency of the	10		10		10		percentage should be entered (0%). The House of Lords Economic Affairs Committee report on The Economics of Renewable Energy
reserve generation (%) Carbon dioxide emissions from turbine life -	Calculate wrt installed capacity		Calculate wrt installed capacity		Calculate wrt installed capacity		(2008) (www.parliament.the-stationery-office.co.uk/pa/td200708tdselect/ideconal/195/19507.htm#n36) notes that to cover peak demand a '20% margin of extra capacity has been sufficient to keep the risk of a power cut
(eg. manufacture, construction, decommissioning)	Calculate wit instaned capacity		carculate with installed capacity		calculate wit installed capacity		due to insufficient generation at a very low level.' The estimate provided by BERR was a range of 10% to 20% of installed capacity of wind energy. E.ON is reported as proposing that the capacity
							credit of wind power should be 8%, and The Renewable Energy Foundation proposed the use of the square root of the wind capacity (in GW) as conventional capacity (e.g. 36 GW of wind plant to
					×		match 6 GW of conventional plant).
Characteristics of peatland before windfarm development							Note: Extra emissions due to reduced thermal efficiency of the reserve power generation ≈ 10%
Type of peatland	Acid bog 💌		Acid bog 💌		Acid bog 💌 💌		Note: <u>Emissions from turbine life If</u> total emissions for the windfarm are unknown, emissions
Average annual air temperature at site (°C)	7.5		3.9		11.2		will be calculated according to turbine capacity. The normal range of CO ₂ emissions is 394 to 8147 t CO ₂ MW (White & Kulcinski, 2000; White, 2007).
Average depth of peat at site (m) C Content of dry peat (% by weight)	0.68 55		0.50 49		1.00 62		
Average extent of drainage around drainage features at site (m)	7.50		5.00		10.00		Note: <u>Type of peatland</u> An 'acid bog' is fed primarily by rainwater and often inhabited by sphagnum moss, thus making it acidic. See Stoneman & Brooks (1997).
Average water table depth at site (m)	0.30 0.25		0.20 0.20		0.40 0.45		A 'fen' is a type of wetland fed by surface and/or groundwater. See McBride et al. (2011).
Dry soil bulk density (g cm ⁻³) Characteristics of bog plants	0.25		0.20		0.45		Note: Time required for regeneration of previous habitat. Loss of fixation should be assumed to
Time required for regeneration of bog plants after restoration	3		2		5 🛀		be over lifetime of windfarm only. This time could be longer if plants do not regenerate. The requirements for after-use planning include the provision of suitable refugia for peat-forming
(years) Carbon accumulation due to C fixation by bog plants in						/	vegetation, the removal of structures, or an assessment of the impact of leaving them in situ. Methods used to reinstate the site will affect to likely time for regeneration of the previous habitat.
undrained peats (tC ha ⁻¹ yr ⁻¹)	0.25		0.12		0.31		This time could also be shorter if plants regenerate during lifetime of windfarm. If so, enter number of years estimated for regeneration.
Forestry Plantation Characteristics							Note: Carbon fixation by bog plants
Method used to calculate CO_2 loss from forest felling Area of forestry plantation to be felled (ha)	Enter simple data		Enter simple data		Enter simple data		Apparent C accumulation rate in peatland is 0.12 to 0.31 tC ha ⁻¹ yr ⁻¹ (Turunen et al., 2001; Botch et al., 1995). The SNH guidance uses a value of 0.25 tC ha ⁻¹ yr ⁻¹ .
Average rate of carbon sequestration in timber (tC ha-1 yr-1)							1 yr4.
Counterfactual emission factors							Note: Area of forestry plantation to be felled. If the forestry was planned to be removed, with no
To update counterfactual emission factors from the web Click here							further rotations planted, before the windfarm development, the area to be felled should be entered as zero.
(not yet operational) Coal-fired plant emission factor (t CO ₂ MWh ⁻¹)	0.907		0.907		0.907	\backslash	Note: Plantation carbon sequestration. This is dependent on the yield class of the forestry. The
Grid-mix emission factor (t CO_2 MWh ⁻¹)	0.454		0.454		0.454		SNH technical guidance assumed yield class of 16 m3 ha ⁻¹ yr ⁻¹ , compared to the value of 14 m3 ha ⁻¹ yr ⁻¹ provided by the Forestry Commission. Carbon sequestered for yield class 16 m ³ ha ⁻¹ y ⁻¹
Fossil fuel-mix emission factor (t CO_2 MWh ⁻¹)	0.701		0.701		0.701		= 3.6 tC ha ⁻¹ yr ⁻¹ (Cannell, 1999).
Borrow pits							Note: Coal-Fired Plant and Grid Mix Emission Factors. Coal-fired plant EF = 0.86 t CO ₂ MWh ⁻¹ :
Number of borrow pits Average length of pits (m)	1 100		1 50		1 150		Grid-Mix EF = 0.43 t CO ₂ MWh ⁻¹ Source = Defra, 2002.
Average width of pits (m)	100		50		150		Note: Fossil Fuel-Mix Emission Factor. The 5 year average emission factor calculated using estimated CO ₂ emissions for 2002 and 2003 from the National Atmospheric Emission Inventory
Average depth of peat removed from pit (m)	1.05		1.00		1.10		(Baggott et al., 2007), and for 2004 to 2006 (Digest of UK Energy Statistics, 2007) is 0.607 tCO ₂ MWh ⁻¹ .
Foundations and hard-standing area associated with each turbine							
Method used to calculate CO ₂ loss from foundations and hard-	Enter detailed information		Enter detailed information		Enter detailed information		
standing Please enter construction data in sheet: Construction input data	27.5		25		27.5		
r lease enter construction data in sheet. Construction input data	27.5		25		27.5		
Average depth of peat removed from turbine foundations (m)	0.95		0.75		1.25		
	50 25		50 25		50 25		
Average depth of peat removed from hard-standing (m)	0.69		0.50		1.00		
Access tracks Total length of access track (m)	12900		12900		12900 ◄		Note: Total length of access track. If areas of access track overlap with hardstanding area,
Existing track length (m)	0		0		0		exclude these from the total length of access track to avoid double counting of land area lost.
Length of access track that is floating road (m) Floating road width (m)	1900 6		1800 6		2000 6		
Floating road depth (m)	0.50		0.50		0.50		Note: Floating road depth. Accounts for sinking of floating road. Should be entered as the average depth of the road expected over the lifetime of the windfarm. If no sinking is expected,
Length of floating road that is drained (m) Average depth of drains associated with floating roads (m)	1900 0.50		1900 0.50		1900 ∢ 0.50	_	enter as zero Note: Length of floating roat that is drained. Refers to any drains running along the length of the
Length of access track that is excavated road (m)	11000		10500		11500		road
Excavated road width (m) Average depth of peat excavated for road (m)	6 0.58		6 0.50		6 0.70		Note: Rock filled roads. Rock filled roads are assumed to be roads where no peat has been
Length of access track that is rock filled road (m)							removed and rock has been placed on the surface and allowed to settle.
Rock filled road width (m) Rock filled road depth (m)							
Length of rock filled road that is drained (m)							
Average depth of drains associated with rock filled roads (m) Cable Trenches						_	
Length of any cable trench on peat that does not follow access							
tracks and is lined with a permeable medium (eg. sand) (m)	0		0		0		Note: Depth of peat cut for cable trenches. In shallow peats, the cable trenches may be cut below
Average depth of peat cut for cable trenches (m)	0.00		0.00		0.00		the peat. To avoid overestimating the depth of peat affected by the cable trenches, only enter the depth of the peat that is cut.
Additional peat excavated (not							
already accounted for above) Volume of additional peat excavated (m ³)	20258		19500		21000		
Area of additional peat excavated (m ²)	34400.0		33050.0		35595.0		Note: <u>Peat Landslide Hazard</u> . It is assumed that measures have been taken to limit damage (Scottish Executive, 2006, Peat Landslide Hazard and Risk Assessments. Best Practice Guide for Proposed Electricity Generation
Peat Landslide Hazard					+		Developments. Scottish Executive, Edinburgh. pp. 34-36) so that C losses due to peat landslide can be assumed to be negligible. Link: http://www.scottand.gov.uk/Publications/2008/12/21162303/1.
Weblink: Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation							
Developments							
Improvement of C sequestration at site by blocking drains, restoration of habitat etc							
Improvement of degraded bog							
Area of degraded bog to be improved (ha)							
Water table depth in degraded bog before improvement (m) Water table depth in degraded bog after improvement (m)							
Time required for hydrology and habitat of bog to return to its							Note: <u>Period of time when improvement can be guaranteed</u> . This gurantee should be absolute. Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong
previous state on improvement (years) Period of time when effectiveness of the improvement in							supporting evidence that this improvement can be guaranteed for the full period given. This includes the time requirement for the improvement to become effective. For example if time required for
degraded bog can be guaranteed (years)					+		hydrology and habitat to return to its previous state is 10 years and the restoration can be guaranteed over the lifetime of the windfarm (25 years), the period of time when the improvement
Improvement of felled plantation land Area of felled plantation to be improved (ha)							can be guaranteed should be entered as 25 years, and the improvement will be effective for (25 -t0) = 15 years.
Water table depth in felled area before improvement (m)							
Water table depth in felled area after improvement (m) Time required for hydrology and habitat of felled plantation to							Note: Period of time when improvement can be guaranteed. This gurantee should be absolute.
return to its previous state on improvement (years)							Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong supporting evidence that this improvement can be guaranteed for the full period given. This includes
Period of time when effectiveness of the improvement in felled					•		supporting evidence that this improvement can be guaranteed for the full period given. This includes the time requirement for the improvement to become effective. For example if time required for hydrology and habitat to return to its previous state is 10 years and the restoration can be
plantation can be guaranteed (years) Restoration of peat removed from borrow pits							nydrology and nabitat to return to its previous state is 10 years and the restoration can be guaranteed over the lifetime of the windfarm (25 years), the period of time when the improvement can be guaranteed should be entered as 25 years, and the improvement will be effective for (25 -10)
Area of borrow pits to be restored (ha)	5		4		5		can be guaranteed should be entered as 25 years, and the improvement will be enective for (25 -10) = 15 years.
Depth of water table in borrow pit before restoration with respect to the restored surface (m)	0.20		0.10		0.30		
Depth of water table in borrow pit after restoration with respect to	0.30		0.20		0.40		
the restored surface (m) Time required for hydrology and habitat of borrow pit to return to							Note: <u>Period of time when improvement can be guaranteed</u> . This gurantee should be absolute. Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong
its previous state on restoration (years)	3.0		2.0		4.0		supporting evidence that this improvement can be guaranteed for the full period given. This includes the time requirement for the improvement to become effective. For example if time required for
Period of time when effectiveness of the restoration of peat removed from borrow pits can be guaranteed (years)	22		23		21 🗲		hydrology and habitat to return to its previous state is 10 years and the restoration can be guaranteed over the lifetime of the windfarm (25 years), the period of time when the improvement
Early removal of drainage from foundations and hardstanding							can be guaranteed should be entered as 25 years, and the improvement will be effective for (25 -10) = 15 years.
Water table depth around foundations and hardstanding before restoration (m)							
restoration (m) Water table depth around foundations and hardstanding after						•	Note: <u>Period of time when improvement can be guaranteed</u> . This is assumed to be the lifetme of the windfarm as restoration after windfarm decomissioning is already accounted for in restoration of the
restoration (m)							Site

It is a summary of the second seco

restoration (m) Water table depth around foundations and hardstanding detore restoration (m) Time to completion of backfilling, removal of any surface drains, and full restoration of the hydrology (years)				•	Note: <u>Period of time when improvement can be guaranteed</u> . This is assumed to be the lifetme of the windfarm as restoration after windfarm decomissioning is already accounted for in restoration of the site Note: <u>Restoration of site</u> . Iff the water table at the site is returned to its original level or higher on
Restoration of site after decomissioning			. +		decommissioning, and habitat at the site is restored, it is assumed that C losses continue only over the lifetime of the windfarm. Otherwise, C losses from drained peat are assumed to be 100%.
Will the hydrology of the site be restored on decommissioning?	No	No	No		
Will you attempt to block any gullies that have formed due to the windfarm? Will you attempt to block all artificial ditches and facilitate rewetting?	Yes 💌 No 💌	Yes Vo	No		
Will the habitat of the site be restored on decommissioning?	No	No	No		
Will you control grazing on degraded areas?	Yes 💌	Not applicat	Yes 🔻		
Will you manage areas to favour reintroduction of species	No	No	No 💌		Note: Choice of methodology for calculating emission factors. The IPCC default methodology is the

Choice of methodology for calculating emission factors Site specific (required for planning applications)

Core input data ENTER INPUT DATA HEREI VALUES SHOULD ONLY BE CHANGED ON THIS SHEET. DO NOT USE EXAMPLE VALUES AS DEFAULTSIENTER YOUR OWN VALUES THAT ARE SPECIFIC TO YOUR PARTICULAR SITE. Note: The input parameters include some variables that can be specified by default values, but others that must be site specific. Variables that can be taken from defaults are marked purple tags on left hand side.

Invoir: <u>Uncice of methodology for calculating emission factors</u>. The IPCC default methodology is the internationally accepted standard (IPCC, 1997). However, it is stated in IPCC (1997) that these are rough estimates, and "these rates and production periods can be used if countries do not have more appropriate estimates". Therefore, we have developed more site specific estimates for use here based on work from the Sociatis Government flunded ECOSE product (simm et a).coccess Estimating Carbon in Organic Sole - Sequestration and Emissions. Final Report. ISEN 976-01560.

Click here to move to Payback Time Click here Click here to return to Instructions



Forestry input data ENTER DETAILS OF FORESTRY MANAGEMENT HERE!

Note: Data only needed if select to calculate capacity factor from forestry data (cell C15 in Core input data sheet), or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include detailed forestry management (cell C35 in Core input data sheet) (or to include data sheet) (or to include data sheet) (or to include data sheet) (or ton

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No POC losses for bare soil included yet. If extensive areas of base soil is preser	nt at site need modified calculation.						
Г	Expected values		Po	ssible rai	nge of values		Note: Estimated downtime. Estimated downtime for maintenance etc. Few reports on downtime of wind turbines are publically available. However, one review by Garrad Hassan (2011) suggests
lanut data		Record		Record		Record	that the minimum downtime reported was 2% for the annual moving average for between 8 to 9 years of operation of new turbines, for a sample of 240 turbines. For a summary of findings see
Input data	Enter expected value here	source	Enter minimum value here	source		source	Garrad Hassan (2011).
	•	of data	+	of data	+	of data	Note: <u>Emissions from felling and timber removal</u> . Based on emissions factors from UK taken from Morison et al (2011), if clearfelling assumed to be
Windfarm characteristics							performed by harvester and timber is assumed extracted with forwarder, the emissions are 6675 g $\ensuremath{CO_2}\xspace\mathrm{m^3}$
Distance to nearest biofuel plant (km)					/		Note: Emissions associated with transportation.
<u>Dimensions</u> Total wind farm area (ha)							Assuming trasportation by trucks running on diesel and 20% of journey taken on forest roads, emissions factor obtained from Morison et al (2011) is 39.33 g CO ₂ km ⁻¹ t ⁻¹ (range 38.5 – 40.15 g
Performance							$CO_2 \text{ km}^{-1} \text{ t}^{-1}$ - average = 39.33 g $CO_2 \text{ km}^{-1} \text{ t}^{-1}$)
Height of turbines (m)							
Average site windspeed (m s ⁻¹) Estimated downtime for maintenance etc (%)					▶ /		
Emissions due to forestry operations							
Emissions from felling (g CO ₂ m ⁻³)					*/		
Emissions of CO ₂ associated with transportation (g CO ₂ km ⁻¹ t ⁻¹)					*		
Forestry Plantation Characteristics Note - total number of turbines already specified							Note: Power curve Based on Vestas 2.0MW Optispeed turbine with roughness class C2, modelled over wind speed
AREA 1							of 5-10 m s ⁻¹ . To define a the power curve for a different turbine type, plot annual power output, <i>F</i> (MWh) against annual windspeed, W (m s ⁻¹) and fit a linear regression to obtain slope, a, and
Number of turbines in this area Power curve - NOT USED!	User-defined		User-defined	1	there do for a d		intercept, b: P = aW + b
(In CORE INPUT DATA sheet you have selected	User-defined		User-defined		User-defined		$P \equiv dW + D$
to input capacity factor directly. No need to select!)							
Major soil sub-group	Peaty gley 💌		Peaty gley	2	Peaty gley	-	Note Orlands server
Species	Scots pine		Scots pine 💌		Scots pine 💌 💌		Note: <u>Soil sub-group</u> Used in determination of forestry characteristic.
Felled Forest Biomass used as biofuel?	No		No		No		Peaty gley = Peaty Soils (5-50cm) e.g. peaty gley, peaty podsol Deep peat = Deep Peat (>50cm) e.g. basin and blanket bogs
Felling regime				•			
Age of forestry when felled for windfarm (yr)							Note: <u>Species</u> So far only Scots pine and Sitka spruce included.
Area felled around each turbine (ha)							Note: Value of folled foreste: Values sustable in Manual J. 2000
Width of forest around felled area (m) Value of felled forestry as a biomass fuel (MW/b f^{1})							Note: <u>Value of felled forestry</u> Values available in Mason et al., 2009.
Value of felled forestry as a biomass fuel (MWh t ¹) (Carbon : Biomass) ratio of felled forestry							
Replanting regime				1			Note: Carbon : Biomass ratio of felled forestry Wood biomass can be converted to dry
Years after felling when replanting occurs Age of seedlings on planting (yr)							weight using wood density based values from Lavers (1983) with a subsequent
Area replanted around each turbine (ha)							assumption that C:dry matter ratio is 50% (Matthews 1993). For simplicity an integrated factor, the 'wood density to biomass factor' taken from Mason et al (2009)
AREA 2							can be used.
Number of turbines in this area				-			Value = 0.5
Power curve - NOT USED! (In CORE INPUT DATA sheet you have selected	•		•		•		
to input capacity factor directly. No need to select!)							
Major soil sub-group					•		
· · ·					-		
Species							
Felled Forest Biomass used as biofuel?							
Felling regime Age of forestry when felled for windfarm (yr)							
Area felled around each turbine (ha)							
Width of forest around felled area (m)							
Value of felled forestry as a biomass fuel (MWh t ¹)							
(Carbon : Biomass) ratio of felled forestry Replanting regime				•			
Years after felling when replanting occurs							
Age of seedlings on planting (yr) Area replanted around each turbine (ha)							
AREA 3 Number of turbines in this area							
Power curve - NOT USED!	•		•		▼		
(In CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!)							
Major soil sub-group					•		
Species					•		
Felled Forest Biomass used as biofuel?							
Felling regime							
Age of forestry when felled for windfarm (yr) Area felled around each turbine (ha)							
Width of forest around felled area (m)							
Value of felled forestry as a biomass fuel (MWh t ⁻¹)							
(Carbon : Biomass) ratio of felled forestry Replanting regime							
Years after felling when replanting occurs							
Age of seedlings on planting (yr)							
Area replanted around each turbine (ha)							
AREA 4 Number of turbines in this area							
Power curve - NOT USED!	•		•	1	•		
(In CORE INPUT DATA sheet you have selected							
to input capacity factor directly. No need to select!)							
Major soil sub-group	•		· · · · · · · · · · · · · · · · · · ·		▼		
Species	•		▼		•		
Felled Forest Biomass used as biofuel?			•		-		
Felling regime				1			
Age of forestry when felled for windfarm (yr)							
Area felled around each turbine (ha) Width of forest around felled area (m)							
Value of felled forestry as a biomass fuel (MWh t ⁻¹)							
(Carbon : Biomass) ratio of felled forestry							
Replanting regime Years after felling when replanting occurs							
Age of seedlings on planting (yr)							
Area replanted around each turbine (ha)							
AREA 5							
Number of turbines in this area Power curve - NOT USED!				1			
(In CORE INPUT DATA sheet you have selected	•		•		· · · · · · · · · · · · · · · · · · ·		
to input capacity factor directly. No need to select!)							
Major soil sub-group	•				▼		
Species	•		•		•		

to input capacity factor directly. No need to select!)				
Major soil sub-group	•	▼	•	
Species			•	
Felled Forest Biomass used as biofuel?	•	•	▼	
Felling regime				
Age of forestry when felled for windfarm (yr)				
Area felled around each turbine (ha)				
Width of forest around felled area (m)				
Value of felled forestry as a biomass fuel (MWh t ¹)				
(Carbon : Biomass) ratio of felled forestry				
Replanting regime				
Years after felling when replanting occurs				
Age of seedlings on planting (yr)				
Area replanted around each turbine (ha)				

Forestry input data			

ENTER DETAILS OF FORESTRY MANAGEMENT HERE!	
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INTER DETAILS OF FORESTRY MAINAGEMENT HERE! Note: Data only needed if select to calculate capacity factor from forestry data (cell C15 in Core input data sheet), or to include detailed forestry management (cell C35 in Core input data sheet)

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Construction input data

ENTER DETAILS OFCONSTRUCTION HERE!

Note: This data only used in the calculation if the selection "Enter detailed information" is made in cell C50 of the Core input data sheet.

Click here to move to Payback Time Click here to return to Core input data

					Core input data	Knere
	Expected values		Pos	sible ran	ge of values	
Input data	Enter expected value here	Record source	Enter minimum value here	Record source	Enter maximum value here	Record source
		of data		of data		of data
Construction design Note - total number of turbines already specified:	19		19		19	
AKEA 1 Number of turbines in this area	19		19		19	
Turbine foundations	0.3		0.3		0.3	
Depth of hole dug when constructing foundations (m) Approximate geometric shape of whole dug when constructing	Rectangular		Rectangular 🗸		Rectangular	
foundations Length at surface (m)	27.5		25		27.5	
Width at surface (m) Length at bottom (m)	27.5 25		25 25		27.5 25	
Width at bottom (m)	25		25		25	
Depth of hole dug when constructing hardstanding (m)	0.6		0.6		0.6	
Approximate geometric shape of whole dug when constructing hardstanding	Rectangular		Rectangular		Rectangular	
Length at surface (m) Width at surface (m)	50 25		50 25		50 25	
Length at bottom (m) Width at bottom (m)	50 25		50 25		50 25	
Piling	No 🔽		No 🔽		No V	
Is piling used? Volume of Concrete						
Volume of concrete used (m ³)	750		500		750	
AREA 2 Number of turbines in this area						
Turbine foundations Depth of hole dug when constructing foundations (m)						
Approximate geometric shape of whole dug when constructing	Rectangular		Rectangular		Rectangular 💌	
foundations Length at surface (m)						
Width at surface (m) Length at bottom (m)						
Width at bottom (m)						
Hardstanding Depth of hole dug when constructing hardstanding (m)						
Approximate geometric shape of whole dug when constructing hardstanding	Rectangular		Rectangular		Rectangular	
Length at surface (m) Width at surface (m)						
Length at bottom (m)						
Width at bottom (m) Piling						
Is piling used? Volume of Concrete	No		No		No	
Volume of concrete used (m ³)						
AREA 3 Number of turbines in this area						
Turbine foundations						
Depth of hole dug when constructing foundations (m) Approximate geometric shape of whole dug when constructing	Rectangular		Rectangular		Rectangular	
foundations Length at surface (m)						
Width at surface (m) Length at bottom (m)						
Width at bottom (m) Hardstanding						
Depth of hole dug when constructing hardstanding (m)						
Approximate geometric shape of whole dug when constructing hardstanding	Rectangular		Rectangular		Rectangular	
Length at surface (m) Width at surface (m)						
Length at bottom (m) Width at bottom (m)						
Piling	No		No		No	
Is piling used? Volume of Concrete						
Volume of concrete used (m ³)						
AREA 4 Number of turbines in this area						
Turbine foundations Depth of hole dug when constructing foundations (m)						
Approximate geometric shape of whole dug when constructing	•		•		•	
foundations Length at surface (m)						
Width at surface (m) Length at bottom (m)						
Width at bottom (m) Hardstanding						
Depth of hole dug when constructing hardstanding (m) Approximate geometric shape of whole dug when constructing						
hardstanding			•			
Length at surface (m) Width at surface (m)						
Length at bottom (m) Width at bottom (m)						
Piling Is piling used?				••••••		
Volume of Concrete						
Volume of concrete used (m ³)						
AREA 5 Number of turbines in this area						
Turbine foundations Depth of hole dug when constructing foundations (m)						
Approximate geometric shape of whole dug when constructing foundations	•		-		-	
Length at surface (m)						
Width at surface (m) Length at bottom (m)						
Width at bottom (m) Hardstanding						
Depth of hole dug when constructing hardstanding (m) Approximate geometric shape of whole dug when constructing	-					
	-		•		-	
Length at surface (m) Width at surface (m)						
Length at surface (m)						
Width at surface (m) Length at bottom (m) Width at bottom (m) <u>Piling</u>						
Length at surface (m) Width at surface (m) Length at bottom (m) Width at bottom (m)						

Results PAYBACK TIME AND CO₂ EMISSIONS

Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generate coal-fired capacity or grid-mix.

Click here to return to Input data Click here to return to Instructions



	Exp.	Min.	Max.
1. Windfarm CO ₂ emission saving over	_		
coal-fired electricity generation (tCO ₂ yr ⁻¹)	134506	108601	167535
grid-mix of electricity generation (tCO ₂ yr ⁻¹)	67327	54361	83860
fossil fuel - mix of electricity generation (tCO ₂ yr ⁻¹)	103957	83936	129484
Energy output from windfarm over lifetime (MWh)	3707451	2993423	4617836
Total CO_2 losses due to wind farm (t CO_2 eq.)			
2. Losses due to turbine life (eg. manufacture, construction, decomissioning)	49830	49787	49830
3. Losses due to backup	48128	0	48128
4. Losses due to reduced carbon fixing potential	1057	369	1787
5. Losses from soil organic matter	59102	29471	199351
6. Losses due to DOC & POC leaching	0	0	0
7. Losses due to felling forestry	0	0	0
Total losses of carbon dioxide	158117	79627	299096
8. Total CO ₂ gains due to improvement of site (t CO ₂ eq.)			
8a. Gains due to improvement of degraded bogs	0	0	0
8b. Gains due to improvement of felled forestry	0	0	0
8c. Gains due to restoration of peat from borrow pits	0	0	0
8d. Gains due to removal of drainage from foundations & hardstanding	0	0	0
Total gains	0	0	0

RESULTS			
	Exp.	Min.	Max.
Net emissions of carbon dioxide (t CO _{2 eq} .)			
	158117	79627	299096
Carbon Payback Time			
coal-fired electricity generation (years)	1.2	0.5	2.8
grid-mix of electricity generation (years)	2.3	0.9	5.5
fossil fuel - mix of electricity generation (years)	1.5	0.6	3.6
Ratio of soil carbon loss to gain by restoration (TARGET ratio (Natural Resources Wales) < 1.0)	No gains!	No gains!	No gains!
Ratio of CO ₂ eq. emissions to power generation (g / kWh) (TARGET ratio by 2030 (electricity generation) < 50 g /kWh)	43	27	65





Click here to return to Input data Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix. Click here to return to Instructions



degraded bogs

DOC & POC

Data used in barchart of carbon payback time using



	Exp.	/
Turbine life	49830	
Backup	48128	48
Bog plants	1057	6
Soil organic carbon	59102	29
DOC & POC	0	
Management of forestry	0	
Improved degraded bogs	0	
Improved felled forestry	0	
Restored borrow pits	0	
Stop drainage of foundations	0	

Greenhouse gas emissions	Carbon payback time (months)					
	Exp.	Min.	Max.	Exp.	Min.	Max.
Turbine life	49830	43	0	6	0	0
Backup	48128	48128	0	6	7	0
Bog plants	1057	689	730	0	0	0
Soil organic carbon	59102	29631	140250	7	4	13
DOC & POC	0	0	0	0	0	0
Management of forestry	0	0	0	0	0	0
Improved degraded bogs	0	0	0	0	0	0
Improved felled forestry	0	0	0	0	0	0
Restored borrow pits	0	0	0	0	0	0
Stop drainage of foundations	0	0	0	0	0	0
	158117			18		

Greenhouse gas emissions		Carbon pay	/back time ((montns)		
	Exp.	Min.	Max.	Exp.	Min.	Max.
Turbine life	49830	43	0	6	0	0
Backup	48128	48128	0	6	7	0
Bog plants	1057	689	730	0	0	0
Soil organic carbon	59102	29631	140250	7	4	13
DOC & POC	0	0	0	0	0	0
Management of forestry	0	0	0	0	0	0
Improved degraded bogs	0	0	0	0	0	0
Improved felled forestry	0	0	0	0	0	0
Restored borrow pits	0	0	0	0	0	0
Stop drainage of foundations	0	0	0	0	0	0
	158117			18		

fossil-fuel mix as counterfactual

<i>lin</i>	Max	
43	0	
128	0	
89	730	
631	140250	
0	0	
0	0	
0	0	
0	0	
0	0	
0	0	

Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Windfarm CO₂ emission saving Note: The total emission savings are given by estimating the total possible electrical output of the windfarr multiplied by the emission factor for the counterfactual case (coal-fire generation and electricity from grid)

Click here to move to Payback Time Click here

		Total	-	Foi	restry Are	ea 1	Foi	restry Are	ea 2	For	restry Are	ea 3	Foi	estry Are	ea 4	Fo	estry Are	ea 5
Values taken from input sheet	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Ехр	Min	Max	Exp	Min	Max
Power Generation Characteristics																		
No. of turbines	19	19	19	0	0	0	0	0	0	0		0	0	0	0			0
Power rating of turbines (turbine capacity) (MW)	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3	3.3
Power of windfarm (MW)	62.7	62.7	62.7	0	0	0	0	0	0	0		0	0	0	0			0
Estimated downtime for maintenance etc (%)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Counterfactual emission factors																		
Coal-fired plant emission factor (t CO ₂ MWh ⁻¹)	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907	0.907
Grid-mix emission factor (t CO ₂ MWh ⁻¹)	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454	0.454
Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹)	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701

Calculation of capacity factor	1	Direct input of capacity factor							
		Exp	Min	Max					
Entered capacity factor (%)		27	21.8	33.63					
Parameters			Slope (a)			Intercept (b)			
Partial power curves for different turbines		Exp	Min	Max	Exp	Min	Max		
User-defined		0.0	0.0	0.0	0.0	0.0	0.0		
Vestas 2.0 MW Optispeed C2		1392.5	1392.5	1392.5	-4291.9	-4291.9	-4291.9		

	•	Total		Fo	restry Are	ea 1	Fo	restry Are	ea 2	Foi	restry Ar	ea 3	Fo	restry Are	ea 4	Foi	estry Ar	ea 5
Calculation of capacity factor from forestry management	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Ехр	Min	Max	Exp	Min	Max	Ехр	Min	Max
Wind speed ratio calculated in 7d				########	#######	#######	########	#######	#######	#######	#######	#######	#######	*****	*****	#######	########	#######
Average site windspeed (m s ⁻¹)	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0
Annual theoretical energy output	28908	28908	28908	28908	28908	28908	28908	28908	28908	28908	28908	28908		28908	28908	28908	28908	28908
from turbine (MW turbine ⁻¹ yr ⁻¹)	20300	20300	20300	20300	20000	20300	20000	20000	20300	20000	20000	20300	20300	20300	20300	20300	20000	20300
Power curve				User- defined	Partial power curves for different turbines													
(Power curve code)				1	0	0	0	0	0	0	0	0		0	0	0	0	0
Slope (a)				0	Exp		Exp	Exp	Exp	Exp	Exp							
Intercept (b)				0	Exp													
Annual power output from an individual turbine (MW turbine ⁻¹ yr ⁻¹)					****	########	****	"""""	########	########	########	########		<i></i>	****	<i></i>	########	#######
Calculated capacity factor (%)				#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######
		Total		Fo	restry Are	ea 1	Fo	restry Are	ea 2	Foi	restry Ar	ea 3	Fo	restry Ar	ea 4	Foi	estry Ar	ea 5
Calculation of annual energy outp	ut from w	vind farm																
Direct input of capacity factor																		
Capacity factor(%)	27	22	34	27	22	34	27	22	34	27	22	34	27	22	34	27	22	34
Annual energy output from windfarm (MW yr ⁻¹)	148298	119737	184713	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
RESULTS		Total			Area 1			Area 2			Area 3			Area 4			Area 5	
Windfarm CO ₂ emission saving		lotai			Alcui	l I			1						1		Alcus	1
over																		
coal-fired electricity generation (tCO ₂ yr ⁻¹)	134506	108601	167535	0	0	0	0	0	0	0	0	0		о	0	0	0	0
grid-mix of electricity generation (tCO ₂ yr ⁻¹)	67327	54360.6	83859.9	0	0	0	0	0	0	0	0	0		0	0	0	0	0
fossil fuel - mix of electricity generation (tCO ₂ yr ⁻¹)	103957	83935.6	129484	0	0	0	0	0	0	0	0	0		0	0	0	0	0

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Windfarm CO, emission saving Note: The total emission savings are given by estimating the total possible electrical output of the windfarm multiplied by the emission factor for the counterfactual case (coal-fire generation and electricity from grid)

turbine life ing the emis isplacing ele	sions due to	turbine life			
Calcu	late wrt in capacity	stalled			
Exp	Min	Max	í		
0	0	0			
ife from e	energy ou	tput			
2616	2616	2616			
19	19	19			
49700	49700	49700			
Exp	Total Min	Max		truction A Min	Are
750	500	750	750	500	
0.173	0.173	0.173	0.173	0.173	C
130	0/	130	130	07	
49830	49787	49830			
	urbine life	e (eg.			
ng)					
4	6	4			
9	11	7			
6	7	5			
Click here			-		
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Construction Area 3 Exp Min Max

0 0.173 0 0 0.173 0 0 0.173 0

Max Min

a 1 Max

Exp

Construction Area 5 Exp Min Max

0 0.173 0

0 0 0.173 0.173 0 0

Exp Min Max

construction, decomissioning) is calculated by comparing the ensistend auto-with carbon-savings achieved by the windfarm while displacing electricity generated from coal-lifed capacity or grid-mix.

Version 1.1-3 March 2008

CONCRETE	Concrete type	ECO ₂ (kgCO ₂ km ²)	ECO, BgCOytonne)	
Binding, mass fill, strip footings, mass foundations	GEN1 70 mm (CEM I only)	173	75	
Trench foundations ¹	GEN1 120 mm * (CEM I only)	154	80	
Reinforced Foundations	RC30 70 mm *** (CEM I only)	318	132	
Ground floors 1	RC35 70 mm ** (CEM I only)	315	133	
Structural in situ foors, superstructure, walls, tusements	RC40 70 mm *** (CEM I only)	372	153	
High strength concrete ¹	RC50 70mm *** (CEM I only)	436	176	
Dense concrete aggregate block ²	Precast block	147	75	
Aerated concrete block 2	Precast block	121	240	
Generic lightweight aggregate block	Precast block	168	120	
TIMBER		ECO, (kgCOyler)	ECO, (kgCOylonne)	
Timber, UK Sawn Hantwood		369	470	
Timber, UK Sawn Softwood *		185	440	
Plywood *		398	750	
STEEL		ECO, (kgCO2/m ²)	ECO, (kgCO,/tonne)	
OK Produced Structural Steel Sections		15,313	1,932	

includes 25 kg/m² steel reinforcement
 includes 30 kg/m² steel reinforcement
 includes 100 kg/m² steel reinforcement

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 1
 The ECC2 Sparse for GEN 1, RCI2H0 and RC45/50 were derived using industry agreed representative Sparse for unematitions materials, aggraphies, retritorement, administer and an appropriate Spars for 2. BRE Environmental Profess database, Buikding Research Edatabatenet (BRE), 2000

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Emissions due to backup power generation

Note: CO₂ loss due to back up is calculated from the extra capacity required for backup of the windfarm given in the input data.

	Expected	Minimum	Maximum
Reserve capacity required for backup			
No. of turbines	19	19	19
Power rating of turbines (turbine capacity) (MW)	3.3	3.3	3.3
Power of wind farm (MW h ⁻¹)	62.7	62.7	62.7
Rated capacity (MW yr ⁻¹)	549252	549252	549252
Extra capacity required for backup (%)	5	0	5
Additional emissions due to reduced thermal efficiency of the reserve generation (%)	10	10	10
Reserve capacity (MWh yr ¹)	2746	0	2746

Carbon dioxide emissions due to backup power			
generation			
Coal-fired plant emission factor (t CO ₂ MWh ⁻¹)	0.907	0.907	0.907
Grid-mix emission factor (t CO ₂ MWh ⁻¹)	0.454	0.454	0.454
Fossil fuel- mix emission factor (t CO ₂ MWh ⁻¹)	0.701	0.701	0.701
Lifetime of windfarm (years)	25	25	25
Annual emissions due to backup from			
coal-fired electricity generation (tCO ₂ yr ⁻¹)	2491	0	2491
grid-mix of electricity generation (tCO ₂ yr ⁻¹)	1247	0	1247
fossil fuel - mix of electricity generation (tCO ₂ yr ⁻¹)	1925	0	1925

RESULTS			
Fotal emissions due to backup from			
coal-fired electricity generation (tCO ₂)	62271	0	62271
grid-mix of electricity generation (tCO ₂)	31170	0	31170
fossil fuel - mix of electricity generation (tCO2)	48128	0	48128 -
Additional CO ₂ payback time of windfarm due to backup			
coal-fired electricity generation (months)	6	0	4
grid-mix of electricity generation (months)	6	0	4
fossil fuel - mix of electricity generation (months)	6	0	4

Click here to move to Payback Time Click here Click here to return to Instructions Click here

Emissions due to backup power generation

Note: CO2 loss due to back up is calculated from the extra capacity required for backup of the windfarm given in the input data.

Note: Wind generated electricity is inherently variable, providing unique challenges to the electricity generating industry for provision of a supply to meet consumer demand (Netz, 2004). Backup power is required to accompany wind generation to stabilise the supply to the consumer. This backup power will usually be obtained from a fossil fuel source. At a high level of wind power penetration in the overall generating mix, and with current grid management techniques, the capacity for fossil fuel backup may become strained because it is being used to balance the fluctuating consumer demand with a variable and highly unpredictable output from wind turbines (White, 2007). The Carbon Trust (Carbon Trust/DTI, 2004) concluded that increasing levels of intermittent generation do not present major technical issues at the percentages of renewables expected by 2010 and 2020, but the UK renewables target at the time of that report was only 20%. When national reliance on wind power is low (less than ~20%), the additional fossil fuel generated power requirement can be considered to be insignificant and may be obtained from within the spare generating capacity of other power sectors (Dale et al, 2004). However, as the national supply from wind power increases above 20%, without improvements in grid management techniques, emissions due to backup power generation may become more significant. The extra capacity needed for backup power generation is currently estimated to be 5% of the rated capacity of the wind plant if wind power contributes more than 20% to the national grid (Dale et al 2004). Moving towards the SG target of 50% electricity generation from renewable sources, more short-term capacity may be required in terms of pumped-storage hydro-generated power, or a better mix of offshore and onshore wind generating capacity. Grid management techniques are anticipated to reduce this extra capacity, with improved demand side management, smart meters, grid reinforcement and other developments. However, given current grid management techniques, it is suggested that 5% extra capacity should be assumed for backup power generation if wind power contributes more than 20% to the national grid. At lower contributions, the extra capacity required for backup should be assumed to be zero. These assumptions should be revisited as technology improves.

Assumption: Backup assumed to be by fossil-fuel-mix of electricity generation. Note that hydroelectricity may also be used for backup, so this assumption may make the value for backup generation too high. These assumptions should be revisited as technology develops.

Emissions due to loss of bog plants

Note: Annual C fixation by the site is calculated by multiplying area of the windfarm by the annual C accumulation due to bog plant fixation

	Expected	Minimum	Maximum
Area where carbon accumulation by bog plants is lost			
Total area of land lost due to windfarm construction (m ²)	158791	144975	176086
Total area affected by drainage due to windfarm construction (m ⁻²)	253133	165451	347902
Total area where fixation by plants is lost (m ²)	411923	310426	523988
Total loss of carbon accumulation			
Carbon accumulation in undrained peats (tC ha ⁻¹ yr ⁻¹)	0.25	0.12	0.31
Lifetime of windfarm (years)	25	25	25
Time required for regeneration of bog plants after restoration (years)	3	2	5
Carbon accumulation up to time of restoration $(tCO_2 \text{ eq. ha}^{-1})$	26	12	34
RESULTS			
Total loss of carbon accumulation by bog plants			
Total area where fixation by plants is lost (ha)	41	31	52
Carbon accumulation over lifetime of windfarm (tCO ₂ eq. ha ⁻¹)	26	12	34
Total loss of carbon fixation by plants at the site (t CO ₂)	1057	369	1787
Additional CO ₂ payback time of windfarm due to loss of CO2 fixing	g potential		
coal-fired electricity generation (months)	0	0	0
grid-mix of electricity generation (months)	0	0	0
fossil fuel - mix of electricity generation (months)	0	0	0

Click here to move to Payback Time Click here

Emissions due to loss of bog plants

Note: Annual C fixation by the site is calculated by multiplying area of the windfarm by the annual C accumulation due to bog plant fixation

Assumptions: 1. Bog plants are 100% lost from the area where peat is removed for construction. 2. Bog plants are 100% lost from the area where peat is drained. 3. The recovery of carbon accumulation by plants on restoration of land is as given in inputs.

Emissions due to loss of soil organic carbon

Note: Loss of C stored in peatland is estimated from % site lost by peat removal (sheet 5a), CO₂ loss from removed peat (sheet 5b), % site affected by drainage (sheet 5c), and the CO2 loss from drained peat (sheet 5d).

		Expected result	Minimum result	Maximum result
	CO ₂ loss due to windfarm construction			
ck	CO_2 loss from removed peat (t CO_2 equiv)	40778	21772	112110
k	CO ₂ loss from drained peat (t CO ₂ equiv)	18323	7699	87241
	RESULTS			
	Total CO_2 loss from peat (removed + drained) (t CO_2 equiv)	59102	29471	199351
	Additional CO ₂ payback time of windfarm due to loss of soil CO2			
	coal-fired electricity generation (months)	5	3	14
	grid-mix of electricity generation (months)	11	7	29
	fossil fuel - mix of electricity generation (months)	7	4	18

Click here to move to Payback Time

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Emissions due to loss of soil organic carbon

Note: Loss of C stored in peatland is estimated from % site lost by peat removal (sheet 5a), CO₂ loss from removed peat (sheet 5b), % site affected by drainage (sheet 5c), and the CO2 loss from drained peat (sheet 5d).

Volume of Peat Removed			
Note: % site lost by peat removal is estimated from peat removed in borrow pits, turbine foundations, hard- standing and access tracks.			
If peat is removed for any other reason, this must be added in as additional peat excavated in the core input sheet.			
Peat removed from borrow pits		Total	
real removed from borrow pits	Exp	Min	Max
		I VIIII	INICAA
Number of borrow pits	1	1	1
	1 100	1 50	1 150
Number of borrow pits Average length of pits (m) Average width of pits (m)	1	1	1
Average length of pits (m)	1 100	1 50	1 150
Average length of pits (m) Average width of pits (m)	1 100 100	1 50	1 150 150

Volume of peat removed from borrow pits																	
(m ³)	10500	2500	24750														
Peat removed from turbine foundations		Total			truction			truction	• • • • • • • • • • • • • • • • • • •		struction			struction			truction
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min
Method used to calculate CO ₂ loss from	Enter det	ailed info	rmation														
foundations			mation														
Calculation method code		2															
No. of turbines	19	19	19	19	19	19	0	0	0	0	0	0	0	0	0	0	0
Length at surface (m)				28	25	28	0	0	0	0	0	0	0	0	0	0	0
Width at surface (m)				28	25	28	0	0	0	0	0	0	0	0	0	0	0
Length at bottom (m)				25	25	25	0	0	0	0	0	0	0	0	0	0	0
Width at bottom (m)				25	25	25	0	0	0	0	0	0	0	0	0	0	0
Depth of foundations (m)				0	0	0	0	0	0	0	0	0	0	0	0	0	0
Area of land lost in hard-standing (m ²)	13241	11875	13240.63	13241	11875	13241	0	0	0	0	0	0	0	0	0	0	0
Volume of peat removed from foundation	0070 400	0500.5	0070 400	0070 400	0500 5	0070 400	~	<u> </u>		<u> </u>	_	<u>^</u>	<u> </u>	_			<u> </u>
area (m ³)	3972.188	3562.5	3972.188	3972.188	3562.5	3972.188	0	0	0	0	0	0	0	0	0	0	0
										_							
Peat removed from hard-standing			1														

Area 5 Max

Peat removed from hard-standing																		
Method used to calculate CO ₂ loss from	Entor dat	tailed info	motion															
foundations	Enter der		malion															
Calculation method code		2																
No. of turbines	19	19	19	19	19	19	0	0	0	0	0	0	0	0		0	0	0
Length at surface (m)				50	50	50	0	0	0	0	0	0	0	0		0	0	0
Width at surface (m)				25	25	25	0	0	0	0	0	0	0	0		0	0	0
Length at bottom (m)				50	50	50	0	0	0	0	0	0	0	0		0	0	0
Width at bottom (m)				25	25	25	0	0	0	0	0	0	0	0		0	0	0
Depth of hardstanding (m)				0	0.3	0.3	0	0	0	0	0	0	0	0	0	0	0	0
Area of land lost in hard-standing (m ²)	23750	23750	23750	23750	23750	23750	0	0	0	0	0	0	0	0		0	0	0
Volume of peat removed from	74.05	7405	7405	7405	7405	7405	0	0	~	~	0	~	0	0		~	0	~
hardstandingarea (m ³)	7125	7125	7125	7125	7125	7125	0	0	0	0	0	0	0	0		0	0	0

		Total	
Peat removed from access tracks	Exp	Min	Max
Floating roads	•		
Length of access track that is floating road			
(m)	1900	1800	2000
Floating road width (m)	6	6	6
Floating road depth (m)	0.5	0.5	0.5
Area of land lost in floating roads (m ²)	11400	10800	12000
Volume of peat removed for floating roads	5700	5400	6000
Excavated roads			
Length of access track that is excavated			
road (m)	11000	10500	11500
Excavated road width (m)	6	6	6
Average depth of peat excavated for road			
(m)	0.58	0.5	0.7
Area of land lost in excavated roads (m ²)	66000	63000	69000
Volume of peat removed for excavated			
roads	38280	31500	48300
Rock-filled roads			
Length of access track that is rock filled road			
(m)	0	0	0
Rock filled road width (m)	0	0	0
Rock filled road depth (m)	0	0	0
Area of land lost in excavated roads (m ²)	0	0	0
	_		_
Volume of peat removed for rock-filled roads	0	0	0
Total area of land lost in access tracks (m ²)	77400	73800	81000
Total volume of peat removed due to access	77400	13000	01000
tracks (m ³)	43980	36900	54300
	43900	30900	34300
Additional peat excavated -			
(not already accounted for above)			
Volume of additional peat excavated (m ³)	20258	19500	21000
Area of additional peat excavated (m ²)	34400	33050	35595
	5	30000	30000
RESULTS		Total	
	Exp	Min	Мах
Total volume of peat removed (m ³) due to			
windfarm construction	85835.2	69587.5	111147
Total area of land lost due to windfarm			
construction (m ²)	158791	144975	176086

Click here to move to 5b. CO2 loss from removed peat



Click here to move to Payback Time



Volume of Peat Removed Note: % site lost by peat removal is estimated from peat removed in borrow pits, turbine foundations, hard-standing and access tracks.

If peat is removed for any other reason, this must be added in to the volume of peat removed, area of land lost and % site lost at the bottom of this worksheet.

CO₂ loss from removed peats

Ch

Note: If peat is treated in such a way that it is permanently restored, so that less than 100% of the C is lost to the atmosphere, a lower percentage can be entered in cell C10

	Expected	Minimum	Maximum
CO ₂ loss from removed peat			
C Content of dry peat (% by weight)	55	49	62
Dry soil bulk density (g cm ⁻³)	0.25	0.20	0.45
% C contained in removed peat that is lost as CO ₂	100	100	100 🗲
Total volume of peat removed (m ³) due to windfarm construction	85835	69588	111147
CO_2 loss from removed peat (t CO_2)	43279	25007	113714
CO ₂ loss from undrained peat left in situ			
Total area of land lost due to windfarm construction (ha)	16	14	18
CO_2 loss from undrained peat left in situ (t CO_2 ha ⁻¹)	157	223	91
CO_2 loss from undrained peat left in situ (t CO_2)	2501	3235	1604
CO ₂ loss attributable to peat removal only	1	1	
CO_2 loss from removed peat (t CO_2)	43279	25007	113714
CO_2 loss from undrained peat left in situ (t CO_2)	2501	3235	1604
RESULTS			
CO ₂ loss attributable to peat removal only (t CO ₂)	40778	21772	112110

Assumption: If peat is not restored, 100% of the carbon contained in the removed peat is lost as CO_2

Click here to move to 5. Loss of soil CO_2

Click here to move to Payback Time

CO₂ loss from removed peats

Note: If peat is treated in such a way that it is permanently restored, so that less than 100% of the C is lost to the atmosphere, a lower percentage can be entered in cell C10

Click here

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Volume of peat drained Note: Extent of site affected by drainage is calculated assuming an average extent of drainage around each drainage feature as given in the input data.

Extent of drainage around each metre		Total	
of drainage ditch	Exp	Min	Max
Average extent of drainage around drainage features at site (m)	8	5	10

Peat affected by drainage around		Total	
borrow pits	Exp	Min	Max
Number of borrow pits	1	1	1
Average length of pits (m)	100	50	150
Average width of pits (m)	100	50	150
Average depth of peat removed from pit (m)	1.1	1.0	1.1
Area affected by drainage per borrow pit (m ²)	3225	1100	6400
Total area affected by drainage around borrowpits (m ²)	3225	1100	6400
Total volume affected by drainage around borrowpits (m ³)	1693	550	3520

Peat affected by drainage around		Total		Cons	truction A	Area 1	Cons	truction	Area 2	Cons	truction A	Area 3	Construction Area 4			Construction Area 5		
turbine foundation and hardstanding	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
No. of turbines	19	19	19	19	19	19	0	0	0	0	0	0	0	0	0	0	0	0
Average length of turbine foundations at				25	25	25		0	0	0	0	0	0	0	0	0	0	0
base (m)				20	20	20		0	0	U		U	0	U	U	U	U	U
Average width of turbine foundations at				25	25	25		0	0	0	0	0	0	0	0	0	0	0
base(m)				20	20	20		0	0	U		U	0	0	0	U	U	U U
Average depth of peat removed from				0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
turbine foundations (m)				0.0	0.0	0.5		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Average length of hard-standing at base				50	50	50		0	0	0	0	0	0	0	0	0	0	0
(m)				50	50	50		0	0			U	0	0	0			v
Average width of hard-standing at base				25	25	25		0	0	0	0	0	0	0	0	0	0	0
(m)				20	20	20		0	0	U		U	0	0	0	U	U	v
Average depth of peat removed from				0.6	0.6	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
hard-standing (m)				0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Maximum depth of drains (m)				0.6	0.6	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total length of foundation and				75	75	75		0	0	0	0	0	0	0	0	0	0	0
hardstanding (m)				15	15	75		0	0			U	0	0	0			v
Total width of foundation and				50	50	50		0	0	0	0	0	0	0	0	0	0	0
hardstanding (m)				50		50		Ŭ	Ŭ			U	0	Ŭ	Ŭ			Ŭ
Area affected by drainage of foundation	2100	1350	2900	2100	1350	2900		0	0	0	0	0	0	0	0	0	0	0
and hardstanding area (m ²)	2100	1550	2900	2100	1550	2300	0	0	0	U		U	0	0	0	U	U	U
Total area affected by drainage of	39900	25650	55100	39900	25650	55100		0	0	0	0	0	0	0	0	0	0	0
foundation and hardstanding area (m ²)	39900	20000	55100	39900	20000	00100		0	0	U	U	U	0	U	U	U	U	U
Total volume affected by drainage of	44070	7005	40500	44070	7005	40500		_				_	_					
foundation and hardstanding area (m ³)	11970	7695	16530	11970	7695	16530	0	0	0	0	0	0	0	0	0	0	0	0

Peat affected by drainage of access	_	Total	
tracks	Exp	Min	Max
Floating roads			
Length of floating road that is drained (m)	1900	1900	1900
Floating road width (m)	6.0	6.0	6.0
Average depth of drains associated with	0.0	0.0	0.0
floating roads (m)	0.50	0.50	0.50
Area affected by drainage of floating			
roads (m ²)	39900	30400	49400
Volume affected by drainage of floating			
roads (m ³)	9975	7600	12350
Excavated Road			
Length of access track that is excavated	11000	10500	11500
road (m)	11000	10500	11500
Excavated road width (m)	6	6	6
Average depth of peat excavated for	0.6	0.5	0.7
road (m)	0.0	0.0	0.1
Area affected by drainage of excavated	165000	105000	230000
roads (m ²)			
Volume affected by drainage of	47850	26250	80500
excavated roads (m ³)			
Rock-filled roads			
Length of rock filled road that is drained (m)	0	0	0
Rock filled road width (m)	0	0	0
Average depth of drains associated with	-	-	-
rock filled roads (m)	0.0	0.0	0.0
Area affected by drainage of rock-filled			
roads (m ²)	0	0	0
Volume affected by drainage of rock-			
filled roads (m ²)	0	0	0
Total area affected by drainage of	004000	135400	070400
access track (m ²)	204900	135400	279400
Total volume affected by drainage of	57825	33850	92850
access track (m ³)	57625	33650	92650
Peat affected by drainage of cable		Total	
trenches	Exp	Min	Max
Length of any cable trench on peat that			
does not follow access tracks and is lined with a permeable medium (eg.	0	0	0
sand) (m)			
Average depth of peat cut for cable			
trenches (m)	0.0	0.0	0.0
Total area affected by drainage of cable			
	0	0	0
, ,	0	Ū	Ũ
trenches (m ²) Total volume affected by drainage of	0.00	0.00	0.00

Drainage around additional peat		Total		
excavated	Exp	Min	Max	
Volume of additional peat excavated (m ³)	20258.0	19500.0	21000.0	
Area of additional peat excavated (m ²)	34400.0	33050.0	35595.0	
Average depth of excavated peat (m) Radius of area excavated (m) Radius of excavated and drained area	1 105	1 103	1 106 ·	Assumption: Area excavate assumed to be a circle
(m)	112	108	116	
Total area affected by drainage (m ²)	5108	3301	7002]
Total volume affected by drainage (m ³)	3007.98	1808.28	4449.21	

RESULTS		Total	
RESOLIS	Exp	Min	Max
Total area affected by drainage due to windfarm (m ²)	253133	165451	347902
Total volume affected by drainage due to windfarm (m ³)	74496.1	43903.28	117349.2

Click here to move to 5d. CO2 loss from Click here drained peat

Click here to move to Payback Time Click here



Volume of peat drained Note: Extent of site affected by drainage is calculated assuming an average extent of drainage around each drainage feature as given in the input data.

CO₂ loss due to drainage Note: Note, CO₂ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included becaus it is the established approach, although it contains no site detail. The new equations have been derived directly from experimental data for acid bogs and fens (see Nayak et al, 2008 - Final report).

Click here to move to 5. Loss of soil CO2 lick here Click here to move to Payback Time Click here

	Expected	Minimum	Maximum
Drained Land	•		
Total area affected by drainage due to wind farm construction (ha)	25	17	35
0	No	No	No
Will the habitat of the site be restored on decommissioning?	No	No	No

Calculations of C Loss from Drained Land if Site is NOT Restored after Decommissioning

Check	Total volume affected by drainage due to wind farm (m ³)	74496	43903	117349	
	C Content of dry peat (% by weight)	55	49	62	
	Dry soil bulk density (g cm ⁻³)	0.25	0.20	0.45	
	Total GHG emissions from Drained Land (t CO ₂ equiv.)	37562	15777	120059	Assumption: Losses of GHG from drained and undrained land have the
	Total GHG Emissions from Undrained Land (t CO ₂ equiv.)	19239	8078	32818 .	same proportion throughout the
					emission period

Calculations of C loss from Drained Land if Site IS Restored after Decommissioning

	1. Losses if Land is Drained				
	Flooded period (days year ⁻¹)	0	0	0	Assumption: The drained soil is not flooded at any time of the year.
	Lifetime of windfarm (years)	25	25	25	noodod at any ante of the year.
	Time required for regeneration of bog plants after restoration	3	2	5	
	(years)	Ŭ		, , , , , , , , , , , , , , , , , , ,	
	Methane Emissions from Drained Land				
Check	Rate of methane emission in drained soil ((t CH_4 -C) ha ⁻¹ yr ⁻¹)	0.002	0.006	-0.015	Note:Conversion = $(23 \times 16/12) =$ 30.67 CO ₂ equiv. (CH ₄ -C) ⁻¹
	Conversion factor: CH ₄ -C to CO ₂ equivalents	30.67	30.67	30.67	
	CH_4 emissions from drained land (t CO_2 equiv.)	46	88	-484	
	Carbon Dioxide Emissions from Drained Land				
Check	Rate of carbon dioxide emission in drained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	10.92	15.94	11.57	
	CO ₂ emissions from drained land (t CO ₂)	7737	7122	12076	
	Total GHG emissions from Drained Land (t CO ₂ equiv.)	7784	7211	11592]

2. Losses if Land is Undrained

Γ

	Flooded period (days year ⁻¹)	178	178	178	
	Lifetime of windfarm (years)	25	25	25	
	Time required for regeneration of bog plants after restoration (years)	3	2	5	
	Methane Emissions from Undrained Land				
Check	Rate of methane emission in undrained soil ((t CH ₄ -C) ha ⁻¹ yr ⁻¹)	0.00	0.01	0.02	
	Conversion factor: CH ₄ -C to CO ₂ equivalents	30.67	30.67	30.67	Note:Conversion = $(23 \times 16/12) =$
	CH_4 emissions from undrained land (t CO_2 equiv.)	23	43	304	30.67 CO ₂ equiv. (CH ₄ -C) ⁻¹
	Carbon Dioxide Emissions from Undrained Land				
Check	Rate of carbon dioxide emission in undrained soil (t CO_2 ha ⁻¹ yr ⁻¹)	10.92	15.94	5.36	
	CO_2 emissions from undrained land (t CO_2)	3964	3649	2865	
	Total GHG Emissions from Undrained Land (t CO ₂ equiv.)	3987	3692	3169	

3. CO₂ Losses due to Drainage

RESULTS	19239	8078	32818
Total GHG emissions from drained land (t CO_2 equiv.)	37562	15777	120059
Total GHG emissions from undrained land (t CO_2 equiv.)	19239	8078	32818

Click here to move to 5. Loss of soil CO_2

Click here to move to Payback Time



CO₂ loss due to drainage

Note: Note, CO₂ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been derived directly from experimental data for acid bogs and fens (see Nayak et al, 2008 - Final report).

Emission rates from soils

Note: Note, CO₂ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).

Click here to move to Payback Time

Click here to move to 5d. Click here

	d = Acid Bog				
Calculations following IPCC default methodology	Expected	Minimum	Maximum		
mission characteristics of acid bogs (IPCC, 1997)	178	178	178	7	
looded period (days year ⁻¹) .nnual rate of methane emission (t CH₄-C ha ⁻¹ yr ⁻¹)					
	0.04015	0.04015	0.04015		
nnual rate of carbon dioxide emission (t CO ₂ ha ⁻¹ yr ⁻¹)	35.2	35.2	35.2		
mission characteristics of fens (IPCC, 1997)		1	•	_	Assumption: The period of flooding is taken to be 178 days yr ⁻¹ for acid bogs
looded period (days year ⁻¹)	169	169	169		and 169 days yr ⁻¹ based on the monthly mean temperature and the
nnual rate of methane emission (t CH_4 -C ha ⁻¹ yr ⁻¹)	0.219	0.219	0.219		lengths of inundation (IPCC, 1997, Revised 1996 IPCC guidelines for national greenhouse gas
nnual rate of carbon dioxide emission (t CO ₂ ha ⁻¹ yr ⁻¹)	35.2	35.2	35.2	」 ∕	inventories, Vol 3, table 5-13)
elected emission characteristics (IPCC, 1997)				_/	Assumption: The CH₄ emission rate provided for acid bogs is 11 (1-38) mg
looded period (days year ⁻¹)	178	178	178	7	CH ₄ -C m ⁻² day ⁻¹ x 365 days; and for fens is 60 (21-162) mg CH ₄ -C m ⁻² day ⁻¹
nnual rate of methane emission (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.04015	0.04015	0.04015	•	x 365 days (Aselmann & Crutzen ,1989.
nnual rate of carbon dioxide emission (t CO_2 ha ⁻¹ yr ⁻¹)	35.2	35.2	35.2		J.Atm.Chem. 8, 307-358)
Calculations following ECOSSE based methodology		-	-		Assumption: CO_2 emissions on drainage of organic soils for upland crops (e.g., grain, vegetables) are 3.667X9.6 (7.9-11.3) t CO_2 ha ⁻¹ yr ⁻¹ in
otal area affected by drainage due to wind farm construction (ha)	25	17	35	٦	temperate climates (Armentano and Menges,
otal volume affected by drainage due to wind farm construction (m ³)	74496	43903	117349		1986. J. Ecol. 74, 755-774).
				_	Note: Carbon dioxide emissions from acid bogs. Equation derived by regression analysis again measurements (Nayak et al, 2009). The equation derived was
toil Characteristics that Determine Emission Rates	7.5	11.2	3.9	7	$R_{002} = (3.667/1000) \times ((6700 \times exp(-0.26 \times exp(-0.0515 \times ((Wx100)-50)))) + ((72.54 \times Where R_{002} is the annual rate of CO2 emissions (t CO2 (ha)-1 yr-1),$
	1.0		0.0		T = average annual peat temperature (°C) and W is the water table depth (m).
verage water table depth at site (m)	0.30	0.40	0.20	,	The equation shows a significant correlation with measurements (r ² =0.53 P > 0.05).
verage water table depth of drained land (m)	0.30	0.40	0.34	」 /	Evaluation against 29 independent experiments shows a significant association (r ² + 0.21; P>0. an average error of 3023 t CO ₂ ha ⁻¹ yr ⁻¹ which is non-significant (P<0.05) (Smith et al, 1997).
nnual Emission Rates following site specific methodology					
cid bogs] /	measurements (Nayak et al, 2009). The equation derived was $R_{CH4} = (1/1000) \times (500 \times \exp(-0.1234 \times (W \times 100)) + ((3.529 \times 7) - 36.67))$
ate of carbon dioxide emission in drained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	10.92	15.94	11.57		where R _{CH4} is the annual rate of CH ₄ emissions (t CH ₄ -C (ha) ⁻¹ yr ⁻¹),
ate of carbon dioxide emission in undrained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	10.92	15.94	5.36		T = average annual air temperature (°C) and W is the water table depth (m).
Rate of methane emission in drained soil ((t CH_4 -C) ha ⁻¹ yr ⁻¹)	0.002	0.006	-0.015	٦_	The equation shows a significant correlation with measurements (r ² = 0.54, P > 0.05).
Rate of methane emission in undrained soil ((t CH_4 -C) ha ⁻¹ yr ⁻¹)	0.00	0.01	0.02		 Evaluation against 7 independent experiments shows a significant association (r² • 0.81; P>0.0 average error of 27 t CH₄-C ha⁻¹ yr⁻¹ (significance not defined due to lack of replicates - Smith et
ens				_	
Rate of carbon dioxide emission in drained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	31.94	47.57	35.50		Note: Carbon dioxide emissions from fens. Equation derived by regression analysis against 44
Rate of carbon dioxide emission in undrained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	31.94	47.57	14.29	1	measurements (Nayak et al, 2009). The equation derived was
Rate of methane emission in drained soil ((t CH ₄ -C) ha ⁻¹ yr ⁻¹)	0.026	0.009	0.014	1	$R_{002} = (3.667/1000) \times (16244 \times exp(-0.175 \times exp(-0.073 \times ((Wx100)-50)))+(153.23 \times 7))$ where R_{002} is the annual rate of CO ₂ emissions (t CO ₂ (ha) ⁻¹ yr ⁻¹).
ate of methane emission in undrained soil ((t CH ₄ -C) ha ⁻¹ yr ⁻¹)	0.03	0.01	0.07	K	T = average annual peat temperature (°C) and W is the water table depth (m).
alested emission observatoristics following site specific methods by			•	_ \	The equation shows a significant correlation with measurements ($r^2 = 0.42$, $P > 0.05$). Evaluation against 18 independent experiments shows a significant association ($r^2 = 0.56$; $P > 0$.
elected emission characteristics following site specific methodolog tate of carbon dioxide emission in drained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	10.92	15.94	11.57	¬ ∖	an average error of 2108 t CO ₂ harl yr ⁻¹ (significance not defined due to lack of replicates-Smith
tate of carbon dioxide emission in undrained soil (t CO_2 ha ⁻¹ yr ⁻¹)	10.92	15.94	5.36		Note: Methane emissions from fens. Equation derived by regression analysis against experimer from 35 measurements (Nayak et al, 2009). The equation derived was
Rate of methane emission in drained soil ((t CH_4 -C) ha ⁻¹ yr ⁻¹)	0.002	0.006	-0.015	\dashv \land	$R_{OH4} = (1/1000) \times (-10+563.62 \times \exp(-0.097 \times (W \times 100)) + (0.662 \times T))$
tate of methane emission in undrained soil (($t CH_4 C$) ha ⁻¹ yr ⁻¹)	0.002	0.00	0.02		where R_{CH4} is the annual rate of CH ₄ emissions (t CH ₄ -C (ha) ⁻¹ yr ⁻¹), T = average annual air temperature (°C) and We have the sheat begin to be the first of the sheat of
			1	_	W is the water table depth (m). The equation shows a significant correlation with measurements (r ² = 0.41, P > 0.05). Evaluation against 7 independent experiments shows a significant association (r ² = 0.69; P > 0.09 an average error of 164 t CH ₄ -C ha ⁻¹ yr ⁻¹ (significance not defined due to lack of replicate-Smith
		15.94	11.57	٦	
elected Emission Rates	10.92				
elected Emission Rates Rate of carbon dioxide emission in drained soil (t CO ₂ ha ⁻¹ yr ⁻¹)	10.92 10.92				
RESULTS Selected Emission Rates Rate of carbon dioxide emission in drained soil (t CO_2 ha ⁻¹ yr ⁻¹) Rate of carbon dioxide emission in undrained soil (t CO_2 ha ⁻¹ yr ⁻¹) Rate of methane emission in drained soil ((t CH_4 -C) ha ⁻¹ yr ⁻¹)	10.92 10.92 0.002	15.94	5.36 -0.015		

Note: Note, CO₂ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).



Emissions due to loss of DOC and POC

Note: Note, CO2 losses from DOC and POC are calculated using a simple approach derived from generic estimates of the percentage of the total CO2 loss that is due to DOC or POC leaching

No POC losses for bare soil included yet. If extensive areas of bare soil is present at site need modified calculation (Birnie et al, 1991)

	Expected	Minimum	Maximum		
Total C loss					Note: Only restored drained land included because if land is not
Gross CO ₂ loss from restored drained land (t CO ₂)	0	0	0	4	restored, the C lost has already been counted as carbon dioxide
Gross CH ₄ loss from restored drained land (t CO ₂ equiv.)	0	0	0		<u>.</u>
Gross CO ₂ loss from improved land (t CO ₂)					
Degraded Bog	0	0	0		
Felled Forestry	0	0	0		
Borrow Pits	0	0	0		
Foundations & Hardstanding	0	0	0		Assumption: DOC loss ranges between 7 - 40% of the total gased
Gross CH ₄ loss from improved land (t CO ₂ equiv.)					loss if calculated from the reported (minimum and maximum) value
Degraded Bog	0	0	0		in Worrall 2009 and is 26% of the total gaseous loss if calculated fu the mean of reported maximum and minimum value in Worrall 200
Felled Forestry	0	0	0		These DOC values are flux based on soil water concentration (i.e
Borrow Pits	0	0	0		12.5 - 85.9 MgC/KM ² /yr)
Foundations & Hardstanding	0	0	0		and not on flux at catchment outlet (i.e. 10.3 - 21.8 MgC/KM ² /y
Conversion factor: CH ₄ -C to CO ₂ equivalents	30.6667	30.6667	30.6667	1/	Worrall, F. et al., 2009. The multi-annual carbon budget of a peat-covered catchment. Science of
% total soil C losses, lost as DOC	26	7	40	ĭ	Assumption: In the long term, 100% of leached DOC is assumed to
% DOC loss emitted as CO ₂ over the long term	100	100	100	•	lost as CO ₂
% total soil C losses, lost as POC	8	4	10	₹	Assumption: POC loss ranges between 4-10% of the total
% POC loss emitted as CO ₂ over the long term	100	100	100		gaseous loss if calculated from the reported values and is
Total gaseous loss of C (t C)	0	0	0	7	of the total gaseous loss if calculated from the mean of
Total C loss as DOC (t C)	0	0	0	$\langle \rangle$	reported maximum and minimum value in Worrall 2009.
Total C loss as POC (t C)	0	0	0		range is (7 - 22.4 MgC/KM ² /yr) (Worrall et al, 2009).
RESULTS					
Total CO ₂ loss due to DOC leaching (t CO ₂)	•	•	•		
	U	U	U		Assumption: In the long term, 100% of leached POC is assumed to
Total CO ₂ loss due to POC leaching (t CO ₂)	0	0	0		lost as CO ₂
Total CO, loss due to DOC & POC leaching (t CO)	0	0	0		

Total CO₂ loss due to DOC & POC leaching (t CO₂) 0 0 0 Additional CO₂ payback time of windfarm due to DOC & POC ...coal-fired electricity generation (months) 0 0 0 ... grid-mix of electricity generation (months) 0 0 0 ...fossil fuel - mix of electricity generation (months) 0 0 0

Assumption: DOC loss ranges between 7 - 40% of the total gaseous loss if calculated from the reported (minimum and maximum) values in Worrall 2009 and is 26% of the total gaseous loss if calculated from the mean of reported maximum and minimum value in Worrall 2009. These DOC values are flux based on soil water concentration (i.e. 12.5 - 85.9 MaC/KM²/vr)

and not on flux at catchment outlet (i.e. 10.3 - 21.8 MgC/KM²/yr) Worrall, F. et al., 2009. The multi-annual carbon budget of a peat-covered catchment. Science of The

Assumption: In the long term, 100% of leached DOC is assumed to be lost as CO₂

Assumption: POC loss ranges between 4-10% of the total gaseous loss if calculated from the reported values and is 8% of the total gaseous loss if calculated from the mean of reported maximum and minimum value in Worrall 2009. POC range is (7 - 22.4 MgC/KM²/yr) (Worrall et al, 2009).

Assumption: In the long term, 100% of leached POC is assumed to be lost as CO₂

Click here to move to Payback Time

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Emissions due to loss of DOC and POC

Note: Note, CO2 losses from DOC and POC are calculated using a simple approach derived from generic estimates of the percentage of the total CO2 loss that is due to DOC or POC leaching

No POC losses for bare soil included yet. If extensive areas of bare soil is present at site need modified calculation (Birnie et al, 1991)

Emissions due to forest felling - calculation using simple management data

Note: Emissions due to forestry felling are calculated from the reduced carbon sequestered per crop rotation. If the forestry was due to be removed before the planned development, this C loss is not attributable to the wind farm and so the area of forestry to be felled should be entered as zero.

	Expected	Minimum	Maximum
Emissions due to forestry felling			
Area of forestry plantation to be felled (ha)	0	0	0
Carbon sequestered (tC ha ⁻¹ yr ⁻¹)	0	0	0
Lifetime of windfarm (years)	25	25	25
Carbon sequestered over the lifetime of the windfarm (t C ha ⁻¹)	0	0	0
RESULTS			
Total carbon loss due to felling of forestry (t CO ₂)	0	0	0
Additional CO ₂ payback time of windfarm due to management	t of forestry		
coal-fired electricity generation (months)	0	0	0
grid-mix of electricity generation (months)	0	0	0
fossil fuel - mix of electricity generation (months)	0	0	0

Click here to move to Payback Time Click

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Emissions due to forest felling - calculation using simple management data

Note: Emissions due to forestry felling are calculated from the reduced carbon sequestered per crop rotation. If the forestry was due to be removed before the planned development, this C loss is not attributable to the wind farm and so the area of forestry to be felled should be entered as zero.

	Eve	Total Min	Max		restry Are Min			restry Are Min			restry Are Min			restry Are Min			restry Are Min	
Loss of carbon	Exp	Min	Max	Ехр	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
sequestration due to felling of forestry for the wind																		
farm Number of turbines Area felled around each	0	0	0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0
urbine (ha) area of forestry plantation to	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
e felled for wind farm (ha) area replanted around each	-	-		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
urbine (ha) Area of forestry plantation to	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
be replanted (ha) Area deforested for wind arm (ha)	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
Carbon sequestered per nectare for lifetime of the				0	0	0	0	0	0	0	0		0	0	0	0	0	0
vind farm (t C ha ⁻¹) Fotal potential carbon																		
sequestration loss due to felling of forestry for the wind farm (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cleared Forest Floor Emissions																		
Soil type				Peaty Gley	Peaty Gley	Peaty Gley	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Dee Pea
ife time of wind farm (years)	25	25	25	25	25	25	25	25	25	25	25		25	25	25	25	25	25
Area deforested for wind arm (ha)	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
Carbon released per hectare unforested (tC ha ⁻¹ yr ⁻¹)				3.98	3.98	3.98	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
Fotal emissions due to cleared land (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Emissions from harvesting operations																		
Soil type				Peaty Gley	Peaty Gley	Peaty Gley	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Dee Pea
Emissions from harvesting operations (g $CO_2 m^{-3}$)	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
Age of forest to be felled (years)	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
Area of forestry plantation to be felled for wind farm (ha)	0	0	0	0	0	0	о	0	0	0	0		0	0	0	0	0	0
/olume of wood felled (m ³ ha ³				0	0	0	0	0	0	0	0		0	0	0	0	0	о
, Emissions due to narvesting operations (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Savings from use of felled forestry as biofuel																		
s timber used as biofuel?				No	No	No	No	No	No	No	No	No	No	No	No	No	No	No
Area of forestry plantation to be felled for wind farm (ha)	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
Carbon in felled forestry (tC ha ⁻¹)				282	282	282	282	282	282	282	282	282	282	282	282	282	282	282
(Carbon : Biomass) ratio of felled forestry Biomass weight of felled				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
forestry (t) Value of felled forestry as a	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
biomass fuel (MWh t ⁻¹) Fotal biomass power value (MWh)				0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.00000 0	0.000 0
Fossil fuel-mix emission actor (t $CO_2 MWh^{-1}$)	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.70
Savings in CO ₂ emissions associated with using felled orestry as a biofuel (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0
Distance to nearest biomass power plant (km)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Emissions of CO ₂ associated with transportation by each km distance (t CO ₂ km ⁻¹)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Fotal emissions of CO ₂ associated with ransportation (t CO _{2 eq.})				0	0	0	0	0	0	0	0		0	0	0	0	0	0
Fossil fuel equivalent saving (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Savings from use of replanted forestry as a																		
biofuel Area of replanted forestry	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
/ha) Soil type	~			Peaty	Peaty	Peaty	Deep	Deep	Deep	Deep	Deep	Deep	Deep	Deep	Deep	Deep	Deep	Dee
Number of years replanted				Gley 25	Gley 25	Gley 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Peat 25	Pea 25
orestry grown on site (years) Carbon in replanted forestry																		
when felled (tC ha ⁻¹) Carbon : Biomass) ratio of				149	149	149	149	149	149	149	149	149	149	149	149	149	149	149
elled forestry Biomass weight (t)	0	0	0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0	0.0 0
Value of replanted forestry as a biomass fuel (MWh t ⁻¹)				0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.000
Total biomass power value MWh)				0	0	0	0	0	0	0	0		0	0	0	0	0	0
Fossil fuel-mix emission actor (t CO ₂ MWh ⁻¹)	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.701	0.70
Savings in CO_2 emissions associated with using eplanted forestry as a				0	0	0	0	0	0	0	0		0	0	0	0	0	0
biofuel (t CO ₂) Distance to nearest biomass	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.
ower plant (km) Emissions of CO ₂ associated																		
the transmission (t. CO. June		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	

power plant (km)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Emissions of CO2 associated																		
with transportation (t CO2 km	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
¹ t ⁻¹)																		
Carbon equivalent of transportation (t CO _{2 eq.})				0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Fossil fuel equivalent saving (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
RESULTS																		
Total Carbon loss								0										
associated with forest management (t CO ₂)	0	0	0	0	0	0	0	U	0	0	0	U	0	0	0	0	0	U
Additional CO ₂ payback time	e of windfa	arm due to	manage	ment of fo	restrv													
coal-fired electricity	1	1	I															
generation (months)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
grid-mix of electricity	0	0	0	0	0	0	0	0	0	0	0	<u> </u>	0	0	0	0	0	•
generation (months) fossil fuel - mix of	U	U	0	U	U	U	U	U	U	v	v	v	U	U	U	v	U	U
electricity generation													0	0	0			

CO, loss from forests - calculation using detailed management information Forest carbon calculator (Perks et al, 2009)

									-									
Carbon sequestration in tr																		
Simplified version of the 3PG mode	I (Xenakis et al	l, 2008). This v	ersion, doesn't re	quire climate	data as no ex	plicit environ	mental modifi	ieris										
calculated. Instead, it uses a factor																		
annual incoming solar radiation, a r																		
The model calculates gross primary																		
wood and foliage. A soil model calc	ulates the size	of old and you	ng carbon pools,	respiration lo	ises from the	se pools and	from this net	ecosystem										
productivity (NEP).																		
The model does not need temp/rain on site yield class and temperature																		
model for many species even for a	amuning such	ancy (LUE), h	r "decidures"	ti use etitoer	cy (QTE) is t	isao, making	it easier to de	weich are										
Calibratico for Okto Comos aluns f	WE - 0.08 (m)	diada as 1115	-2210040	and for SD OF	- 0.05 (m)	the first	5 - 1 97 /AC	MD										
Values taken from input		Total		Fo	restry Are	sa 1	Fe	restry An	ea 2	Fo	prestry An	ea 3	Fo	prestry An	ea 4	Fo	restry Ar	ea 5
sheet	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max		Min	Max
Accumulated temperature	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050	(< 1050
(day-degrees > 5°C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)	deg.C)
Code number	- 1 i	- i		- 1 C	- 14 C	1			1.1		1.14	1.1	1.1		1.1		1.1	
Major Soll Sub Group	Peaty gley			Peaty	Peaty	Peaty	0	0	0	0	0	0	0	0	0		0	0
Code number	1			gley 1	gley 1	gley 1		•		•	•		0				•	•
Species	Scots pine			Scots pine	Scots pine	Scots pine	0	0	0	0	0	0	0	0	0		0	0
Code number	1			1	1	1		•		•	•		0				•	•
Age of forestry when felled for windfarm (vr)	0			0	0	0	0	0	0	0	0	0	0	0	0		0	0
for windfarm (yr) Lifetime of windfarm																		
(vears)	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25		25	25
Years after felling when	0			0	0		0	0	0	0	0		0	0	0		~	0
replanting occurs	U			U	U	0	U U			U	U	0	U		0		0	
Age of seedlings on				0	0	0	0	0	0	0	0	0	0	0	0		0	0
planting (yr)						•								, v	, v			
Years when replanted																		
forestry will be grown on wind farm site	25			25	25	25	25	25	25	25	25	25	25	25	25		25	25
wind farm site																		
RESULTS																		
Calculated Net Primary		Total	1		restry Are			restry An			prestry An			prestry An			restry Ar	
Production	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Εхφ	Min	Max	Exp	Min	Max
Net loss in forest primary				_		_				- T	- T						- T	
production over lifetime	#N/A	#N/A	#N/A	139	139	139	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A		#N/A	#N/A
of wind farm (t C ha ¹)																		
Total forest net primary																		
production at felling for	#N/A	#N/A	#N/A	282	282	282	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A		#N/A	#N/A
wind farm (t C ha ¹) Net primary production or		ļ	· · · · ·															
replanted forestry				_		_				- T	- T						- T	
assuming same species		1	1															
replanted and managed	#N/A	#N/A	#N/A	149	149	149	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A		#N/A	#N/A
over lifespan of windfarm			1															
(tCha ⁻¹)																		

BACKGROUND CALCULATIONS

				Sol	icies			lelected Valu	10	
Parameter			Units		Sitka	Area 1	Area 2	Area 3	Area 4	
3PG module				Scots Pine	Spruce		~~~			
Average annual photosynthetic	ally active radiation	2880	MJ m ⁻² yr ⁻¹							
Light extinction coefficient		0.5	-			0.5				
Specific leaf area			m² kg ⁻¹ C	6	8	6				
Leaf longevity			yes	4	7	- 4				
Fine root longevity		1	yes							
Maximum light-use efficiency			kg C MJ ⁻¹ day ⁻¹	0.00152	0.00168	0.00152		0.001658		
Total reduction factor for misc	environmental					0.3178		#N/A		
effects			-							
Ratio of NPP to GPP		0.47	-			0.47				
Allocation to foliage		0.25	-			0.25				
Coefficient for allocation respo	nse to nitrogen	1.00	-							
Age for 50% reduction in light-	use efficiency		yes	100	120	100				
Initial foliage biomass		0.005	kg C m ²			0.005				
Understorey module										
Understorey LAI		3.00				3.00	3.00	3.00	3.00	
	Quantum			T						
Conversion Factors	yield efficiency (mol.mol ⁻¹)	80	Light use efficiency (kgC MJ ⁻¹)			GPP Reduc	tion Factor L	ookup Tabk		
	0.05		0.00130				Accur	nulated temp	0/36/19	1
							Less men	1050 10	More than	
							1050 °C yr	1350 ° C yr	1050 °C yr	
					Soil type		1			
	Light use		Quantum yield	1			1			1
	efficiency	80	afficiency	1			1			1
	(kgC MJ ⁻¹)		(mol mol ")			Code	1	2	3	
	0.00135		0.0489		Peary Glay	1	0.3178	0.3551	0.3720	
gDM_mol	24				Deep Peat	2	0.3177	0.3569	0.3679	
molPAR MJ	2.3									

Integration step (yrs)	1		Forestry Area 1		Forestry Area 2			Forestry Area 3		Forestry Area 4		Forestry A	rea 5
		State variables	Light interception	Primary production State va	bles Light interception	Primary production	State variables	Light interception	Primary production	State variables Light interception	Primary production	State variables Light interception	Primary production
			όραυ	¥4000	όραυ - όρα _{υπ} , όραυ _υ	-		¢ραυ _{υε} . ¢ρα _{υε} . Utilized		épau - épaus, épaus,		épau - épaux.	lpau _{us} - Utilzed y vene
Age (years)	Thinning regime	W-Foliage LAI-Leaf area	Utilized photosynth- absorbed etically active photosynth	NPP - NPP - Currulated Net primary Total net total net	U-Lest absorbed photosynth- etically active photosyn	h- Net primary Total net total net	WY-Foliage LAI-Leaf	Utilized photosynth- absorbed etically active photosynth	Net primary Total net total net	WY-Folage LAI-Leaf absorbed photosynth- biomena (he care information)	d NPP NPP Cumulated With the Net primary Total net total net	- Foliage LAI - Least absorbed etically active pl	bacrbad NPP NPP Cumulated atoxynth- Net primary Total net total net
		m²) index(m²m²)	etically active the radiation of radiation of radiation the	trees production primary Cm ²)	m ² m ²) etically active radiation of radiation radiation the the	of trees production production (kg C m ² yr ²) (t C ha ⁻¹ yr ²)	Cm ²) (m ² m ²)	etically active radiation of radiation or radiation the	f trees production primary (kg C m ² yr ²) (t C ha ¹ yr ²)	Cm ²) (m ² m ²) etically active the station of reduction of the station of reduction of the station of the stati	of trees production production (kg C m ² yr ²) (t C ha ² yr ²)	Cm ²) (m ² m ²) etically active the radiation of ra	diation of trees production production the (kg C m ² yr ²) (t C ha ¹ yr ²)
			(MJ m ² yr ¹) (MJ m ² yr ¹) (MJ m ² yr ²)	(com)	(MJ m ² yr ¹) (MJ m ² yr ¹) (MJ m ²) (MJ m ² yr ¹) (MJ m ²)	9 (CAL)		(MJ m ² yr ¹) (MJ m ² yr ¹) (MJ m ² yr ¹)	(c.m.)	(MJ m ² yr ²)		(MJ m ² yr ¹) (MJ m ² yr ²) (M	dentorey Um ² yr ²)
1	0.00	0.0074 0.04	13.63 2204 701 20.19 2188 695	0.0 5.1 5 0.0050	0.04 PNIA 2193 PNIP RNIA PNIA PNIA PNIP	ANA ANA ANA ANA ANA ANA	0.0050 0.04 #N(A #N(A	#N/A 2193 #N/A #N/A #N/A #N/A	aNA aNA aNA aNA aNA aNA	6.0050 0.04 INVA 2193 INVA INVA INVA INVA INVA INVA	anua anua anua d	10050 0.04 PNIA 2193 RNA RN/A PNIA RNIA	ania ania ania ania ania ania ania ania
3	0.00	0.0164 0.10	43.86 2130 677	0.0 5.1 15 ANA	ANIA ANIA ANIA ANIA	aN/A aN/A aN/A	ANIA ANIA	INVA INVA INVA	aN/A aN/A aN/A	ENCA ENCA ENCA ENCA ENCA	anua anua anua	RNIA RNIA RNIA ANIA	ania ania ania ania
5	0.00	0.0242 0.15	92.84 2010 639	0.0 5.2 20 100A 0.1 5.2 31 4NA	ANIA ANIA ANIA ANIA		ANGA ANGA	INVA INVA INVA	anya anya anya	INCA INCA INCA INCA INCA		INCA INVA INVA INVA	anua anua anua anua
7	0.00	0.0524 0.31	2010 2188 665 2462 2144 688 4.86 2139 667 4.86 2139 667 9.85 2139 667 11155 1265 676 1213.18 1102 660 1202.8 1162 687 213.13 1170 668 1203.3 164 640 203.3 164 640 205.3 164 433 207.3 1164 423 203.73 1164 433 442.04 1168 374 442.05 1168 374 442.06 1168 374 452.05 365 365 450.00 1052 345	0.1 5.3 36 RVA 0.1 5.3 41 RVA	ANDA PROA PROA PROA ANIA ANIA ANIA ANIA		ANGA ANGA	INVA INVA INVA	anya anya anya	NULL NULL <th< td=""><td></td><td></td><td>ANIA ANIA ANIA ANIA</td></th<>			ANIA ANIA ANIA ANIA
9	0.00	0.0755 0.45	185.55 1784 587	0.1 5.3 47 RVA 0.1 5.4 52 RVA	ANDA PROA PROA PROA ANIA ANIA ANIA ANIA		ANGA ANGA	INVA INVA INVA	anya anya anya	ANIA ANIA ANIA ANIA ANIA		INCA INVA INVA INVA	ANIA ANIA ANIA ANIA
10	0.00	0.1069 0.64	249.18 1628 518 001.01 1510 100	0.2 5.4 56 RVA	ANDA PROA PROA PROA ANIA ANIA ANIA ANIA		ANGA ANGA	INVA INVA INVA	anya anya anya	ANIA ANIA ANIA ANIA ANIA		INCA INVA INVA INVA	ANIA ANIA ANIA ANIA
12	0.00	0.1239 0.74	28421 1543 490 320.53 1454 462	0.2 5.6 74 IN/A	INCA INCA INCA INCA	aN/A aN/A aN/A	ANIA ANIA	INVA INVA INVA	aN/A aN/A aN/A	ENCA ENCA ENCA ENCA ENCA	anua anua anua	RNIA RNIA RNIA ANIA	ania anua anua anua
14	0.00	0.1876 1.13	357-33 1364 433 393.77 1274 405	0.3 5.7 86 ANA	INCA INCA INCA INCA	aN/A aN/A aN/A	ANIA ANIA	INVA INVA INVA	aN/A aN/A aN/A	ENCA ENCA ENCA ENCA ENCA	anua anua anua	RNIA RNIA RNIA ANIA	ania anua anua anua
10	0.00	0.2349 1.41	423.06 1166 376 462.58 1108 351 462.74 1020 207	0.3 5.8 97 INVA	ANUA ANUA ANUA ANUA ANUA	ANIA ANIA ANIA	NNIA NNIA	INVA INVA INVA	ativa ativa ativa	ADUA ADUA DINA DINA ANIA ADUA ADUA DINA ADUA ADUA	ANIA ANIA ANIA ANIA ANIA ANIA	ENIA ENIA ENIA ENIA ENIA ENIA ENIA ENIA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
19	0.00	0.2823 1.69	522.22 959 305 494.00 1052 234	0.4 5.9 109 #N/A	#N(A #N(A #N)A #N)A		NN/A NN/A	INVA INVA INVA	ANA ANA ANA	NNA NNA NNA NNA NNA		RNA RNA RNA RNA	ANIA ANIA ANIA ANIA
20 21	0.00	0.2514 1.51 0.2750 1.65	484.09 1052 334 513.29 980 312	0.3 5.8 115 RVA 0.4 5.9 121 RVA	ANCA PROA PROA PROA ANCA ANCA ANCA ANCA		ANIA ANIA	INVA INVA INVA	anya anya anya	ANIA ANIA ANIA ANIA ANIA		INCA INVA INVA INVA	ANIA ANIA ANIA ANIA
22 23	0.00	0.3199 1.92	563.17 857 272	0.4 6.0 133 IN/A	ANCA PROA PROA PROA ANCA ANCA ANCA ANCA		ANIA ANIA	INVA INVA INVA	anya anya anya	ANIA ANIA ANIA ANIA ANIA		INCA INVA INVA INVA	ANIA ANIA ANIA ANIA
24 25	0.18	0.2082 1.79	539.05 915 291	0.4 5.9 144 AN/A	INCA INCA INCA INCA	aN/A aN/A aN/A	ANA ANA	INVA INVA INVA	aN/A aN/A aN/A		anua anua anua	RNIA RNIA RNIA ANIA	ania anua anua anua
26 27	0.00	0.3199 1.92 0.3403 2.04	582.52 857 272 582.54 806 256	0.4 8.0 150 INA 0.4 6.0 156 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
28 29	0.00	0.3503 2.16 0.3767 2.26	600.18 761 242 615.34 723 230	0.4 E.0 162 INA 0.4 E.0 168 INA	RINIA RINIA RINIA RINIA RINIA RINIA RINIA RINIA	ANA ANA ANA ANA ANA ANA	ANA ANA ANA ANA	INVA INVA INVA INVA INVA INVA	ANA ANA ANA ANA ANA ANA	ENCA ENCA ENCA ENCA ENCA	ANUA ANUA ANUA ANUA ANUA ANUA	encia encia encia encia encia encia encia encia	ANYA ANUA ANUA ANUA ANYA ANUA ANUA ANUA
30 31	0.00	0.3491 2.09	588.73 785 250 604.60 744 003	0.4 6.0 180 AN/A	#NIA #NIA #NIA #NIA	ANIA ANIA ANIA	NVA NVA	eN/A EN/A EN/A	ANA ANA ANA	ANYA ANYA ANYA ANYA ANYA		RECA INCA INVA INVA	anica anica anica anica anica anica anica anica anica
32 33	0.00	0.3832 2.30	618.10 709 225 610.44 678 040	0.4 6.0 192 ANA	#NUA #NUA #NUA #NUA #NUA #NUA #NUA #NUA	ANIA ANIA ANIA ANIA ANIA ANIA	NVA INIA NVA INIA	eN/A eN/A eN/A	ANYA ANYA ANYA	ANDA ANDA ANDA ANDA ANDA ANDA	aNIA ANIA ANIA	RECA BELIA BELIA BELIA RECIA BELIA BELIA BELIA RECIA BELIA BELIA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
10		0.008.0 0.54 0.008.0 0.54 0.1239 0.14 0.1429 0.14 0.1429 0.14 0.1450 0.09 0.1560 0.09 0.1561 1.9 0.2538 1.57 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 1.58 0.2538 2.24 0.2538 2.24 0.2538 2.23 0.2538 2.23 0.2538 2.23 0.2538 2.23 0.2539 2.38 0.2539 2.48 0.4419 2.49 0.4419 2.49 0.4419 2.49 0.4419 2.49 0.4419 2.48 0.4419<	11.91 2.248.8 76 2.248.8 76 76 2.48 2.289.8 67 4.48 2.289.8 67 4.48 2.289.8 67 4.14 2.289.8 67 1.15.2 1.161.8 642 2.14.3 1.162.8 642 2.14.3 1.163.8 1.162 2.14.1 1.79.8 642 2.14.1 1.79.8 642 2.15.2 1.163.8 1.162 2.14.1 1.79.8 642 2.14.2 1.79.8 642 2.14.3 1.79.8 642 2.14.4 1.79.8 7.21 2.14.1 1.79.8 7.21 2.14.2 1.102.8 7.21 2.14.2 1.102.8 7.21 2.14.2 1.102.8 7.21 2.14.2 1.102.8 7.21 2.14.4 1.102.8 7.21 2.14.4 1.102.8 7.21	0.4 6.0 199 eN/A 0.4 6.0 204 eN/A	#N/A #N/A #N/A #N/A #N/A #N/A #N/A #N/A	ANIA ANIA ANIA ANIA ANIA ANIA							
36 37	0.00	0.3/13 2.23 0.3865 2.32	616.72 702 223	0.4 6.0 210 INA 0.4 6.0 216 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
38 39	0.00	0.4000 2.40 0.4119 2.47	626.63 6/4 214 634.69 650 207	0.4 6.0 222 INA 0.5 6.0 228 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
40 41 40	0.05	0.4015 2.41 0.4127 2.48	632.14 649 206	0.4 ED 234 INA 0.5 E0 240 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	INCA INCA INCA INCA INCA INCA INCA INCA INCA INCA	ANUA ANUA ANUA ANUA ANUA ANUA	enca enca encia encia encia encia encia encia	ANA ANA ANA ANA ANA ANA ANA ANA
42 43	0.00	0.4224 2.53 0.4307 2.58	637.79 630 200 642.02 615 195	0.5 6.0 246 INA 0.5 6.0 252 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
44 45	0.05	0.4377 2.63 0.4199 2.52	645.01 602 191 629.87 635 202	0.5 8.0 258 INA 0.4 5.9 264 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	BYOA BYOA <th< td=""><td>anua anua anua anua anua anua</td><td>RNIA INVA INVA INVA INVA INVA INVA INVA INVA</td><td>ania anua anua anua ania anua anua anua</td></th<>	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
46 47	0.00	0.42/5 2.58 0.4337 2.60	633.14 621 197 635.18 609 194 636.14 600 191 636.12 593 188	0.5 5.9 270 INA 0.5 5.9 276 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA RNGA	ania anua anua anua ania anua anua anua
48 49	0.00	0.4387 2.63 0.4426 2.66	636.14 600 191 636.12 503 188	0.5 5.9 282 INA 0.5 5.9 288 INA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	NNA NNA NNA NNA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
50	0.00	0.4456 2.67 0.0050 0.03	635.23 588 187 13.63 2204 701	0.5 5.9 294 IN/A 0.0 5.1 5 IN/A	8N/A 8N/A 8N/A 8N/A 0.04 8N/A 2193 8N/	ANA ANA ANA ANA ANA ANA	#N/A #N/A 0.0050 0.04	#N/A #N/A #N/A #N/A 2193 #N/A	aN/A aN/A aN/A aN/A aN/A aN/A	8N/A 8N/A 8N/A 8N/A 8N/A 8N/A 0.0050 0.04 8N/A 2193 8N/A	ANIA ANIA ANIA ANIA O	RNA RNA RNA RNA 1.0050 0.04 RNA 2193	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
52 53	0.00	0.0074 0.04 0.0110 0.07	20.19 2188 605 29.82 2164 688	0.0 5.1 10 ANA 0.0 5.1 15 ANA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	aN/A aN/A aN/A aN/A aN/A aN/A	NNA NNA NNA NNA	INVA INVA INVA INVA INVA INVA INVA INVA	ANA ANA ANA ANA ANA ANA	Ample Ample <th< td=""><td>ANIA ANIA ANIA ANIA ANIA ANIA</td><td>MAX MAX MAX</td></th<> <td></td>	ANIA ANIA ANIA ANIA ANIA ANIA	MAX MAX	
54	0.00	0.0164 0.10	43.86 2130 677 64.10 2081 661	0.0 5.2 20 INA 0.0 5.2 26 INA	BEDA BEDA <td< td=""><td>ANA ANA ANA ANA ANA ANA</td><td>ANIA ANIA ANIA ANIA</td><td>INVA INVA INVA INVA INVA INVA</td><td>aNA aNA aNA aNA aNA aNA</td><td>INCA INCA INCA INCA INCA INCA INCA INCA INCA INCA</td><td>anua anua anua anua anua anua</td><td>RNIA INVA INVA INVA INVA INVA INVA INVA INVA</td><td>ania ania ania ania ania ania ania ania</td></td<>	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	INCA INCA INCA INCA INCA INCA INCA INCA INCA INCA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania ania ania ania ania ania ania ania
58 57	0.00	0.0356 0.21 0.0433 0.26	92.84 2010 639 111.55 1965 624	0.1 5.2 31 ANA 0.1 5.3 36 ANA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA
58 59	0.00	0.0631 0.38	133.18 1912 608 157.85 1852 589	0.1 5.3 41 ANA 0.1 5.3 47 ANA	enca enca enca enca enca enca enca	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	INVA INVA INVA INVA INVA INVA	ANA ANA ANA ANA ANA ANA		ANIA ANIA ANIA ANIA ANIA ANIA	enca enca pinia enca enca enca enca enca	ANA ANA ANA ANA ANA ANA ANA ANA
60 61	0.00	0.0755 0.45 0.0898 0.54	185.55 1784 567 216.11 1709 543	0.1 5.4 52 ANVA 0.2 5.4 58 ANVA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
62 63	0.00	0.1059 0.64 0.1239 0.74	249.18 1628 518 284.21 1543 490	0.2 5.5 63 ANA 0.2 5.5 69 ANA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
64 65	0.00	0.1437 0.86 0.1650 0.99	320.53 1454 462 357.33 1384 433	0.2 5.6 74 #N/A 0.3 5.6 80 #N/A	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA BNA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
66 67	0.00	0.1876 1.13 0.2110 1.27	393.77 1274 405 429.08 1188 378	0.3 5.7 86 4N/A 0.3 5.8 91 4N/A	NDLA NDLA NDLA NDLA NDLA NDLA NDLA NDLA	aN/A aN/A aN/A aN/A aN/A aN/A	NIA NIA NIA NIA	IN/A INIA INIA IN/A INIA INIA	aN/A aN/A aN/A aN/A aN/A aN/A	RNA RNA RNA RNA RNA RNA	ANIA ANIA ANIA ANIA ANIA ANIA	RNA RNA RNA RNA RNA RNA RNA RNA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA
68	0.00	0.2588 1.55	462.58 1106 361 493.74 1029 327	0.3 5.8 97 INA 0.4 5.9 103 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
70 71	0.00	0.2823 1.69 0.2514 1.51	522.22 959 305 484.09 1052 334	0.4 5.9 109 INA 0.3 5.8 115 INA	RECA RECA RECA RECA RECA	ANA ANA ANA ANA ANA ANA	ANA ANA	INVA INVA INVA INVA INVA INVA	aNA aNA aNA aNA aNA aNA	RUA INUA INUA INUA INUA INUA	anua anua anua anua anua anua	RNIA INVA INVA INVA INVA INVA INVA INVA INVA	ania anua anua anua ania anua anua anua
72 73	0.00	0.2750 1.65 0.2980 1.79	513.29 980 312 539.67 915 291	0.4 5.9 121 #N/A 0.4 5.9 127 #N/A	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	NNA NNA NNA NNA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
74 75	0.00	0.3199 1.92 0.3405 2.04	563.17 857 272 583.84 806 256	0.4 6.0 133 #N/A 0.4 6.0 139 #N/A	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	ANA ANA ANA ANA ANA ANA	NNA NNA NNA NNA	IN/A INIA INIA IN/A INIA INIA	ANA ANA ANA ANA ANA ANA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA	enca enca enca enca enca enca enca enca	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
76 77	0.00	0.2982 1.79 0.3199 1.92	539.05 915 291 562.22 857 272	0.4 5.9 144 ANA 0.4 8.0 150 ANA	ANCA ANCA ANCA ANCA ANCA ANCA ANCA ANCA	ania ania ania ania ania ania	NNA NNA NNA NNA	IN/A IN/A IN/A IN/A IN/A IN/A	ANA ANA ANA ANA ANA ANA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA	RNA RNA RNA RNA RNA RNA RNA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
78 79	0.00	0.3403 2.04 0.3593 2.16	582.54 806 256 600.18 761 242	0.4 6.0 156 4N/A 0.4 6.0 162 4N/A	ANCA ANCA ANIA ANI ANCA ANIA ANIA	8N/A 8N/A 8N/A 8N/A 8N/A 8N/A	NNA NNA NNA NNA	BN/A BNIA BNIA BN/A BNIA BNIA	AN/A AN/A AN/A AN/A AN/A AN/A	ANCA ANCA ANCA ANCA ANCA ANCA ANCA ANCA	ANIA ANIA ANIA ANIA ANIA ANIA	enia enia enia enia enia enia	AN'A ANIA ANIA ANIA AN'A ANIA ANIA ANIA
計量因為其低低原理 總合 经合体 化磷酸钾 使使为 下方 沒有 內方 有方 指子 酸盐 化盐酸盐 建酸酸盐 使用的 的复数 化乙酰基乙酰胺 化氯化化 化化化化化化化化化化化化化化化化化化化化化化化化化化化化化化化化	0.00	00074 0.04 000740 0.04 0.0110 0.05 0.0110 0.05 0.0110 0.01 0.0110 0.01 0.0110 0.01 0.01058 0.01 0.01058 0.01 0.01058 0.01 0.01058 0.01 0.01058 0.01 0.01058 0.04 0.00058 0.04 0.00058 0.04 0.00058 0.04 0.1407 0.04 0.1407 0.04 0.1407 0.04 0.20088 0.05 0.20088 0.04 0.20088 0.04 0.20088 1.01 0.20088 1.02 0.20088 1.03 0.20088 1.04 0.20098 2.03 0.20098 2.03 0.20098 2.03 0.20098 2.03 0.20098 2.03 0	11.11 2.24.84 7.67 4.24.8 2.23.8 6.27 4.24.8 2.23.8 6.27 4.24.8 2.23.8 6.27 4.24.8 2.23.8 6.27 11.12.5 11.12.6 6.27 11.13.1 11.12.6 6.27 2.42.8 1.08.14 6.29 2.42.11 1.08.2 6.29 2.42.11 1.08.14 6.29 2.42.11 1.08.14 6.29 2.42.14 1.08.14 6.29 2.42.14 1.08.14 6.29 2.42.14 1.08.14 6.29 2.42.14 1.08.14 6.29 2.42.14 1.08.14 6.29 2.42.14 1.09.14 6.29 2.42.14 1.09.14 6.29 2.42.14 1.09.14 7.21 2.42.14 1.09.14 7.21 2.42.14 1.09.14 7.21 2.42.14 1.09.14 7.21 2.42.14 1.09.14<	0.4 6.0 168 AN/A 0.4 6.0 174 AN/A	ANCA ANCA ANLA ANLA ANCA ANLA ANLA ANLA	ANA ANA ANA ANA ANA ANA							
82 83	0.00	0.369 2.20	528.73 785 250 604.60 744 237	0.4 6.0 180 AN/A 0.4 6.0 188 AN/A	#NCA #NCA #NCA #NCA #NCA #NCA #NCA #NCA	ANYA ANYA ANYA ANYA ANYA ANYA	NVA INA NVA INA	INCA INIA INIA INIA INIA INIA	anva anva anva anva anva anva	ANCA ANCA ANCA ANCA ANCA ANCA ANCA ANCA	anua anua anua anua anua anua	RUA RUA RNIA RNIA RNIA RNIA RNIA	anua anua anua anua anua anua anua anua
84 85	0.00	0.3832 2.30 0.3978 2.39	618.10 709 225 629.44 678 216	0.4 6.0 192 AN/A 0.4 6.0 199 AN/A	ANCA ANCA ANLA ANLA ANCA ANLA ANLA ANLA	ANA ANA ANA ANA ANA ANA	NVA INA NVA INA	INCA INIA INIA INIA INIA INIA	aN/A aN/A aN/A aN/A aN/A aN/A	ANCA ANCA ANCA ANCA ANCA ANCA ANCA ANCA	anta ania ania ania ania ania	RICA INIA INIA INIA INIA INIA INIA INIA	anva anua anua anua anua anua anua anua
86 87	0.00	0.3545 2.13 0.3713 2.23	530.46 773 246 604.74 734 233	0.4 6.0 204 AN/A 0.4 6.0 210 AN/A	800A 800A 800A 800A 800A 800A 800A 800A	ANA ANA ANA ANA ANA ANA	NVA INA NVA INA	INVA INVA INVA INVA INVA INVA	aN/A aN/A aN/A aN/A aN/A aN/A	RUA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	anta ania ania ania ania ania	RICA INIA INIA INIA INIA INIA INIA INIA	anva anua anua anua anua anva anua anua anua
88 89	0.00	0.3885 2.32 0.4000 2.40	616.72 702 223 626.63 674 214	0.4 6.0 216 жүх 0.4 6.0 216 жүх 0.4 6.0 228 жүх 0.5 6.0 228 жүх 0.4 6.0 228 жүх 0.5 6.0 228 жүх 0.6 6.0 228 жүх 0.6 6.0 226 жүх 0.6 6.0 228 жүх 0.6 6.0 228 жүх 0.6 5.0 228 жүх 0.4 5.0 228 жүх 0.5 5.9 228 жүх 0.5 5.9 228 жүх 0.5 5.9 228 жүх 0.5 5.9 270 жүх 0.5 5.9 228 жүх	476A 676A 676A 6767 476A 6767A 6767A 6767A	ANIA ANIA ANIA ANIA ANIA ANIA	#N/A #N(A #N/A #N(A	RVA BNIA BNIA BNIA BNIA BNIA	ANA ANA ANA ANA ANA ANA	870A 870A 870A 870A 870A 870A 870A 870A 870A 870A 870A	ANIA ANIA ANIA ANIA ANIA ANIA	RICA INIA INIA INIA INIA INIA INIA INIA INIA INIA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
90 91	0.00	0.4119 2.47 0.4015 2.41	634,69 650 207 624,90 671 213	0.5 6.0 228 AN/A 0.4 6.0 234 AN/A	ANGA BNGA BNGA BNGA BNGA BNGA BNGA BNGA BNGA	ANIA ANIA ANIA ANIA ANIA ANIA	#N/A #N/A #N/A #N/A	RN/A BNIA BNIA BN/A BNIA BNIA	aN/A aN/A aN/A aN/A aN/A aN/A	ARCA ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANI	ANIA ANIA ANIA ANIA ANIA ANIA	erca erca erca erca erca erca erca	ANVA ANVA ANVA ANVA ANVA ANVA ANVA ANVA
92 93	0.00	0.4127 2.48 0.4224 2.53	632.14 649 206 637.79 630 200	0.5 6.0 240 ANA 0.5 6.0 246 ANA	ANCA ANCA ANLA ANLA ANCA ANLA ANLA ANLA	ANA ANA ANA ANA ANA ANA	NVA INA NVA INA	INCA INIA INIA INIA INIA INIA	aN/A aN/A aN/A aN/A aN/A aN/A	ANCA ANCA ANCA ANCA ANCA ANCA ANCA ANCA	anta ania ania ania ania ania	RICA INIA INIA INIA INIA INIA INIA INIA	anva anua anua anua anua anua anua anua
94 95	0.00	0.4307 2.58 0.4377 2.63	642.02 615 195 645.01 602 191	0.5 6.0 252 AN/A 0.5 6.0 258 AN/A	476A 676A 676A 6767 476A 6767A 6767A 6767A	ANIA ANIA ANIA ANIA ANIA ANIA	#N/A #N(A #N/A #N(A	RVA BNIA BNIA BNIA BNIA BNIA	ANA ANA ANA ANA ANA ANA	870A 870A 870A 870A 870A 870A 870A 870A 870A 870A 870A	ANIA ANIA ANIA ANIA ANIA ANIA	RICA INIA INIA INIA INIA INIA INIA INIA INIA INIA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
96 97	0.00	0.4199 2.52 0.4275 2.56 0.4337 2.60 0.4387 2.63	645.01 602 191 629.87 635 202 633.14 621 197 635.18 609 194 636.14 600 191	0.4 5.9 284 MNA 0.5 5.9 270 MNA 0.5 5.9 276 MNA 0.5 5.9 282 MNA	ANGA BNGA BNGA BNGA BNGA BNGA BNGA BNGA	ANIA ANIA ANIA ANIA ANIA ANIA	#N/A #N/A #N/A #N/A	RN/A BNIA BNIA BN/A BNIA BNIA	ANA ANA ANA ANA ANA ANA	BYGA BYGA <td< td=""><td>ANA ANA ANA ANA ANA ANA</td><td>800A 800A 800A 800A 800A 800A 800A 800A</td><td>ANA ANA ANA ANA ANA ANA ANA ANA ANA ANA ANA ANA</td></td<>	ANA ANA ANA ANA ANA ANA	800A 800A 800A 800A 800A 800A 800A 800A	ANA ANA ANA ANA ANA ANA ANA ANA ANA ANA ANA ANA
98 99	0.00	0.4337 2.60 0.4387 2.63	635.18 609 194 636.14 600 <u>191</u>	0.5 5.9 276 AN/A 0.5 5.9 282 AN/A	RNIA BNIA BNIA BNIA RNIA BNIA BNIA BNIA RNIA BNIA BNIA BNIA	ANA ANA ANA ANA ANA ANA	#N/A #N/A #N/A #N/A	BNA BNA BNA BNA BNA BNA	ANA ANA ANA ANA ANA ANA	ANCA ANCA ANEA ANEA ANEA ANEA ANEA ANEA ANEA ANE	ANA ANA ANA ANA ANA ANA	enca enca encia encia encia encia encia encia	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
100	0.00	0.4426 2.68 0.0050 0.03	636.12 593 166	0.5 5.9 288 MNA 0.0 5.1 5 MNA	#N/A #N/A #N/A #N/A 0.04 #N/A 2193 #N/	ANA ANA ANA ANA ANA ANA	#N/A #N/A 0.0050 0.04	IN/A IN/A IN/A	AN/A AN/A AN/A	ANGA ANGA ANGA ANGA ANGA	aNA aNA aNA	RN/A RN/A RN/A RN/A 1.0050 0.04 RN/A 2193	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
102 103	0.00 0.00	0.0074 0.04 0.0110 0.07	20.19 2188 605 20.82 2164 688	0.0 5.1 10 MNA 0.0 5.1 15 MNA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	ANIA ANIA ANIA ANIA ANIA ANIA	ING ING ING ING	BN/A BN/A BN/A BN/A BN/A BN/A	AN'A AN'A AN'A AN'A AN'A AN'A	ANCA ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANI	ANIA ANIA ANIA ANIA ANIA ANIA	RNA RNA RNA RNA RNA RNA RNA RNA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA
104 105	0.00 0.00	0.0184 0.10 0.0242 0.15	43.88 2130 677 64.10 2081 681	0.0 5.2 20 MNA 0.0 5.2 26 MNA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	ANIA ANIA ANIA ANIA ANIA ANIA	ING ING ING ING	BN/A BN/A BN/A BN/A BN/A BN/A	AN'A AN'A AN'A AN'A AN'A AN'A	ANDA ALVAN ALVAN ALVAN ALVAN ANDA ALVAN ALVAN ALVAN ALVAN ANDA ALVAN ALVAN ALVAN ALVAN ALVAN ALVAN ALVAN ALVAN ALVAN ALVAN ALVAN	ANIA ANIA ANIA ANIA ANIA ANIA	RNA RNA RNA RNA RNA RNA RNA RNA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA
106 107	0.00 0.00	0.0356 0.21 0.0433 0.26	13.63 220.4 70.1 20.13 21.84 626 20.24 70.1 52.84 20.25 27.84 62.0 20.24 20.0 62.0 20.25 20.0 62.0 20.26 20.0 62.0 20.26 20.0 62.0 11.55 10.6 62.4 12.3.16 10.0 54.3 24.9.1 10.62.0 54.0 23.0.3.3 154.4 42.6 23.0.3.3 154.4 42.6 23.0.3.3 154.4 42.6 24.9.1.8 27.7 27.4 44.0.0 118.8 37.4 44.0.0 118.8 37.4	0.1 5.2 31 #N/A 0.1 5.3 36 #N/A	ANUA ANUA ANUA ANUA ANUA ANUA ANUA ANUA	ANA ANA ANA ANA ANA ANA	#VXA #VXA	BADA 2121 BADA BADA 2121 BADA BADA BADA BADA	المركبة المركبة <t< td=""><td>2020 0.55 494.5 7125 494.9 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 <td< td=""><td>δ(x) δ(x) δ(x) δ(x) δ(x) δ(x) δ(x) δ(x)</td><td>MPLA MPLA MPLA MPLA MPLA MPLA MPLA MPLA</td><td>HOL HOL HOL</td></td<></td></t<>	2020 0.55 494.5 7125 494.9 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 2024 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 494.6 <td< td=""><td>δ(x) δ(x) δ(x) δ(x) δ(x) δ(x) δ(x) δ(x)</td><td>MPLA MPLA MPLA MPLA MPLA MPLA MPLA MPLA</td><td>HOL HOL HOL</td></td<>	δ(x) δ(x) δ(x) δ(x) δ(x) δ(x) δ(x) δ(x)	MPLA MPLA MPLA MPLA	HOL HOL
108 109	0.00 0.00	0.0524 0.31 0.0631 0.38	133.18 1912 608 157.85 1852 589	0.1 5.3 41 AN/A 0.1 5.3 47 AN/A	ANCA ANCA ANNA ANN ANCA ANNA ANNA ANNA	AN/A AN/A AN/A AN/A AN/A AN/A	#N/A #N/A #N/A #N/A	PN/A PN/A PN/A PN/A PN/A PN/A	AN'A AN'A AN'A AN'A AN'A AN'A	ANUA ANUA ANUA ANUA ANUA ANUA ANUA ANUA	ANIA ANIA ANIA ANIA ANIA ANIA	RNA RNA RNA RNA RNA RNA RNA RNA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
110 111	0.00	0.0755 0.45 0.0898 0.54	185.55 1784 567 216.11 1709 543	0.1 5.4 52 ANIA 0.2 5.4 58 ANIA	ANCA ANCA ANUA ANU ANCA ANUA ANUA ANUA	AN/A AN/A AN/A AN/A AN/A AN/A	ANIA ANIA ANIA ANIA	PN/A PN/A PN/A PN/A PN/A PN/A	ANA ANA ANA ANA ANA ANA	ANCA ANCA ANCA ANCA ANCA ANCA ANCA ANCA	ANIA ANIA ANIA ANIA ANIA ANIA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
112 113	0.00	0.1059 0.64 0.1239 0.74	249.18 1628 518 284.21 1543 490	0.2 5.5 63 AN/A 0.2 5.5 69 AN/A	#NUA #NUA #NUA #NUA #NUA #NUA #NUA #NUA	ANA ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	#N/A #N/A #N/A #N/A #N/A #N/A	ANA ANA ANA ANA ANA ANA	870/A 870/A 870/A 870/A 870/A 870/A 870/A 870/A 870/A 870/A	ANIA ANIA ANIA ANIA ANIA ANIA	RNIA RNIA RNIA RNIA RNIA RNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA
114	0.00	0.1437 0.86 0.1650 0.99	320.53 1454 462 357.33 1364 433	0.2 5.6 74 MN/A 0.3 5.6 80 MN/A	#NUA #NUA #NUA #NUA #NUA #NUA #NUA #NUA	ANA ANA ANA ANA ANA	ANIA ANIA ANIA ANIA	#N/A #N/A #N/A #N/A #N/A #N/A	ANA ANA ANA ANA ANA ANA	800A 800A 800'A 800'A 800'A 800A 800'A 800'A 800'A 800'A	ANIA ANIA ANIA ANIA ANIA ANIA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA
116	0.00		313.77 1274 405 429.08 1188 378	0.3 5.7 86 4N/A 0.3 5.8 91 4N/A	#NCA #NCA #NUA #NUA #NCA #NCA #NUA #NUA	AN/A AN/A AN/A AN/A AN/A AN/A	#N/A #N/A #N/A #N/A	BN/A BNIA BNIA BN/A BNIA BNIA	#N/A #N/A #N/A #N/A #N/A #N/A	81N/A 81N/A 81N/A 81N/A 81N/A 81N/A 81N/A 81N/A 81N/A 81N/A	ANIA ANIA ANIA ANIA ANIA ANIA	RNIA RNIA RNIA RNIA RNIA RNIA	ANYA ANYA ANYA ANYA ANYA ANYA ANYA ANYA
118 119	0.00	0.2349 1.41 0.2588 1.55	462.58 1106 351 493.74 1029 527	0.3 5.8 97 AN/A 0.4 5.9 103 AN/A	#NUA #NUA #NUA #NUA #NUA #NUA #NUA #NUA	ANA ANA ANA ANA ANA	NIA NIA NIA NIA	#N/A #N/A #N/A #N/A #N/A #N/A	ANA ANA ANA ANA ANA ANA	ANCA ANCA ANCA ANCA ANCA ANCA	ANIA ANIA ANIA ANIA ANIA ANIA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	AN'A AN'A AN'A AN'A AN'A AN'A AN'A AN'A
120 121	0.00	0.2823 1.69 0.2514 1.51	522.22 959 305 484.09 1052 334	0.4 5.9 109 AN/A	ANCA ANCA ANUA ANUA	AN/A ANIA ANIA	NNA NNA	6N/A 6N/A 6N/A 6N/A 6N/A 6N/A	#N/A #N/A #N/A #N/A #N/A #N/A	870/A 870/A 870/A 870/A 870/A 870/A	ANIA ANIA ANIA ANIA ANIA ANIA	RNA RNA RNA RNA	ANIA ANIA ANIA ANIA

120	0.00			522.22			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
121	0.00			484.09			0.3			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
122	0.00			513.29			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
123	0.00			539.67			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
124	0.00			563.17			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
125	0.00			583.84			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
126	0.00			539.05			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
127	0.00			562.22			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
128	0.00			582.54			0.4			#N/A		iN/A						#N/A		#N/A							#N/A									#N/A		#N/A			#NGA
129	0.00			600.18			0.4																				#N/A									#N/A		#N/A			#NGA
130	0.00			615.34			0.4																													#N/A					#NGA
131	0.00			570.25			0.4																				#N/A											#N/A			#NGA
132	0.00			588.73			0.4					iN/A															#N/A											#N/A			#NGA
133	0.00			604.60			0.4					iN/A															#N/A														#NGA
134	0.00			618.10			0.4					#N/A															#N/A											#N/A			#NGA
135	0.00			629.44			0.4																				#N/A											#N/A			#NGA
136	0.00			590.46			0.4					iN/A															#N/A											#N/A			#NGA
137	0.00			604.74			0.4					iN/A															#N/A														#NGA
138	0.00			616.72			0.4					iN/A															#N/A											#N/A			#NGA
139	0.00			626.63			0.4					iN/A															#N/A									#N/A		#N/A			#NGA
140	0.00			634.69			0.5			#N/A		iN/A								iN/A			#N/A				#N/A									#N/A		#N/A			#NGA
141	0.00			624.90			0.4			#N/A		#N/A								#N/A			#N/A													#N/A		#N/A			#NGA
142	0.00			632.14			0.5					iN/A															#N/A											#N/A			#NGA
143	0.00			637.79			0.5					iN/A															#N/A											#N/A			#NGA
144	0.00			642.02			0.5																				#N/A											#N/A			#NGA
145	0.00			645.01			0.5			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
146	0.00			629.87			0.4			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
147	0.00			633.14			0.5			#N/A		iN/A						#N/A		#N/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#NGA
148	0.00			635.18			0.5			#N/A		#N/A						#N/A		iN/A			#N/A			#N/A	#N/A			#N/A						#N/A		#N/A			#N/A
149	0.00	0.4387	2.63	638.14	600	191	0.5	5.9	282	iN/A	#N/A	#N/A	#N/A	#N/A	#N/A	ANIA	#N/A	#N/A	#N/A	iN/A	#N/A	#N/A	#N/A	ANIA	#N/A	AN/A	#N/A	#N/A	#N/A	#N/A	ANA	#N/A	#N/A	#N/A	#N/A						

Carbon expectration in trees Employee and/or of the 90° novel (neural of al. 2005). This vector, describ happed crimes data as no explicit environment in moltan is advantant insular. The start (from 1 to its presenting the total effect of environment or opport. The simplicit encoder equipres around of shared accelerate programment of the start the model accelerate programment of the start of the start

Carbon sequestration in soil under trees

Note. More data needed. This should be the respiration from newly felled and disturbed soil, so as to include respiration from fresh plant inputs, from background soil organic matter decomposition, and from the disturbance of soil resulting in the release of additional C from soil aggregates. Different types of management disturbance should be considered. This information is not yet available, but will become available following experiments to be done by Mike Perks during 2009-2012. As an interim measure, C sequestration in soil under trees is used, so including background respiration from soil organic matter decomposition and respiration from fresh plant input.

Carbon Sequestration in Soil

Under Trees: Lookup Table

Peaty Gley	Deep Peat	(t
(t C ha ⁻¹ yr ⁻¹)	C ha⁻¹ yr⁻¹)	
3.98	5.00	

Average stand data Data obtained from Forestry Commission growth and yield tables (Edwards & Christie, 1981)

STAND_ID SPECIES ForestGALES Sitka Spruce

YIELD CLASS 14: Peaty Gley

			A			
	Initial	Age	Average tree height	Volume	Spacing	Maximum tree height
Yield class	Spacing (m)	(years)	(m)	m ³ ha ⁻¹	(m)	(m)
14	1.7	0	0.00	0.0	1.37	1.00
14	1.7	1	0.04	0.0	1.38	1.14
14	1.7	2	0.12	0.0	1.40	1.30
14	1.7	3	0.24	0.0	1.42	1.50
14	1.7	4	0.39	0.0	1.43	1.72
14	1.7	5	0.58	0.0	1.45	1.97
14	1.7	6	0.79	0.0	1.47	2.24
14	1.7	7	1.04	0.0	1.49	2.54
14	1.7	8	1.32	0.0	1.51	2.86
14	1.7	9	1.63	0.0	1.53	3.21
14	1.7	10	1.97	0.0	1.54	3.57
14	1.7	11	2.33	0.0	1.56	3.95
14	1.7	12	2.72	0.0	1.58	4.35
14	1.7	13	3.14	0.0	1.60	4.77
14	1.7	14	3.58	6.2	1.62	5.20
14	1.7	15	4.04	16.1	1.64	5.65
14	1.7	16	4.52	26.9	1.66	6.11
14	1.7	17	5.08	62	1.74	6.9
14	1.7	18	5.68	76.4	1.75	7.48
14	1.7	19	6.29	90.8	1.77	8.06
14	1.7	20	6.90	105.2	1.79	8.64
14	1.7	21	7.51	119.6	1.8	9.22
14	1.7	22	8.11	134	1.82	9.8
14	1.7	23	8.72	151.8	1.84	10.38
14	1.7	24	9.33	169.6	1.85	10.96
14	1.7	25	9.93	187.4	1.86	11.54
14	1.7	26	10.54	205.2	1.87	12.12
14	1.7	27	11.15	223	1.89	12.7
14	1.7	28	11.71	242.6	1.91	13.24
14	1.7	29	12.28	262.2	1.94	13.78
14	1.7	30	12.84	281.8	1.97	14.32
14	1.7	31	13.41	301.4	2	14.86
14	1.7	32	13.97	321	2.03	15.4
14	1.7	33	14.50	340.4	2.06	15.9
14	1.7	34	15.02	359.8	2.09	16.4
14	1.7	35	15.54	379.2	2.12	16.9
14	1.7	36	16.07	398.6	2.15	17.4
14	1.7	37	16.59	418	2.18	17.9
14	1.7	38	17.07	435.8	2.21	18.36
14	1.7	39	17.55	453.6	2.24	18.82
14	1.7	40	18.04	471.4	2.27	19.28
14	1.7	41	18.52	489.2	2.3	19.74
14	1.7	42	19.00	507	2.33	20.2
14	1.7	43	19.42	522.6	2.36	20.6
14	1.7	44	19.84	538.2	2.39	21
14	1.7	45	20.25	553.8	2.41	21.4
14	1.7	46	20.67	569.4	2.44	21.8
14	1.7	47	21.09	585	2.47	22.2
14	1.7	48	21.47	598.6	2.5	22.56
14	1.7	49	21.85	612.2	2.52	22.92
14	1.7	50	22.22	625.8	2.55	23.28

YIELD CLASS 12: Deep Peat

Yield class	Initial Spacing (m)	Age (years)	Average tree height (m)	Volume m³ ha ⁻¹	Spacing (m)	Maximum tree height (m)
12	1.7	0	0.00	0.0	1.38	1.00
12	1.7	1	0.00	0.0	1.40	1.09
12	1.7	2	0.03	0.0	1.41	1.20
12	1.7	3	0.09	0.0	1.43	1.35
12	1.7	4	0.19	0.0	1.45	1.52
12	1.7	5	0.33	0.0	1.46	1.72
12	1.7	6	0.49	0.0	1.48	1.94
12	1.7	7	0.69	0.0	1.49	2.18
12	1.7	8	0.91	0.0	1.51	2.44
12	1.7	9	1.16	0.0	1.53	2.73
12	1.7	10	1.44	0.0	1.54	3.04
12	1.7	11	1.74	0.0	1.56	3.36
12	1.7	12	2.07	0.0	1.58	3.70
12	1.7	13	2.42	0.0	1.59	4.06
12	1.7	14	2.79	0.3	1.61	4.43
12	1.7	15	3.18	8.5	1.63	4.81
12	1.7	16	3.60	17.6	1.65	5.21
12	1.7	17	4.03	27.6	1.66	5.62
12	1.7	18	4.47	38.3	1.68	6.03
12	1.7	19	5.08	63	1.74	6.9
12	1.7	20	5.64	76.2	1.75	7.44
12	1.7	21	6.21	89.4	1.77	7.98
12	1.7	22	6.77	102.6	1.78	8.52
12	1.7	23	7.34	115.8	1.8	9.06
12	1.7	24	7.90	129	1.82	9.6
12	1.7	25	8.45	145.2	1.83	10.12
12	1.7	26	8.99	161.4	1.85	10.64
12	1.7	27	9.54	177.6	1.87	11.16
12	1.7	28	10.08	193.8	1.89	11.68
12	1.7	29	10.62	210	1.91	12.2
12	1.7	30	11.15	227.6	1.92	12.7
12	1.7	31	11.67	245.2	1.94	13.2
12	1.7	32	12.19	262.8	1.96	13.7
12	1.7	33	12.72	280.4	1.97	14.2
12	1.7	34	13.24	298	1.99	14.7
12	1.7	35	13.70	315.2	2.02	15.14
12	1.7	36	14.16	332.4	2.04	15.58
12	1.7	37	14.62	349.6	2.07	16.02
12	1.7	38	15.08	366.8	2.1	16.46
12	1.7	39	15.54	384	2.13	16.9
12	1.7	40	15.98	399.8	2.15	17.32
12	1.7	41	16.42	415.6	2.18	17.74
12	1.7	42	16.86	431.4	2.2	18.16
12	1.7	43	17.30	447.2	2.23	18.58
12	1.7	44	17.74	463	2.26	19
12	1.7	45	18.12	477	2.28	19.36
12	1.7	46	18.50	491	2.31	19.72
12	1.7	47	18.87	505	2.33	20.08
12	1.7	48	19.25	519	2.36	20.44
12	1.7	49	19.63	533	2.39	20.8
12	1.7	50	19.96	544.8	2.41	21.12



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Machinesist intervel bounds 13 14 15 16 <t< th=""><th></th><th></th></t<>		
Exp Image: Comparison of the comparison of t		Max Mind speed at back of in felled gap (m s ²) s ²) Wind speed over replanted forestry (m s ²)
1 1	111 <th< td=""><td>Holds PALAS PALAS PALAS RULS TAS FALAS FALAS RULS FALAS <td< td=""></td<></td></th<>	Holds PALAS PALAS PALAS RULS TAS FALAS FALAS RULS FALAS FALAS FALAS RULS FALAS <td< td=""></td<>

Height of turbines (m)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Forest dimensions		restry Are			restry Are			orestry Are			restry Are			restry Are	
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
Width of forest around felled area (m)	0	0	0	0	0	0		0	0	0	0	0	0		0
Width of felled forestry around turbine (m)	0	0	0	0	0	0		0	0	0	0	0	0		0
Tree height at construction of windfarm	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00		0.00
(m) Final Height of replanted	9.93	9.93	9.93	9.93	9.93	9.93		9.93	9.93	9.93	9.93	9.93	9.93		9.93
forestry (m) Tree height at end of windfarm life (m)	9.93	9.93	9.93	9.93	9.93	9.93		9.93	9.93	9.93	9.93	9.93	9.93		9.93
Wind speed	Fo	restry Are	a1	Fe	restry Are	a 2	F	prestry Are	a 3	Fo	erestry Are	a 4	Fo	restry Are	a 5
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
forestry at hub height (m s ²) Wind speed at back of forest at hub height (m s ²) Wind speed over felled bare ground at hub height (m s ²) Wind speed over	back of fo	back of fo	back of fo	rback of fo	back of fo	back of fo	back of fo	rback of for d in felled g	back of fo	back of for 3 in felled g	back of fo	back of fo	rback of for of in felled o	back of fo 3 in felled (back of 1 in felle
replanted forestry at hub height (m s ⁻²)	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replant
Wind speed ratios	Fo	restry Are	a 1	Fo	restry Are		FC	orestry Are	a 3	Fo		a 4	Fo	restry Are	a 5
(used in worksheet 1)	Exp	Min	Max	Exp	Min	Max	Exo	Min	Max	Exp	Min	Max	Ехр	Min	Max
Standard Forestry Practice No felling	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALU
Felled Felled & replanted	#VALUE!				#VALUE!		#VALUE! #VALUE!		#VALUE! #VALUE!	#VALUE!	#VALUE! #VALUE!		#VALUE!	#VALUE! #VALUE!	#VALU #VALU
BACKGROUND CALCU		Forestry Area			Forestry Area			Forestry Area			Forestry Area			orestry Area	
Roughness of upstream ground	Exp	Min	Max	Exp	Min	Max	Ехр	Min	Max	Exp	Min	Max	Exp	Min	Max
(m)	0.03	0.03	0.03	0.03	0.03	0.03		0.03	0.03	0.03	0.03	0.03	0.03		0.03
Roughness of ground in gap (m)		0.03	0.03	0.03	0.03	0.03		0.03	0.03	0.03	0.03	0.03	0.03		0.03
Roughness of forest (m) Roughness of SRF (m)	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75	0.75
Sero plane displacement over prest (m)	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46	6.46
Sero plane displacement over SRF (m)	6.46	6.46	6.46	6.46	6.46	6.46		6.46	6.46	6.46	6.46	6.46	6.46		6.46
Exponential decay factor for wind profile in forest (alpha)	4	4	4	4	4	4		4	4	4	4	4	4		4
Maximum height of top of toundary layer (m)	5000	5000	5000	5000	5000	5000		5000	5000	5000	5000	5000	5000		5000
Von Karman's constant	0.4	0.4	0.4	0.4	0.4	0.4		0.4	0.4	0.4	0.4	0.4	0.4		0.4

Forestry Area 3 Exp Min Max

a Min Max

Forestry Area 4 Exp Min Max

Exp Min Max

Calculation of wind speed ratios_ Note: Wind speed ratios derived from WINDFLOW model (Gardinar, 2004)

> Forestry Area 1 Exp Min Max

Values taken from input sheet Age of forestry when feiled for windfarm (yr) Life time of wind farm (years) Area felled around each turbine (ha) Width of forest around felled area (m) Height of turbines (m)

19.0 19.0 <th< th=""><th>9 1149 1920 1949 1949 1949 1949 1949 1949 1949 194</th><th>1940 <th< th=""><th>1949 1948 1948 1949 1949 1949 1949 1949</th></th<></th></th<>	9 1149 1920 1949 1949 1949 1949 1949 1949 1949 194	1940 1940 <th< th=""><th>1949 1948 1948 1949 1949 1949 1949 1949</th></th<>	1949 1948 1948 1949 1949 1949 1949 1949
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22.72 2 22.73 2 22.73 2 22.74 2 22.75 2 22.76 2	12.72 2 12.73 2 12.73 2 12.74 2 12.74 2 12.75 2 12.76 2	22.72 22.7 22.73 22.7 22.73 22.7 22.74 22.7 22.75 22.7 22.76 22.7	2 22.72 3 22.73 3 22.73 4 22.74 5 22.75 8 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 2 22.73 2 22.73 2 22.74 2 22.75 2 22.76 2	2.72 22 2.73 22 2.73 22 2.74 22 2.74 22 2.75 22 2.76 22	.72 22.72 .73 22.73 .73 22.73 .74 22.74 .75 22.75 .76 22.76	22.72 22.73 22.73 22.74 22.75 22.76								22.72 22.73 22.73 22.74 22.74 22.75 22.76							22.72 22 22.73 22 22.73 22 22.74 22 22.75 22 22.76 22				22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22. 22.73 22. 22.73 22. 22.74 22. 22.75 22. 22.76 22.	72 22. 73 22. 73 22. 74 22. 75 22. 76 22.	72 22.72 73 22.73 73 22.73 74 22.74 75 22.75 76 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 22 22.73 22 22.73 22 22.74 22 22.75 22 22.76 22	1.72 22.73 1.73 22.73 1.73 22.73 1.74 22.74 1.75 22.76 1.76 22.76	22.72 22.73 22.73 22.74 22.74 22.75 22.76	22.72 22.73 22.73 22.74 22.75 22.76	22.72 2 22.73 2 22.73 2 22.74 2 22.75 2 22.76 2	22.72 22.7 22.73 22.7 22.73 22.7 22.74 22.7 22.75 22.7 22.76 22.7	2 22.75 3 22.75 3 22.75 4 22.74 5 22.76 16 22.76	72 73 .73 2.74 2.75 2.76
22.77 : 22.78 : 22.79 : 22.80 : 22.81 :	12.77 2 12.78 2 12.79 2 12.80 2 12.81 2	22.77 22.7 22.78 22.7 22.79 22.7 22.80 22.8 22.81 22.8	7 22.77 8 22.78 9 22.79 0 22.80 1 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 2 22.78 2 22.79 2 22.80 2 22.81 2 22.81 2	2.77 22 2.78 22 2.79 22 2.80 22 2.81 22	.77 22.77 .78 22.78 .79 22.79 .80 22.80 .81 22.81	22.77 22.78 22.79 22.80 22.81								22.77 22.78 22.79 22.80 22.81							22.77 22 22.78 22 22.79 22 22.80 22 22.81 22		77 22.7 78 22.7 79 22.8 80 22.8 81 22.8		22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22. 22.78 22. 22.79 22. 22.80 22. 22.81 22.	77 22. 78 22. 79 22. 80 22. 81 22.	77 22.77 78 22.78 79 22.79 .80 22.80 .81 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22 22.78 22 22.79 22 22.80 22 22.81 22	1.77 22.77 1.78 22.78 1.79 22.79 1.80 22.80 1.81 22.81	22.77 22.78 22.79 22.80 22.81	22.77 22.78 22.79 22.80 22.81	22.77 2 22.78 2 22.79 2 22.80 2 22.81 2 22.81 2	22.77 22.7 22.78 22.7 22.79 22.7 22.80 22.8 22.81 22.8	7 22.77 8 22.78 9 22.79 0 22.80 11 22.81 1 22.81	.77 .78 .79 1.80 2.81
22.83 2 22.84 2 22.84 2 22.85 2 22.85 2	12.83 2 12.84 2 12.84 2 12.85 2 12.85 2	22.83 22.8 22.84 22.8 22.84 22.8 22.85 22.8 22.85 22.8 22.86 22.8	3 22.83 4 22.84 4 22.84 5 22.85 6 22.85	22.83 22.84 22.84 22.85 22.85	22.83 22.84 22.84 22.85 22.85 22.86	22.83 2 22.84 2 22.84 2 22.85 2 22.85 2 22.85 2	2.83 22 2.84 22 2.84 22 2.85 22 2.85 22 2.85 22	.83 22.83 .84 22.84 .84 22.84 .85 22.85 .86 22.85	22.83 22.84 22.84 22.85 22.86								22.83 22.84 22.84 22.85 22.85 22.85							22.83 22 22.84 22 22.84 22 22.85 22 22.85 22 22.86 22		83 22.8 84 22.8 84 22.8 85 22.8 85 22.8 86 22.8		22.83 22.84 22.84 22.85 22.85	22.83 22.84 22.84 22.85 22.85	22.83 22.84 22.84 22.85 22.85 22.85	22.83 22.84 22.84 22.85 22.85 22.86	22.83 22.84 22.84 22.85 22.86	22.83 22. 22.84 22. 22.84 22. 22.85 22. 22.85 22.	83 22. 84 22. 84 22. 85 22. 86 22.	83 22.83 84 22.84 84 22.84 85 22.85 86 22.85	22.83 22.84 22.84 22.85 22.85 22.86	22.83 22.84 22.84 22.85 22.85	22.83 22.84 22.84 22.85 22.86	22.83 22.84 22.84 22.85 22.85	22.83 2 22.84 2 22.84 2 22.85 2 22.85 2	1.83 22.83 1.84 22.84 1.84 22.84 1.85 22.85 1.85 22.85 1.85 22.85	22.83 22.84 22.84 22.84 22.85 22.85	22.83 22.84 22.84 22.85 22.86	22.83 2 22.84 2 22.84 2 22.85 2 22.85 2	22.83 22.8 22.84 22.8 22.84 22.8 22.85 22.8 22.85 22.8	3 22.8 4 22.8 4 22.8 5 22.8 6 22.8	.83 .84 2.84 2.85 2.86
22.87 22.88 2 22.89 2 22.90 2 22.91 2 22.92 2	12.87 2 12.88 2 12.89 2 12.90 2 12.91 2 12.91 2 12.92 2	22.87 22.8 22.88 22.8 22.89 22.8 22.90 22.9 22.91 22.9 22.92 22.9	7 22.87 8 22.88 9 22.89 0 22.90 1 22.91 2 22.92	22.87 22.88 22.89 22.90 22.91 22.91	22.87 22.88 22.89 22.90 22.91 22.91 22.92	22.87 2 22.88 2 22.89 2 22.90 2 22.91 2 22.92 2	2.87 22 2.88 22 2.89 22 2.90 22 2.91 22 2.91 22 2.92 22	.87 22.87 .88 22.88 .89 22.89 .90 22.90 .91 22.91 .92 22.92	22.87 22.88 22.89 22.90 22.91 22.92								22.87 22.88 22.89 22.90 22.90 22.91 22.91							22.87 22 22.88 22 22.89 22 22.90 22 22.91 22 22.91 22 22.92 22		87 22.8 88 22.8 89 22.8 90 22.9 91 22.9 92 22.9		22.87 22.88 22.89 22.90 22.91 22.92	22.87 22.88 22.89 22.90 22.91 22.92	22.87 22.88 22.89 22.90 22.91 22.91	22.87 22.88 22.89 22.90 22.91 22.92	22.87 22.88 22.89 22.90 22.91 22.92	22.87 22. 22.88 22. 22.89 22. 22.90 22. 22.91 22. 22.91 22. 22.92 22.	87 22. 88 22. 89 22. 90 22. 91 22. 91 22.	.87 22.87 .88 22.88 .89 22.89 .90 22.90 .91 22.91 .92 22.92	22.87 22.88 22.89 22.90 22.91 22.91	22.87 22.88 22.90 22.91 22.92	22.87 22.88 22.89 22.90 22.91 22.92	22.87 22.88 22.89 22.90 22.91 22.92	22.87 22 22.88 22 22.89 22 22.90 22 22.91 22 22.92 22	1.87 22.87 1.88 22.88 1.89 22.88 1.90 22.90 1.91 22.91 1.92 22.92	22.87 22.88 22.89 22.90 22.91 22.91 22.92	22.87 22.88 22.90 22.91 22.92	22.87 2 22.88 2 22.89 2 22.90 2 22.91 2 22.91 2 22.92 2	22.87 22.8 22.88 22.8 22.89 22.8 22.90 22.9 22.91 22.9 22.92 22.9	17 22.83 18 22.85 19 22.85 10 22.90 11 22.91 12 22.92	87 .88 .89 .90 2.91 2.92
22.92 2 22.93 2 22.94 2 22.95 2 22.96 2 22.96 2	2.92 2 2.93 2 2.94 2 2.95 2 2.96 2 2.96 2	22.92 22.9 22.93 22.9 22.94 22.9 22.95 22.9 22.96 22.9 22.96 22.9	2 22.92 3 22.93 4 22.94 5 22.95 8 22.96 7 22.97	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 2 22.93 2 22.94 2 22.95 2 22.95 2 22.96 2 22.96 2	2.92 22 2.93 22 2.94 22 2.95 22 2.95 22 2.96 22	.92 22.92 .93 22.93 .94 22.94 .95 22.95 .96 22.96 .97 22.97	22.92 22.93 22.94 22.95 22.96 22.96 22.97								22.92 22.93 22.94 22.95 22.95 22.96 22.96							22.92 22 22.93 22 22.94 22 22.95 22 22.96 22 22.96 22		92 22.9 93 22.9 94 22.9 95 22.9 96 22.9		22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96 23.97	22.92 22. 22.93 22. 22.94 22. 22.95 22. 22.96 22. 22.96 22.	92 22. 93 22. 94 22. 95 22. 96 22. 96 22.	92 22.92 93 22.93 94 22.94 95 22.95 96 22.96 97 29.97	22.92 22.93 22.94 22.95 22.96 22.96 23.97	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 22 22.93 22 22.94 22 22.95 22 22.96 22 22.96 22	1.92 22.90 1.93 22.90 1.94 22.94 1.95 22.96 1.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96 22.96	22.92 22.93 22.94 22.95 22.96 22.96	22.92 2 22.93 2 22.94 2 22.95 2 22.96 2 22.96 2	22.92 22.9 22.93 22.9 22.94 22.9 22.95 22.9 22.96 22.9 22.96 22.9	2 22.90 3 22.90 4 22.94 5 22.95 6 22.96 6 22.96 7 22.90	92 93 94 95 295
22.98 2 22.98 2 22.99 2 23.00 2 23.01 2	12.98 2 12.98 2 12.99 2 13.00 2 13.01 2	22.98 22.9 22.98 22.9 22.99 22.9 23.00 23.0 23.01 23.0	8 22.98 8 22.98 9 22.99 0 23.00 1 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 2 22.98 2 22.99 2 23.00 2 23.01 2	2.98 22 2.98 22 2.99 22 3.00 23 3.01 23	.98 22.98 .98 22.98 .99 22.99 .00 23.00 .01 23.01	22.98 22.98 22.99 23.00 23.01								22.98 22.98 22.99 22.99 23.00 23.01							22.98 22 22.98 22 22.99 22 23.00 23 23.01 23		98 22.9 98 22.9 99 22.9 00 23.0 01 23.0		22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22. 22.98 22. 22.99 22. 23.00 23. 23.01 23.	98 22. 98 22. 99 22. 99 23. 00 23. 01 23.	98 22.98 98 22.98 99 22.99 99 22.99 00 23.00 01 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 22 22.98 22 22.99 22 23.00 22 23.01 22	1.98 22.98 1.98 22.98 1.99 22.99 1.00 23.00 1.01 23.01	22.98 22.98 22.99 22.99 23.00 23.01	22.98 22.98 22.99 23.00 23.01	22.98 2 22.98 2 22.99 2 23.00 2 23.01 2	22.98 22.9 22.98 22.9 22.99 22.9 23.00 23.0 23.01 23.0	6 22.98 8 22.98 9 22.95 0 22.95 10 23.00 11 23.01	.98 .98 .99 .00 3.01
23.02 23.03 2 23.03 2 23.04 2 23.05 2 23.06 2	13.02 2 13.03 2 13.03 2 13.04 2 13.05 2 13.06 2	23.02 23.0 23.03 23.0 23.03 23.0 23.04 23.0 23.05 23.0 23.06 23.0	2 23.02 3 23.03 3 23.03 4 23.04 5 23.05 6 23.06	23.02 23.03 23.04 23.05 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 2 23.03 2 23.03 2 23.04 2 23.04 2 23.05 2 23.06 2	3.02 23 3.03 23 3.03 23 3.04 23 3.04 23 3.05 23 3.06 23	.02 23.02 .03 23.03 .03 23.03 .04 23.04 .05 23.05 .06 23.06	23.02 23.03 23.03 23.04 23.04 23.05 23.06								2 23.02 23.03 23.03 23.04 23.04 5 23.05 23.06							23.02 23 23.03 23 23.03 23 23.04 23 23.05 23 23.06 23		02 23.0 03 23.0 03 23.0 04 23.0 05 23.0 06 23.0		23.02 23.03 23.04 23.05 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 23.03 23.04 23.05 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 23. 23.03 23. 23.03 23. 23.04 23. 23.04 23. 23.05 23. 23.06 23.	02 23. 03 23. 03 23. 04 23. 05 23. 06 23.	.02 23.02 .03 23.03 .03 23.03 .04 23.04 .05 23.05 .06 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 23.03 23.04 23.04 23.05 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 2 23.03 2 23.03 2 23.04 2 23.05 2 23.06 2	1.02 23.02 1.03 23.03 1.04 23.04 1.05 23.05 1.06 23.06	23.02 23.03 23.03 23.04 23.05 23.06	23.02 23.03 23.04 23.04 23.05 23.06	23.02 2 23.03 2 23.03 2 23.04 2 23.05 2 23.06 2	23.02 23.0 23.03 23.0 23.03 23.0 23.04 23.0 23.05 23.0 23.06 23.0	2 23.00 3 23.00 3 23.00 4 23.04 5 23.05 6 23.06	02 .03 .03 .04 3.05 3.06
23.07 : 23.08 : 23.08 : 23.09 : 23.10 : 23.10 :	13.07 2 13.08 2 13.08 2 13.09 2 13.10 2	23.07 23.0 23.08 23.0 23.08 23.0 23.09 23.0 23.10 23.1 23.10 23.1	7 23.07 8 23.08 8 23.08 9 23.09 0 23.10 1 23.11	23.07 23.08 23.09 23.10 23.10	23.07 23.08 23.08 23.09 23.10 23.11	23.07 2 23.08 2 23.08 2 23.09 2 23.10 2 23.11 2	3.07 23 3.08 23 3.08 23 3.09 23 3.10 23 3.10 23	.07 23.07 .08 23.08 .09 23.09 .10 23.10 11 23.10	23.07 23.08 23.08 23.09 23.10 23.10								23.07 23.08 23.08 23.09 23.10 23.10							23.07 23 23.08 23 23.08 23 23.09 23 23.09 23 23.10 23 29.11 23		07 23.0 08 23.0 08 23.0 09 23.0 10 23.1		23.07 23.08 23.09 23.10 23.11	23.07 23.08 23.08 23.09 23.10 23.11	23.07 23.08 23.08 23.09 23.10 23.11	23.07 23.08 23.08 23.09 23.10 23.11	23.07 23.08 23.08 23.09 23.10 23.11	23.07 23. 23.08 23. 23.08 23. 23.09 23. 23.10 23. 23.10 23.	07 23. 08 23. 08 23. 09 23. 10 23.	.07 23.07 .08 23.08 .08 23.08 .09 23.09 .10 23.10	23.07 23.08 23.08 23.09 23.10 23.10	23.07 23.08 23.08 23.09 23.10 23.11	23.07 23.08 23.08 23.09 23.10 23.11	23.07 23.08 23.09 23.10 23.11	23.07 22 23.08 22 23.08 22 23.09 22 23.10 22 23.10 22	L07 23.05 L08 23.06 L08 23.06 L09 23.06 L09 23.05 L10 23.10	23.07 23.08 23.09 23.09 23.10 23.11	23.07 23.08 23.08 23.09 23.10 23.11	23.07 2 23.08 2 23.08 2 23.09 2 23.10 2 23.10 2	23.07 23.0 23.08 23.0 23.08 23.0 23.09 23.0 23.10 23.1 23.10 23.1	7 23.05 8 23.08 8 23.08 9 23.08 9 23.05 0 23.10 1 23.11	07 .08 .08 .09 3.10
23.12 23.12 23.13 23.14 23.15	13.12 2 13.12 2 13.13 2 13.14 2 13.14 2	23.12 23.1 23.12 23.1 23.13 23.1 23.14 23.1 23.15 23.1	2 23.12 2 23.12 3 23.13 4 23.14 5 23.15		23.12 23.12 23.13 23.14 23.15	23.12 2 23.12 2 23.13 2 23.14 2 23.15 2	3.12 23 3.12 23 3.13 23 3.14 23 3.15 23	.12 23.12 .12 23.12 .13 23.13 .14 23.14 .15 23.15	23.12 23.12 23.13 23.14 23.15								23.12 23.12 23.13 23.14 23.14 23.15											23.12 23.12 23.13 23.14 23.15		23.12 23.12 23.13 23.14 23.15			23.12 23. 23.12 23. 23.13 23. 23.14 23. 23.15 23.	12 23. 12 23. 13 23. 14 23. 15 23.				23.12 23.12 23.13 23.14 23.15	23.12 23.12 23.13 23.14 23.15	23.12 2 23.12 2 23.13 2 23.14 2 23.15 2	1.12 23.12 1.12 23.12 1.13 23.13 1.14 23.14 1.15 23.15	23.12 23.12 23.13 23.14 23.14 23.15	23.12 23.12 23.13 23.14 23.15	23.12 2 23.12 2 23.13 2 23.14 2 23.15 2	23.12 23.1 23.12 23.1 23.13 23.1 23.14 23.1 23.15 23.1	2 23.12 2 23.12 3 23.13 4 23.14 5 23.14	.12 .12 .13 .14 8.15
13.16 13.16 13.17 13.18 13.19 13.19	13.16 2 13.16 2 13.17 2 13.18 2 13.19 2 13.19 2	23.16 23.1 23.16 23.1 23.17 23.1 23.18 23.1 23.19 23.1 23.19 23.1 23.19 23.1	6 23.16 6 23.16 7 23.17 8 23.18 9 23.19 9 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19 23.19	23.16 2 23.16 2 23.17 2 23.18 2 23.19 2 23.19 2	3.16 23 3.16 23 3.17 23 3.18 23 3.19 23 3.19 23	.16 23.16 .16 23.16 .17 23.17 .18 23.18 .19 23.19 .19 23.19	23.16 23.16 23.17 23.18 23.19 23.19 23.19			23.16 23.16 23.17 23.18 23.19 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19 23.19				23.16 23.16 23.17 23.17 23.18 23.19 23.19 23.19							23.16 23 23.16 23 23.17 23 23.18 23 23.19 23 23.19 23 23.19 23				23.16 23.16 23.17 23.18 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 23. 23.16 23. 23.17 23. 23.18 23. 23.19 23. 23.19 23. 23.19 23.	16 23. 16 23. 17 23. 18 23. 19 23. 19 23.	.16 23.16 .16 23.16 .17 23.17 .18 23.18 .19 23.19 .19 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 23.17 23.18 23.19 23.19	23.16 2 23.16 2 23.17 2 23.18 2 23.19 2 23.19 2	1.16 23.16 1.16 23.16 1.17 23.11 1.18 23.18 1.19 23.15 1.19 23.15	23.16 23.16 23.17 23.18 23.19 23.19 23.19	23.16 23.16 23.17 23.18 23.19 23.19	23.16 2 23.16 2 23.17 2 23.18 2 23.19 2 23.19 2	23.16 23.1 23.16 23.1 23.17 23.1 23.18 23.1 23.19 23.1 23.19 23.1	6 23.16 6 23.16 7 23.17 8 23.18 9 23.15 9 23.15	16 .16 .17 .18 3.19 3.19
23.20 : 23.21 : 23.22 : 23.23 : 23.23 : 23.23 :	13.20 2 13.21 2 13.22 2 13.23 2 13.23 2 13.23 2	23.20 23.2 23.21 23.2 23.22 23.2 23.23 23.2 23.23 23.2 23.23 23.2 23.23 23.2	0 23.20 1 23.21 2 23.22 3 23.23 3 23.23 3 23.23	23.20 23.21 23.22 23.23 23.23 23.23	23.20 23.21 23.22 23.23 23.23 23.23	23.20 2 23.21 2 23.22 2 23.23 2 23.23 2 23.23 2 23.23 2 23.24 2	3.20 23 3.21 23 3.22 23 3.23 23 3.23 23 3.23 23	20 2320 21 2321 22 2322 23 2323 23 2323 24 2324	23.20 23.21 23.22 23.23 23.23 23.23 23.23								23.20 23.21 23.22 23.23 23.23 23.23 23.23 23.23 23.23											23.20 23.21 23.22 23.23 23.23 23.23	23.20 23.21 23.22 23.23 23.23 23.23 23.23	23.20 23.21 23.22 23.23 23.23 23.23	23.20 23.21 23.22 23.23 23.23 23.23 23.24	23.20 23.21 23.22 23.23 23.23 23.23 23.23	23.20 23. 23.21 23. 23.22 23. 23.23 23. 23.23 23. 23.23 23.	20 23. 21 23. 22 23. 23 23. 23 23. 23 23. 24 29	20 23.20 21 23.21 22 23.22 23 23.23 23 23.23 23 23.23 24 29.24	2320 2321 2322 2323 2323 2323	23.20 23.21 23.22 23.23 23.23 23.23	2320 2321 2322 2323 2323 2323 2324	23.20 23.21 23.22 23.23 23.23 23.23 23.24	23.20 2 23.21 2 23.22 2 23.23 2 23.23 2 23.23 2 23.23 2 23.24 2	1.20 23.20 1.21 23.21 1.22 23.22 1.23 23.22 1.23 23.22 1.23 23.22	23.20 23.21 23.22 23.23 23.23 23.23 23.23	23.20 23.21 23.22 23.23 23.23 23.23	23.20 2 23.21 2 23.22 2 23.23 2 23.23 2 23.23 2 23.23 2 23.24 2	23.20 23.2 23.21 23.2 23.22 23.2 23.23 23.2 23.23 23.2 23.23 23.2 23.23 23.2	0 23.20 11 23.21 12 23.22 13 23.22 13 23.23 13 23.23 14 23.20	20 21 22 23 23 23
23.25 23.26 23.26 23.27 23.27	13.25 2 13.26 2 13.26 2 13.27 2 13.27 2	23.25 23.2 23.26 23.2 23.26 23.2 23.26 23.2 23.27 23.2 23.28 23.2	5 23.25 6 23.26 6 23.26 7 23.27 8 23.28	23.25 23.26 23.26 23.26 23.27 23.28	23.25 23.26 23.26 23.27 23.27 23.28	23.25 2 23.26 2 23.26 2 23.26 2 23.27 2 23.27 2 23.28 2	3.25 23 3.26 23 3.26 23 3.26 23 3.27 23 3.28 23	25 2325 26 2326 26 2326 27 2327 28 2328	23.25 23.26 23.26 23.27 23.27 23.28								23.25 23.26 23.26 23.26 23.27 23.28									25 23.2 26 23.2 26 23.2 26 23.2 27 23.2 28 23.2		23.25 23.26 23.26 23.27 23.27 23.28	23.25 23.26 23.26 23.27 23.27 23.28	23.25 23.26 23.26 23.27 23.27 23.28	2325 2326 2326 2327 2328	23.25 23.26 23.26 23.27 23.28	23.25 23. 23.26 23. 23.26 23. 23.26 23. 23.27 23. 23.28 23.	25 23. 26 23. 26 23. 26 23. 27 23. 28 23.	25 23.25 26 23.26 26 23.26 26 23.26 27 23.27 28 23.28	2325 2326 2326 2327 2327 2328	23.25 23.26 23.26 23.27 23.27 23.28	2325 2326 2326 2327 2327 2328	23.25 23.26 23.26 23.27 23.27 23.28	23.25 2 23.26 2 23.26 2 23.27 2 23.27 2 23.28 2	1.25 23.25 1.26 23.26 1.26 23.26 1.26 23.26 1.27 23.27 1.28 23.26	23.25 23.26 23.26 23.26 23.27 23.27 23.28	23.25 23.26 23.26 23.27 23.27 23.28	23.25 2 23.26 2 23.26 2 23.26 2 23.27 2 23.27 2 23.28 2	23.25 23.2 23.26 23.2 23.26 23.2 23.26 23.2 23.26 23.2 23.27 23.2 23.28 23.2	5 23.25 5 23.26 6 23.26 6 23.26 7 23.27 8 23.26	25 26 26 326 327 328
23.29 23.29 23.30 23.31 23.32 23.32 23.32	13.29 2 13.29 2 13.30 2 13.31 2 13.32 2 13.32 2	23.29 23.2 23.29 23.2 23.30 23.3 23.31 23.3 23.32 23.3 23.32 23.3 23.32 23.3	9 23.29 9 23.29 0 23.30 1 23.31 2 23.32 2 23.32	23.29 23.29 23.30 23.31 23.32 23.32	23.29 23.29 23.30 23.31 23.32 23.32 23.32	23.29 2 23.29 2 23.30 2 23.31 2 23.32 2 23.32 2 23.32 2	3.29 23 3.29 23 3.30 23 3.31 23 3.32 23 3.32 23	29 2329 29 2329 30 2330 31 2331 32 2332 32 2332	23.29 23.29 23.30 23.31 23.32 23.32								23.29 23.29 23.30 23.30 23.31 23.32 23.32 23.32							23.29 23 23.29 23 23.30 23 23.31 23 23.32 23 23.32 23 23.32 23		29 23.2 29 23.2 30 23.3 31 23.3 32 23.3 32 23.3 32 23.3		23.29 23.29 23.30 23.31 23.32 23.32	23.29 23.29 23.30 23.31 23.32 23.32 23.32	23.29 23.29 23.30 23.31 23.32 23.32 23.32	2329 2329 2330 2331 2332 2332 2332	23.29 23.29 23.30 23.31 23.32 23.32 23.32	23.29 23. 23.29 23. 23.30 23. 23.31 23. 23.32 23. 23.32 23.	29 23. 29 23. 30 23. 31 23. 32 23. 32 23.	29 23.29 29 23.29 30 23.30 31 23.31 32 23.32 32 23.32	2329 2329 2330 2331 2332 2332	23.29 23.29 23.30 23.31 23.32 23.32 23.32	2329 2329 2330 2331 2332 2332 2332	23.29 23.29 23.30 23.31 23.32 23.32	23.29 2 23.29 2 23.30 2 23.31 2 23.32 2 23.32 2	129 23.23 129 23.23 1.30 23.33 1.31 23.31 1.32 23.33 1.32 23.33 1.32 23.33	23.29 23.29 23.30 23.31 23.32 23.32 23.32	23.29 23.29 23.30 23.31 23.32 23.32 23.32	23.29 2 23.29 2 23.30 2 23.31 2 23.32 2 23.32 2 23.32 2	23.29 23.2 23.29 23.2 23.30 23.3 23.31 23.3 23.32 23.3 23.32 23.3	9 23.23 9 23.23 0 23.30 11 23.31 12 23.33 12 23.33 12 23.33	29 .29 .30 .31 3.32 3.32
23.33 23.34 23.35 23.35 23.35 23.35 23.35 23.36 23.37	13.33 2 13.34 2 13.35 2 13.35 2 13.36 2 13.37 2	23.33 23.3 23.34 23.3 23.35 23.3 23.35 23.3 23.35 23.3 23.36 23.3 23.37 23.3	3 23.33 4 23.34 5 23.35 5 23.35 6 23.36 7 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 2 23.34 2 23.35 2 23.35 2 23.35 2 23.36 2 23.36 2 23.37 2	3.33 23 3.34 23 3.35 23 3.35 23 3.35 23 3.36 23 3.37 23	.33 23.33 .34 23.34 .35 23.35 .35 23.35 .36 23.36 .37 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37								23.33 23.34 23.35 23.35 23.35 23.36 23.36 23.37							23.33 23 23.34 23 23.35 23 23.35 23 23.35 23 23.36 23 23.36 23 23.37 23		33 23.3 34 23.3 35 23.3 35 23.3 36 23.3 37 23.3		23.33 23.34 23.35 23.35 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.37	23.33 23.34 23.35 23.35 23.35 23.36 23.37	23.33 23. 23.34 23. 23.35 23. 23.35 23. 23.35 23. 23.36 23. 23.37 23.	33 23. 34 23. 35 23. 35 23. 36 23. 36 23. 37 23.	.33 23.33 .34 23.34 .35 23.35 .35 23.35 .36 23.36 .37 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 23.34 23.35 23.35 23.35 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 22 23.34 22 23.35 22 23.35 22 23.35 22 23.36 22 23.37 22	1.33 23.33 1.34 23.34 1.35 23.38 1.35 23.38 1.36 23.38 1.36 23.38	23.33 23.34 23.35 23.35 23.35 23.36 23.36 23.37	23.33 23.34 23.35 23.35 23.36 23.36 23.37	23.33 2 23.34 2 23.35 2 23.35 2 23.35 2 23.36 2 23.36 2 23.37 2	23.33 23.3 23.34 23.3 23.35 23.3 23.35 23.3 23.36 23.3 23.36 23.3 23.37 23.3	3 23.33 4 23.34 5 23.35 6 23.35 6 23.36 6 23.36 7 23.35	33 34 .35 1.35 3.36 3.37
23.38 2 23.38 2 23.39 2 23.40 2 23.40 2	13.38 2 13.38 2 13.39 2 13.40 2 13.40 2	23.38 23.3 23.38 23.3 23.39 23.3 23.40 23.4 23.40 23.4 23.40 23.4	8 23.38 8 23.38 9 23.39 0 23.40 0 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 2 23.38 2 23.39 2 23.40 2 23.40 2 23.40 2	3.38 23 3.38 23 3.39 23 3.40 23 3.40 23	.38 23.38 .38 23.38 .39 23.39 .40 23.40 .40 23.40	23.38 23.38 23.39 23.40 23.40 23.40			23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40				23.38 23.38 23.39 23.40 23.40 23.40							23.38 23 23.38 23 23.39 23 23.40 23 23.40 23 23.40 23		38 23.3 38 23.3 39 23.3 40 23.4 40 23.4		23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23. 23.38 23. 23.39 23. 23.40 23. 23.40 23. 23.40 23. 23.40 23.	38 23. 38 23. 39 23. 40 23. 40 23.	38 23.38 38 23.38 39 23.39 40 23.40 40 23.40	23.38 23.38 23.39 23.40 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 2 23.38 2 23.39 2 23.40 2 23.40 2 23.40 2	1.38 23.38 1.38 23.38 1.39 23.33 1.40 23.40 1.40 23.40	23.38 23.38 23.39 23.40 23.40 23.40	23.38 23.38 23.39 23.40 23.40	23.38 2 23.38 2 23.39 2 23.40 2 23.40 2 23.40 2	23.38 23.3 23.38 23.3 23.39 23.3 23.40 23.4 23.40 23.4 23.40 23.4	8 23.38 8 23.38 9 23.38 0 23.40 0 23.40 0 23.40	38 38 39 1.40 3.40
23.41 23.42 23.43 23.43 23.44 23.44 23.45	13.41 2 13.42 2 13.43 2 13.43 2 13.44 2 13.45 2	23.41 23.4 23.42 23.4 23.43 23.4 23.43 23.4 23.44 23.4 23.45 23.4	23.41 2 23.42 3 23.43 3 23.43 4 23.44 5 23.45	23.41 23.42 23.43 23.43 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.45	23.41 2 23.42 2 23.43 2 23.43 2 23.44 2 23.44 2 23.45 2	3.41 23 3.42 23 3.43 23 3.43 23 3.44 23 3.45 23	.41 23.41 .42 23.42 .43 23.43 .43 23.43 .44 23.44 .45 23.45	23,41 23,42 23,43 23,43 23,44 23,45			23.41 23.42 23.43 23.43 23.44 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.45				23.41 23.42 23.43 23.43 23.43 23.44 5 23.45							23,41 23 23,42 23 23,43 23 23,43 23 23,44 23 23,45 23		41 23.4 42 23.4 43 23.4 43 23.4 44 23.4 45 23.4		23.41 23.42 23.43 23.43 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.45	23.41 23. 23.42 23. 23.43 23. 23.43 23. 23.44 23. 23.45 23.	41 23. 42 23. 43 23. 43 23. 44 23. 45 23.	41 23.41 42 23.42 43 23.43 43 23.43 44 23.44 45 23.45	23,41 23,42 23,43 23,43 23,44 23,45	23.41 23.42 23.43 23.43 23.44 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.45	23.41 23.42 23.43 23.43 23.44 23.45	23.41 2 23.42 2 23.43 2 23.43 2 23.44 2 23.45 2	141 23,41 142 23,42 143 23,43 143 23,43 144 23,44 145 23,44	23.41 23.42 23.43 23.43 23.44 5 23.45	23.41 23.42 23.43 23.43 23.44 23.44 23.45	23.41 2 23.42 2 23.43 2 23.43 2 23.44 2 23.45 2	23.41 23.4 23.42 23.4 23.43 23.4 23.43 23.4 23.44 23.4 23.45 23.4	2 23.40 2 23.42 3 23.43 3 23.43 4 23.44 5 23.44	42 ,43 1,43 1,44 3,45
23.45 23.46 23.47 23.47 23.47 23.48 23.49	13.45 2 13.46 2 13.47 2 13.47 2 13.48 2 13.48 2	23.45 23.4 23.46 23.4 23.47 23.4 23.47 23.4 23.48 23.4 23.48 23.4 23.49 23.4	5 23.45 6 23.46 7 23.47 7 23.47 8 23.48 9 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 2 23.46 2 23.47 2 23.47 2 23.47 2 23.48 2 23.49 2	3.45 23 3.46 23 3.47 23 3.47 23 3.48 23 3.49 23	.45 23.45 .46 23.46 .47 23.47 .47 23.47 .48 23.48 .49 23.49	23.45 23.46 23.47 23.47 23.47 23.48 23.49								23.45 23.46 23.47 23.47 23.47 23.48 23.49							23.45 23 23.46 23 23.47 23 23.47 23 23.47 23 23.48 23 23.49 23		45 23.4 46 23.4 47 23.4 47 23.4 48 23.4 48 23.4 49 23.4		23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23. 23.46 23. 23.47 23. 23.47 23. 23.48 23. 23.48 23. 23.49 23.	45 23. 46 23. 47 23. 47 23. 48 23. 49 23.	45 23.45 46 23.46 47 23.47 47 23.47 48 23.48 49 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 22 23.46 22 23.47 22 23.47 22 23.48 22 23.48 22 23.49 22	1.45 23.46 1.46 23.46 1.47 23.47 1.47 23.47 1.48 23.48 1.49 23.46	23.45 23.46 23.47 23.47 23.47 23.48 23.49	23.45 23.46 23.47 23.47 23.48 23.49	23.45 2 23.46 2 23.46 2 23.47 2 23.47 2 23.48 2 23.49 2 23.50 2 23.50 2 23.50 2 23.50 2 23.51 2 23.52 2	23.45 23.4 23.46 23.4 23.47 23.4 23.47 23.4 23.48 23.4 23.48 23.4 23.49 23.4	5 23.45 6 23.46 7 23.47 7 23.47 8 23.48 9 23.45	45 46 .47 1.47 3.48 3.49
23.50 23.50 23.51 23.52 23.52 23.52	13.50 2 13.50 2 13.51 2 13.52 2 13.52 2	23.50 23.5 23.50 23.5 23.51 23.5 23.52 23.5 23.52 23.5 23.52 23.5	0 23.50 0 23.50 1 23.51 2 23.52 2 23.52 2 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 2 23.50 2 23.51 2 23.52 2 23.52 2 23.52 2	3.50 23 3.50 23 3.51 23 3.52 23 3.52 23 3.52 23 3.52 23	.50 23.50 .50 23.50 .51 23.51 .52 23.52 .52 23.52	23.50 23.50 23.51 23.52 23.52 23.52								23.50 23.50 23.51 23.52 23.52 23.52 23.52							23.50 23 23.50 23 23.51 23 23.52 23 23.52 23 23.52 23				23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23. 23.50 23. 23.51 23. 23.52 23. 23.52 23.	50 23. 50 23. 51 23. 52 23. 52 23.	50 23.50 50 23.50 51 23.51 52 23.52 52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52	23.50 2 23.50 2 23.51 2 23.52 2 23.52 2 23.52 2	1.50 23.50 1.50 23.50 1.51 23.51 1.52 23.52 1.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 23.50 23.51 23.52 23.52 23.52	23.50 2 23.50 2 23.51 2 23.52 2 23.52 2 23.52 2	23.50 23.5 23.50 23.5 23.51 23.5 23.52 23.5 23.52 23.5 23.52 23.5	0 23.50 0 23.50 11 23.51 12 23.52 12 23.52 12 23.52	.50 .51 1.52 1.52
23.54 23.54 23.55 23.56 23.56	13.54 2 13.54 2 13.55 2 13.56 2 13.56 2	23.54 23.5 23.54 23.5 23.55 23.5 23.56 23.5 23.56 23.5	4 23.54 4 23.54 5 23.55 8 23.56 8 23.56	23.54 23.54 23.55 23.56 23.56	23.54 23.54 23.55 23.56 23.56	23.54 2 23.54 2 23.55 2 23.56 2 23.56 2 23.56 2	3.54 23 3.54 23 3.55 23 3.56 23 3.56 23 3.56 23	.54 23.54 .54 23.54 .55 23.55 .56 23.56 .56 23.56	23.54 23.54 23.55 23.56 23.56								23.54 23.54 23.55 23.56 23.56 23.56							23.54 23 23.54 23 23.55 23 23.56 23 23.56 23		54 23.5 54 23.5 55 23.5 56 23.5 56 23.5		23.54 23.54 23.55 23.56 23.56	23.54 23.54 23.55 23.56 23.56	23.54 23.54 23.55 23.56 23.56 23.56	23.54 23.54 23.55 23.56 23.56	23.54 23.54 23.55 23.56 23.56	23.55 23. 23.54 23. 23.55 23. 23.56 23. 23.56 23.	54 23. 54 23. 55 23. 56 23. 56 23.	.54 23.54 .54 23.54 .55 23.55 .56 23.56 .56 23.56	23.54 23.54 23.55 23.56 23.56	23.54 23.54 23.55 23.56 23.56	2355 2354 2355 2356 2356 2356	23.54 23.54 23.55 23.56 23.56	23.54 2 23.54 2 23.55 2 23.56 2 23.56 2	1.54 23.54 1.54 23.54 1.55 23.56 1.56 23.56 1.56 23.56	23.54 23.54 23.55 23.56 23.56	23.54 23.54 23.55 23.56 23.56	23.54 2 23.54 2 23.55 2 23.55 2 23.56 2 23.56 2	23.54 23.5 23.54 23.5 23.55 23.5 23.56 23.5 23.56 23.5	4 23.5 4 23.5 5 23.5 6 23.5 6 23.5	.54 .54 .55 .56 3.56
23.57 23.58 23.58 23.59 23.60 23.60	13.57 2 13.58 2 13.58 2 13.59 2 13.60 2 13.60 2	23.57 23.5 23.58 23.5 23.58 23.5 23.59 23.5 23.60 23.6 23.60 23.6	7 23.57 8 23.58 8 23.58 9 23.59 0 23.60 0 23.60	23.57 23.58 23.59 23.60 23.60	23.57 23.58 23.59 23.60 23.60 23.60	23.57 2 23.58 2 23.58 2 23.59 2 23.60 2 23.60 2	3.57 23 3.58 23 3.58 23 3.59 23 3.60 23 3.60 23	.57 23.57 .58 23.58 .58 23.58 .59 23.59 .60 23.60 .60 23.60	23.57 23.58 23.59 23.60 23.60 23.60			23.57 23.58 23.58 23.59 23.60 23.60	23.57 23.58 23.59 23.60 23.60 23.60				23.57 23.58 23.58 23.59 23.60 23.60 23.60							23.57 23 23.58 23 23.58 23 23.59 23 23.60 23 23.60 23 23.60 23		57 23.5 58 23.5 58 23.5 59 23.5 60 23.6 60 23.6		23.57 23.58 23.59 23.60 23.60	23.57 23.58 23.59 23.60 23.60 23.60	23.57 23.58 23.58 23.59 23.60 23.60	23.57 23.58 23.58 23.59 23.60 23.60 23.60	23.57 23.58 23.59 23.60 23.60 23.60	23.57 23. 23.58 23. 23.58 23. 23.59 23. 23.60 23. 23.60 23.	57 23. 58 23. 58 23. 59 23. 60 23. 60 23.	57 23.57 58 23.58 58 23.58 59 23.59 60 23.60 60 23.60	23.57 23.58 23.59 23.60 23.60	23.57 23.58 23.58 23.59 23.60 23.60	2357 2358 2358 2359 2360 2360	23.57 23.58 23.59 23.60 23.60	23.57 2 23.58 2 23.58 2 23.59 2 23.60 2 23.60 2	1.57 23.51 1.58 23.58 1.59 23.58 1.59 23.56 1.60 23.60 1.60 23.60	23.57 23.58 23.58 23.59 23.60 23.60 23.60	23.57 23.58 23.59 23.60 23.60 23.60	23.57 2 23.58 2 23.58 2 23.59 2 23.60 2 23.60 2	23.57 23.5 23.58 23.5 23.58 23.5 23.59 23.5 23.60 23.6 23.60 23.6	7 23.5 8 23.5 8 23.5 8 23.5 9 23.5 0 23.6 0 23.6	57 58 58 59 3.60 3.60
23.61 : 23.62 : 23.62 : 23.63 : 23.64 : 23.64 :	13.61 2 13.62 2 13.62 2 13.63 2 13.64 2 13.64 2	23.61 23.6 23.62 23.6 23.62 23.6 23.63 23.6 23.64 23.6 23.64 23.6	1 23.61 2 23.62 2 23.62 3 23.63 4 23.64 4 23.64	23.61 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.63 23.63 23.64 23.64	23.61 2 23.62 2 23.62 2 23.63 2 23.64 2 23.64 2	3.61 23 3.62 23 3.62 23 3.63 23 3.64 23 3.64 23	.61 23.61 .62 23.62 .62 23.62 .63 23.63 .64 23.64 .64 23.64	23.61 23.62 23.62 23.63 23.63 23.64 23.64			23.61 23.62 23.62 23.63 23.63 23.64 23.64				61 23.6 62 23.6 62 23.6 63 23.6 64 23.6 64 23.6	23.61 23.62 23.62 23.63 23.63 23.64 23.64	23.61 23.62 23.63 23.63 23.64 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64	23.61 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 2 23.62 2 23.62 2 23.63 2 23.64 2 23.64 2	23.61 23 23.62 23 23.62 23 23.63 23 23.64 23 23.64 23 23.64 23		61 23.6 62 23.6 62 23.6 63 23.6 64 23.6 64 23.6		23.61 23.62 23.63 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 23. 23.62 23. 23.62 23. 23.63 23. 23.64 23. 23.64 23.	61 23. 62 23. 62 23. 63 23. 64 23. 64 23.	.61 23.61 .62 23.62 .62 23.62 .63 23.63 .64 23.64 .64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 23.62 23.63 23.63 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64	23.61 22 23.62 22 23.62 22 23.63 22 23.64 22 23.64 22	1.61 23.61 1.62 23.62 1.62 23.62 1.63 23.63 1.64 23.64 1.64 23.64	23.61 23.62 23.63 23.63 23.64 23.64 23.64	23.61 23.62 23.62 23.63 23.64 23.64 23.64	23.61 2 23.62 2 23.62 2 23.63 2 23.64 2 23.64 2	23.61 23.6 23.62 23.6 23.62 23.6 23.63 23.6 23.64 23.6 23.64 23.6	11 23.61 12 23.62 12 23.63 13 23.63 14 23.64 14 23.64	61 62 62 63 63 64 3.64
23.65 23.66 23.66 23.67 23.68	13.65 2 13.66 2 13.66 2 13.67 2 13.68 2	23.65 23.6 23.66 23.6 23.66 23.6 23.67 23.6 23.68 23.6	5 23.65 8 23.66 6 23.66 7 23.67 8 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 2 23.66 2 23.66 2 23.67 2 23.68 2	3.65 23 3.66 23 3.66 23 3.67 23 3.68 23	.65 23.65 .66 23.66 .66 23.66 .67 23.67 .68 23.68	23.65 23.66 23.66 23.67 23.68								23.65 23.66 23.66 23.66 23.67 23.67							23.65 23 23.66 23 23.66 23 23.66 23 23.67 23 23.68 23		65 23.6 66 23.6 66 23.6 67 23.6 68 23.6		23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23. 23.66 23. 23.66 23. 23.67 23. 23.67 23.	65 23. 66 23. 66 23. 67 23. 68 23.	.65 23.65 .66 23.66 .66 23.66 .67 23.67 .68 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 2 23.66 2 23.66 2 23.67 2 23.68 2	1.65 23.66 1.66 23.66 1.66 23.66 1.67 23.67 1.68 23.68	23.65 23.66 23.66 23.67 23.67 23.68	23.65 23.66 23.66 23.67 23.68	23.65 2 23.66 2 23.66 2 23.66 2 23.67 2 23.68 2	23.65 23.6 23.66 23.6 23.66 23.6 23.67 23.6 23.68 23.6	6 23.66 6 23.66 6 23.66 7 23.66 8 23.66	.65 .66 .66 .67 3.68
23.69 23.69 23.70 23.71 23.71 23.71	13.69 2 13.69 2 13.69 2 13.70 2 13.71 2 13.71 2	23.68 23.6 23.69 23.6 23.69 23.6 23.70 23.7 23.71 23.7 23.71 23.7 23.71 23.7	23.68 23.69 23.69 23.70 1 23.71 1 23.71	23.68 23.69 23.69 23.70 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71	23.68 2 23.69 2 23.69 2 23.70 2 23.71 2 23.71 2	3.69 23 3.69 23 3.69 23 3.70 23 3.71 23 3.71 23	23.68 23.68 .69 23.69 .69 23.69 .70 23.70 .71 23.71 .71 23.71	23.68 23.69 23.70 23.71 23.71							23.63 23.63 69 23.61 69 23.61 70 23.71 71 23.71 71 23.71	23.68 23.69 23.69 23.70 23.71 23.71							23.69 23 23.69 23 23.69 23 23.70 23 23.71 23 23.71 23 23.71 23		es 23.6 69 23.6 69 23.6 70 23.7 71 23.7 71 23.7		23.68 23.69 23.70 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71	23.68 23. 23.69 23. 23.69 23. 23.70 23. 23.71 23. 23.71 23. 23.71 23.	68 23. 69 23. 69 23. 70 23. 71 23. 71 23.	23.68 23.69 23.69 23.69 23.69 23.69 23.69 70 23.70 71 23.71 71 23.71 71 23.71	23.68 23.69 23.69 23.70 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71 23.71	2368 2369 2369 2370 2371 2371	23.68 23.69 23.69 23.70 23.71 23.71	23.68 22 23.69 22 23.69 22 23.70 22 23.71 22 23.71 22 23.71 2	.66 23.66 1.69 23.66 1.69 23.66 1.70 23.70 1.71 23.71 1.71 <u>23.7</u>	23.68 23.69 23.69 23.70 23.71 23.71	23.68 23.69 23.69 23.70 23.71 23.71	21222 2 2253 2 2254 2 2255 2 2255 2 2255 2 2255 2 2255 2 2255 2 2255 2 2255 2 2255 2 2367 2 2369 2 2369 2 2460 2 2464 2 2464 2 2464 2 2464 2 2464 2 2464 2 2464 2 2464 2 2464 2 2466 2 2466 2 2466 2 2466 2 2466 2 2466 2 2466 2 24700 2 24700 2 24700<	23.68 23.6 23.69 23.6 23.69 23.6 23.70 23.7 23.71 23.7 23.71 23.7 23.71 23.7	8 23.68 9 23.66 9 23.66 10 23.70 11 23.71 11 23.71	69 69 69 70 71 3.71
23.72 23.73 23.73 23.74 23.75 23.75	13.72 2 13.73 2 13.73 2 13.74 2 13.75 2 13.75 2	23.72 23.7 23.73 23.7 23.73 23.7 23.74 23.7 23.75 23.7 23.75 23.7	2 23.72 3 23.73 3 23.73 4 23.74 5 23.75 5 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 2 23.73 2 23.73 2 23.74 2 23.74 2 23.75 2 23.75 2	3.72 23 3.73 23 3.73 23 3.74 23 3.75 23 3.75 23	.72 23.72 .73 23.73 .73 23.73 .74 23.74 .75 23.75 .75 23.75	23.72 23.73 23.73 23.74 23.75 23.75								2 23.72 23.73 23.73 23.74 23.74 5 23.75 5 23.75							23.72 23 23.73 23 23.73 23 23.74 23 23.75 23 23.75 23				23.72 23.73 23.73 23.74 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 23. 23.73 23. 23.73 23. 23.74 23. 23.75 23. 23.75 23. 23.75 23.	72 23. 73 23. 73 23. 74 23. 75 23. 75 23.	72 23.72 73 23.73 73 23.73 74 23.74 75 23.75 75 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75	23,72 23,73 23,73 23,74 23,75 23,75	23.72 2. 23.73 2. 23.73 2. 23.74 2. 23.75 2. 23.75 2.	1.72 23.72 1.73 23.73 1.73 23.73 1.74 23.74 1.75 23.75 1.75 23.75	23.72 23.73 23.73 23.74 23.74 23.75 23.75	23.72 23.73 23.73 23.74 23.75 23.75 23.75	23.72 2 23.73 2 23.73 2 23.74 2 23.75 2 23.75 2	23.72 23.7 23.73 23.7 23.73 23.7 23.74 23.7 23.75 23.7 23.75 23.7	2 23.70 3 23.75 3 23.75 4 23.74 5 23.75 5 23.75	72 73 .73 .74 3.75 3.75
23.76 23.76 23.77 23.78 23.78 23.78	13.76 2 13.76 2 13.77 2 13.78 2 13.78 2	23.76 23.7 23.76 23.7 23.77 23.7 23.78 23.7 23.78 23.7 23.78 23.7	23.75 8 23.76 8 23.76 7 23.77 8 23.78 8 23.78	23.76 23.76 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78 23.78	23.76 2 23.76 2 23.77 2 23.77 2 23.78 2 23.78 2	3.76 23 3.76 23 3.77 23 3.77 23 3.78 23 3.78 23	23.75 .76 23.76 .76 23.76 .77 23.77 .78 23.78 .78 23.78	23.76 23.76 23.77 23.77 23.78 23.78			2376 2376 2377 2378 2378					23.76 23.76 23.77 23.77 23.78 23.78							23.76 23 23.76 23 23.77 23 23.78 23 23.78 23 23.78 23				23.76 23.76 23.77 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78 23.78	23.76 23.76 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78 23.78	23.76 23. 23.76 23. 23.77 23. 23.78 23. 23.78 23.	23. 76 23. 76 23. 77 23. 78 23. 78 23.	23.75 76 23.76 77 23.77 78 23.78 78 23.78 78 23.78	23.76 23.76 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78	23,76 23,76 23,77 23,77 23,78 23,78	23.76 2 23.76 2 23.77 2 23.77 2 23.78 2 23.78 2 23.78 2	1.76 23.76 1.76 23.76 1.77 23.77 1.78 23.76 1.78 23.78	23.76 23.76 23.77 23.77 23.78 23.78	23.76 23.76 23.77 23.78 23.78 23.78	23.75 2 23.76 2 23.76 2 23.77 2 23.77 2 23.78 2 23.78 2 23.78 2	23.76 23.7 23.76 23.7 23.77 23.7 23.78 23.7 23.78 23.7 23.78 23.7	23.75 6 23.76 7 23.77 8 23.76 8 23.76 8 23.76	.76 .76 .77 1.78 3.78
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23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23.88 23.88 23.89 23.90 23.90 23.90	23.87 23 23.88 23 23.88 23 23.89 23 23.90 23 23.90 23 23.90 23	3.87 23.87 3.88 23.88 3.88 23.88 3.89 23.89 3.90 23.90 3.90 23.90	23.87 23.88 23.89 23.90 23.90 23.90	23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23.88 23.88 23.89 23.90 23.90 23.90	23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23 23.88 23 23.88 23 23.89 23 23.89 23 23.90 23 23.90 23	3.87 23.87 3.88 23.88 3.88 23.88 3.89 23.89 3.90 23.90 3.90 23.90	23.87 23. 23.88 23. 23.88 23. 23.89 23. 23.90 23. 23.90 23. 23.90 23.	.87 23.87 .88 23.88 .88 23.88 .89 23.89 .90 23.90 .90 23.90	23.87 23.88 23.88 23.89 23.90 23.90 23.90	23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23.88 23.88 23.89 23.90 23.90	23.87 2 23.88 2 23.88 2 23.89 2 23.90 2 23.90 2 23.90 2	3.87 23.87 3.88 23.88 3.89 23.89 3.80 23.89 3.90 23.90 3.90 23.90	23.87 23.88 23.88 23.89 23.90 23.90	23.87 23.87 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23 23.88 23 23.88 23 23.89 23 23.90 23 23.90 23 23.90 23	1.87 23.87 1.88 23.88 1.88 23.88 1.89 23.89 1.90 23.90 1.90 23.90	23.87 23.88 23.88 23.89 23.90 23.90 23.90	23.87 23.8 23.88 23.8 23.88 23.8 23.89 23.8 23.90 23.9 23.90 23.9	7 23.87 8 23.88 8 23.88 9 23.89 0 23.90 0 23.90 0 23.90	23.87 2 23.88 2 23.88 2 23.89 2 23.90 2 23.90 2 23.90 2	1.87 23.87 1.88 23.88 1.88 23.88 1.89 23.89 1.90 23.90 1.90 23.90	23.87 2 23.88 2 23.88 2 23.89 2 23.90 2 23.90 2	3.87 23.87 3.88 23.88 3.88 23.88 3.89 23.89 3.90 23.90 3.90 23.90	23.87 23.88 23.88 23.89 23.90 23.90 23.90	23.87 23. 23.88 23. 23.88 23. 23.89 23. 23.90 23. 23.90 23. 23.90 23.	.87 23.87 .88 23.88 .88 23.88 .89 23.89 .90 23.90 .90 23.90	23.87 23. 23.88 23. 23.88 23. 23.89 23. 23.90 23. 23.90 23.	87 23.87 88 23.88 88 23.88 89 23.89 90 23.90 90 23.90 90 23.90	23.87 23.8 23.88 23.8 23.88 23.8 23.89 23.8 23.90 23.9 23.90 23.9	23.87 23.88 23.88 23.89 23.90 23.90 23.90	23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23.87 23.87 23.88 23.88 23.88 23.88 23.89 23.89 23.90 23.90 23.90 23.90	23 23 23 23 23 23 23 24 24 25 24 25 26 21 20 21
23.91 23.91 23.91 23.91 23.92 23.92 23.93 23.93 23.93 23.93 23.93 23.93 23.94 23.94	23.91 23.91 23.91 23.91 23.92 23.92 23.93 23.93 23.93 23.93 23.94 23.94	23.91 23.91 23.92 23.93 23.93 23.93 23.94	23.91 23 23.91 23 23.92 23 23.93 23 23.93 23 23.93 23 23.94 23	3.91 23.91 3.91 23.91 3.92 23.92 3.93 23.93 3.93 23.93 3.94 23.94	23.91 23.91 23.92 23.93 23.93 23.93 23.94	23.91 23.91 23.91 23.91 23.92 23.92 23.93 23.93 23.93 23.93 23.94 23.94	23.91 23.91 23.92 23.93 23.93 23.93 23.94								23.91 23.91 23.92 23.93 23.93 23.94								23.91 23.9 23.91 23.9 23.92 23.9 23.93 23.9 23.93 23.9 23.93 23.9 23.94 23.9	8 2.3.8.8 9 2.3.8.8 0 2.3.8.8 0 2.3.0.0 1 2.2.3.0 1 2.2.3.0 1 2.2.3.1 2 2.3.0.2 3 2.3.0.2 3 2.3.0.2 4 2.3.0.4 5 2.3.0.4 6 2.3.0.4 6 2.3.0.4 7 2.2.3.0 8 2.3.0.4 9 2.3.0.4 1 4.4.1 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 2 3.4.2 3 3.4.2 4 2.3.2.2 4 2.3.4.2	23.91 2 23.91 2 23.92 2 23.93 2 23.93 2 23.93 2 23.94 2	191 23.91 191 23.91 192 23.92 193 23.93 193 23.93 194 23.94	2391 2 2391 2 2392 2 2393 2 2393 2 2393 2 2394 2	3.91 23.91 3.92 23.92 3.93 23.93 3.93 23.93 3.93 23.93 3.94 23.94	23.91 23.91 23.92 23.93 23.93 23.93 23.94	23.91 23. 23.91 23. 23.92 23. 23.93 23. 23.93 23. 23.93 23. 23.94 23.	89 23.89 90 23.90 90 23.91 91 23.91 91 23.91 92 23.92 93 23.93 94 23.94	23.91 23.9 23.91 23.9 23.92 23.9 23.93 23.9 23.93 23.9 23.93 23.9 23.94 23.9	91 23.91 91 23.91 92 23.92 93 23.93 93 23.93 93 23.93 94 23.94	23.91 23.9 23.91 23.9 23.92 23.9 23.93 23.9 23.93 23.9 23.93 23.9 23.94 23.9	23.91 23.91 23.92 23.93 23.93 23.93 23.93	23.91 23.91 23.91 23.91 23.92 23.92 23.93 23.93 23.93 23.93 23.93 23.93 23.94 23.94	23.91 23.91 23.91 23.91 23.92 23.92 23.93 23.93 23.93 23.93 23.93 23.93 23.94 23.94	23 23 23 3 23 3 23 4 2
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24.88 24.88 24.89 24.89 24.89 24.89 24.90 24.90 24.90 24.90 24.90 24.90 24.90 24.90 24.90 24.90	24.88 24.88 24.89 24.89 24.89 24.89 24.90 24.90 24.90 24.90 24.90 24.90	24.88 24.89 24.90 24.90 24.90 24.90	24.88 24 24.89 24 24.89 24 24.90 24 24.90 24 24.90 24 24.90 24	4.88 24.88 4.89 24.89 4.89 24.89 4.90 24.90 4.90 24.90 4.90 24.90	24.88 24.89 24.90 24.90 24.90 24.90	24.88 24.8 24.89 24.8 24.89 24.8 24.90 24.9 24.90 24.9 24.90 24.9	8 24.88 24.89 24.89 24.90 24.90 24.90 24.90										24.88 24.89 24.90 24.90 24.90 24.90			24.88 24. 24.89 24. 24.90 24. 24.90 24. 24.90 24. 24.90 24.	88 24.88 89 24.89 80 24.89 80 24.90 10 24.90 10 24.90 10 24.90 10 24.90		24.88 24.88 24.89 24.80 24.89 24.80 24.90 24.90 24.90 24.90 24.90 24.90			24.88 2 24.89 2 24.89 2 24.90 2 24.90 2 24.90 2 24.90 2 24.90 2	4.88 24.88 4.89 24.89 4.89 24.89 4.90 24.90 4.90 24.90 4.90 24.90	24.88 24.89 24.90 24.90 24.90 24.90	24.88 24.89 24.90 24.90 24.90 24.90	24.88 24.89 24.89 24.90 24.90 24.90	24.88 24.8 24.89 24.8 24.89 24.8 24.90 24.5 24.90 24.5 24.90 24.5 24.90 24.5	38 24.88 39 24.89 39 24.89 30 24.90 30 24.90 30 24.90 30 24.90	24.88 24.89 24.89 24.90 24.90 24.90 24.90	24.88 24.89 24.89 24.90 24.90 24.90 24.90	24.88 2 24.89 2 24.89 2 24.90 2 24.90 2 24.90 2 24.90 2	24.88 24 24.89 24 24.89 24 24.90 24 24.90 24 24.90 24 24.90 24 24.90 24	.88 24.85 .89 24.85 .89 24.85 .90 24.90 .90 24.90 .90 24.90	24.88 24.89 24.90 24.90 24.90 24.90	24.88 24.89 24.89 24.90 24.90 24.90	24.88 2 24.89 2 24.89 2 24.90 2 24.90 2 24.90 2 24.90 2	4.88 24.88 4.89 24.89 4.89 24.89 4.90 24.90 4.90 24.90 4.90 24.90	24.88 24.89 24.89 24.90 24.90 24.90	24.88 24.89 24.99 24.90 24.90 24.90	24.88 24.89 24.90 24.90 24.90 24.90
24.91 24.91 24.91 24.91 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.93 24.93	24.91 24.91 24.91 24.91 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.93 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24 24.91 24 24.92 24 24.92 24 24.92 24 24.92 24 24.92 24	4.91 24.91 4.91 24.91 4.92 24.92 4.92 24.92 4.92 24.92 4.92 24.92 4.93 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24.9 24.91 24.9 24.92 24.9 24.92 24.9 24.92 24.9 24.92 24.9 24.93 24.9	1 24.91 1 24.91 2 24.92 2 24.92 2 24.92 3 24.93										24.91 24.91 24.92 24.92 24.92 24.92 24.93						24.91 24.91 24.91 24.91 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.92 24.93 24.93			24.91 2 24.91 2 24.92 2 24.92 2 24.92 2 24.92 2 24.93 2	4.91 24.91 4.91 24.91 4.92 24.92 4.92 24.92 4.92 24.92 4.92 24.92 4.93 24.93	24.91 24.91 24.92 24.92 24.92 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24.5 24.91 24.5 24.92 24.5 24.92 24.5 24.92 24.5 24.92 24.5 24.93 24.5	01 24.91 01 24.91 02 24.92 02 24.92 02 24.92 02 24.92 03 24.93	24.91 24.91 224.92 224.92 24.92 224.92 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 2 24.91 2 24.92 2 24.92 2 24.92 2 24.92 2 24.93 2	24.91 24 24.91 24 24.92 24 24.92 24 24.92 24 24.92 24 24.93 24	(91 24.91 (91 24.91 (92 24.92 (92 24.92 (92 24.92 (93 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 2 24.91 2 24.92 2 24.92 2 24.92 2 24.92 2 24.93 2	4.91 24.91 4.91 24.91 4.92 24.92 4.92 24.92 4.92 24.92 4.92 24.92 4.93 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93	24.91 24.91 24.92 24.92 24.92 24.92 24.93
24.93 24.93 24.94 24.94 24.94 24.94 24.94 24.94 24.95 24.95 24.95 24.95	24.93 24.93 24.94 24.94 24.94 24.94 24.94 24.94 24.94 24.94 24.95 24.95 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24 24.94 24 24.94 24 24.94 24 24.95 24 24.95 24	4.93 24.93 4.94 24.94 4.94 24.94 4.94 24.94 4.95 24.95 4.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.9 24.94 24.9 24.94 24.9 24.94 24.9 24.94 24.9 24.95 24.9 24.95 24.9	3 24.93 4 24.94 4 24.94 4 24.94 5 24.95 5 24.95										24.93 24.94 24.94 24.94 24.95 24.95						24.93 24.93 24.94 24.94 24.94 24.94 24.94 24.94 24.95 24.95 24.95 24.95			24.93 2 24.94 2 24.94 2 24.94 2 24.95 2 24.95 2	4.93 24.93 4.94 24.94 4.94 24.94 4.94 24.94 4.95 24.95 4.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.5 24.94 24.5 24.94 24.5 24.94 24.5 24.95 24.5 24.95 24.5	13 24.93 14 24.94 14 24.94 14 24.94 15 24.95 15 24.95	24.93 24.94 24.94 24.94 24.94 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95 24.95	24.93 2 24.94 2 24.94 2 24.94 2 24.95 2 24.95 2	24.93 24 24.94 24 24.94 24 24.94 24 24.95 24 24.95 24	.93 24.93 .94 24.94 .94 24.94 .94 24.94 .95 24.95 .95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 2 24.94 2 24.94 2 24.94 2 24.95 2 24.95 2	4.93 24.93 4.94 24.94 4.94 24.94 4.94 24.94 4.95 24.95 4.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95	24.93 24.94 24.94 24.94 24.95 24.95
24.95 24.95 24.96 24.96 24.96 24.96 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97	24.95 24.95 24.96 24.96 24.96 24.96 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97	24.95 24.96 24.96 24.97 24.97 24.97	24.95 24 24.96 24 24.96 24 24.97 24 24.97 24 24.97 24 24.97 24 24.97 24	4.95 24.95 4.96 24.96 4.97 24.96 4.97 24.97 4.97 24.97 4.97 24.97	24.95 24.96 24.96 24.97 24.97 24.97 24.97	24.95 24.9 24.96 24.9 24.96 24.9 24.97 24.9 24.97 24.9 24.97 24.9 24.97 24.9	5 24.95 5 24.96 5 24.96 7 24.97 7 24.97 7 24.97										24.95 24.96 24.97 24.97 24.97 24.97				16 24.95 16 24.96 16 24.96 17 24.97 17 24.97 17 24.97		24.95 24.95 24.96 24.96 24.96 24.96 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97 24.97			24.95 2 24.96 2 24.96 2 24.97 2 24.97 2 24.97 2 24.97 2 24.97 2	4.95 24.95 4.96 24.96 4.96 24.96 4.97 24.97 4.97 24.97 4.97 24.97	24.95 24.96 24.97 24.97 24.97 24.97	24.95 24.96 24.96 24.97 24.97 24.97 24.97	24.96 24.96 24.97 24.97 24.97 24.97	24.95 24.95 24.96 24.95 24.96 24.95 24.97 24.95 24.97 24.95 24.97 24.95 24.97 24.95 24.97 24.95	05 24.95 06 24.96 06 24.96 07 24.97 07 24.97 07 24.97 07 24.97	5 24.95 5 24.96 5 24.96 7 24.97 7 24.97 7 24.97	24.95 24.96 24.96 24.97 24.97 24.97 24.97	24.95 2 24.96 2 24.96 2 24.97 2 24.97 2 24.97 2 24.97 2	24.95 24 24.96 24 24.96 24 24.97 24 24.97 24 24.97 24 24.97 24	.95 24.95 .96 24.96 .97 24.97 .97 24.97 .97 24.97 .97 24.97	24.95 24.96 24.97 24.97 24.97 24.97	24.95 24.96 24.97 24.97 24.97 24.97	24.95 2 24.96 2 24.96 2 24.97 2 24.97 2 24.97 2 24.97 2	4.95 24.95 4.96 24.96 4.96 24.96 4.97 24.97 4.97 24.97 4.97 24.97	24.95 24.96 24.96 24.97 24.97 24.97 24.97	24.95 24.96 24.97 24.97 24.97 24.97	24.95 24.96 24.96 24.97 24.97 24.97
24.98 24.98 24.98 24.98 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 25.00 25.00	24.98 24.98 24.98 24.98 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 25.00 25.00	24.98 24.99 24.99 24.99 24.99 25.00	24.98 24 24.98 24 24.99 24 24.99 24 24.99 24 24.99 24 25.00 25	4.98 24.98 4.98 24.98 4.99 24.99 4.99 24.99 4.99 24.99 5.00 25.00	24.98 24.98 24.99 24.99 24.99 24.99 25.00	24.98 24.9 24.98 24.9 24.99 24.9 24.99 24.9 24.99 24.9 24.99 24.9 25.00 25.0	8 24.98 8 24.98 9 24.99 9 24.99 9 24.99 9 25.00										24.98 24.99 24.99 24.99 24.99 25.00				18 24.98 18 24.99 19 24.99 19 24.99 19 24.99 19 24.99 10 25.00		24.98 24.98 24.98 24.98 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.99 24.91 24.91 25.00 25.00 25.00			24.98 2 24.98 2 24.99 2 24.99 2 24.99 2 24.99 2 25.00 2	4.98 24.98 4.98 24.98 4.99 24.99 4.99 24.99 4.99 24.99 4.99 24.99 5.00 25.00	24.98 24.99 24.99 24.99 24.99 25.00	24.98 24.98 24.99 24.99 24.99 25.00	24.98 24.99 24.99 24.99 24.99 25.00	24.98 24.9 24.98 24.9 24.99 24.9 24.99 24.9 24.99 24.9 24.99 24.9 24.99 24.5 25.00 25.0	18 24.98 18 24.98 19 24.99 19 24.99 19 24.99 19 24.99 19 24.99 10 24.99 20 24.99 20 24.99 20 24.99 20 25.00	24.98 24.98 24.99 24.99 24.99 24.99 25.00	24.98 24.98 24.99 24.99 24.99 25.00	24.98 2 24.98 2 24.99 2 24.99 2 24.99 2 24.99 2 25.00 2	24.98 24 24.98 24 24.99 24 24.99 24 24.99 24 24.99 24 25.00 25	.98 24.98 .98 24.98 .99 24.95 .99 24.95 .99 24.95 .00 25.00	24.98 24.99 24.99 24.99 24.99 25.00	24.98 24.98 24.99 24.99 24.99 24.99 25.00	24.98 2 24.98 2 24.99 2 24.99 2 24.99 2 24.99 2 25.00 2	4.98 24.98 4.98 24.98 4.99 24.99 4.99 24.99 4.99 24.99 5.00 25.00	24.98 24.98 24.99 24.99 24.99 25.00	24.98 24.98 24.99 24.99 24.99 25.00	24.98 24.98 24.99 24.99 24.99 25.00
25.00 25.00 25.00 25.00 25.01 25.01 25.01 25.01 25.02 25.02 25.02 25.02	25.00 25.00 25.00 25.00 25.01 25.01 25.01 25.01 25.02 25.02 25.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25 25.00 25 25.01 25 25.01 25 25.02 25 25.02 25 25.02 25	5.00 25.00 5.00 25.00 5.01 25.01 5.01 25.01 5.02 25.02 5.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25.0 25.00 25.0 25.01 25.0 25.01 25.0 25.02 25.0 25.02 25.0	0 25.00 0 25.00 1 25.01 1 25.01 2 25.02 2 25.02										25.00 25.00 25.01 25.01 25.02 25.02						25.00 25.00 25.00 25.00 25.01 25.01 25.01 25.01 25.02 25.02 25.02 25.02			25.00 2 25.00 2 25.01 2 25.01 2 25.01 2 25.02 2 25.02 2	5.00 25.00 5.00 25.00 5.01 25.01 5.01 25.01 5.02 25.02 5.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25.0 25.00 25.0 25.01 25.0 25.01 25.0 25.02 25.0 25.02 25.0	00 25.00 00 25.00 01 25.01 01 25.01 02 25.02 02 25.02	0 25.00 0 25.00 1 25.01 2 25.01 2 25.02 2 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 2 25.00 2 25.01 2 25.01 2 25.02 2 25.02 2 25.02 2	25.00 25 25.00 25 25.01 25 25.01 25 25.02 25 25.02 25 25.02 25	00 25.00 00 25.00 01 25.01 01 25.01 02 25.02 02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25.01 25.01 25.02 25.02 25.02	25.00 2 25.00 2 25.01 2 25.01 2 25.01 2 25.02 2 25.02 2	5.00 25.00 5.00 25.00 5.01 25.01 5.01 25.01 5.02 25.02 5.02 25.02	25.00 25.01 25.01 25.01 25.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02	25.00 25.00 25.01 25.01 25.02 25.02
25.02 25.02 25.03 25.03 25.03 25.03 25.03 25.03 25.04 25.04 25.04 25.04	25.02 25.02 25.03 25.03 25.03 25.03 25.03 25.03 25.04 25.04 25.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25 25.03 25 25.03 25 25.03 25 25.04 25 25.04 25	5.02 25.02 5.03 25.03 5.03 25.03 5.03 25.03 5.04 25.04 5.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25.0 25.03 25.0 25.03 25.0 25.03 25.0 25.04 25.0 25.04 25.0	2 25.02 3 25.03 3 25.03 3 25.03 4 25.04 4 25.04										25.02 25.03 25.03 25.03 25.04 25.04						25.02 25.02 25.03 25.03 25.03 25.03 25.03 25.03 25.04 25.04 25.04 25.04			25.02 2 25.03 2 25.03 2 25.03 2 25.03 2 25.04 2 25.04 2	5.02 25.02 5.03 25.03 5.03 25.03 5.03 25.03 5.04 25.04 5.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25.0 25.03 25.0 25.03 25.0 25.03 25.0 25.04 25.0 25.04 25.0	02 25.02 03 25.03 03 25.03 03 25.03 04 25.04 04 25.04	2 25.02 3 25.03 3 25.03 4 25.04 4 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 2 25.03 2 25.03 2 25.03 2 25.03 2 25.04 2 25.04 2	25.02 25 25.03 25 25.03 25 25.03 25 25.04 25 25.04 25	02 25.02 03 25.03 03 25.03 03 25.03 04 25.04 04 25.04	25.02 25.03 25.03 25.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 2 25.03 2 25.03 2 25.03 2 25.03 2 25.04 2 25.04 2	5.02 25.02 5.03 25.03 5.03 25.03 5.03 25.03 5.04 25.04 5.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04	25.02 25.03 25.03 25.03 25.04 25.04
25.05 25.05 25.05 25.05 25.06 25.06 25.06 25.06 25.06 25.06 25.06 25.06	25.05 25.05 25.05 25.05 25.06 25.06 25.06 25.06 25.06 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06	25.05 25 25.05 25 25.06 25 25.06 25 25.06 25 25.06 25	5.05 25.05 5.05 25.05 5.06 25.06 5.06 25.06 5.06 25.06	25.05 25.05 25.06 25.06 25.06 25.06	25.05 25.0 25.05 25.0 25.06 25.0 25.06 25.0 25.06 25.0 25.06 25.0	5 25.05 5 25.05 5 25.06 5 25.06 5 25.06 5 25.06										25.05 25.05 25.06 25.06 25.06			25.05 25. 25.05 25. 25.06 25. 25.06 25. 25.06 25. 25.06 25.	5 25.05 5 25.05 16 25.06 16 25.06 16 25.06 16 25.06		25.05 25.05 25.05 25.05 25.06 25.06 25.06 25.06 25.06 25.06			25.05 2 25.05 2 25.06 2 25.06 2 25.06 2 25.06 2	5.05 25.05 5.05 25.05 5.06 25.06 5.06 25.06 5.06 25.06 5.06 25.06	25.05 25.05 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06 25.06	25.05 25.0 25.05 25.0 25.06 25.0 25.06 25.0 25.06 25.0 25.06 25.0	05 25.05 05 25.05 06 25.06 06 25.06 06 25.06	25.05 25.05 25.06 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06 25.06	25.05 2 25.05 2 25.06 2 25.06 2 25.06 2 25.06 2 25.06 2	25.05 25 25.05 25 25.06 25 25.06 25 25.06 25 25.06 25	05 25.05 05 25.05 06 25.06 06 25.06 06 25.06	25.05 25.05 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06 25.06	25.05 2 25.05 2 25.06 2 25.06 2 25.06 2 25.06 2 25.06 2	5.05 25.05 5.05 25.05 5.06 25.06 5.06 25.06 5.06 25.06 5.06 25.06	25.05 25.05 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06	25.05 25.05 25.06 25.06 25.06 25.06
25.07 25.07 25.07 25.07 25.08 25.08 25.08 25.08 25.08 25.08 25.08 25.08	25.07 25.07 25.08 25.08 25.08 25.08 25.08 25.08 25.08 25.08 25.09 25.09	25.07 25.08 25.08 25.08 25.09	25.07 25 25.07 25 25.08 25 25.08 25 25.08 25 25.08 25 25.09 25	5.07 25.07 5.07 25.07 5.08 25.08 5.08 25.08 5.08 25.08 5.09 25.09	25.07 25.07 25.08 25.08 25.08 25.09	25.07 25.0 25.07 25.0 25.08 25.0 25.08 25.0 25.08 25.0 25.09 25.0	7 25.07 7 25.07 8 25.08 8 25.08 8 25.08 9 25.09										25.07 25.07 25.08 25.08 25.08 25.09				07 25.07 17 25.07 18 25.08 18 25.08 18 25.08 18 25.08 19 25.09		25.07 25.07 25.07 25.07 25.08 25.08 25.08 25.08 25.08 25.08 25.09 25.09			25.07 2 25.07 2 25.08 2 25.08 2 25.08 2 25.08 2 25.09 2 25.09 2	5.07 25.07 5.07 25.07 5.08 25.08 5.08 25.08 5.08 25.08 5.09 25.09	25.07 25.08 25.08 25.08 25.09	25.07 25.08 25.08 25.08 25.09	25.07 25.07 25.08 25.08 25.08 25.09	25.07 25.0 25.07 25.0 25.08 25.0 25.08 25.0 25.08 25.0 25.09 25.0	07 25.07 07 25.07 08 25.08 08 25.08 08 25.08 08 25.09 09 25.09	25.07 25.07 25.08 25.08 25.08 25.08 25.09	25.07 25.08 25.08 25.08 25.08 25.09	25.07 2 25.07 2 25.08 2 25.08 2 25.08 2 25.08 2 25.09 2 25.09 2	25.07 25 25.07 25 25.08 25 25.08 25 25.08 25 25.08 25 25.09 25	07 25.07 07 25.07 08 25.08 08 25.08 08 25.08 09 25.09	25.07 25.08 25.08 25.08 25.09	25.07 25.07 25.08 25.08 25.08 25.09	25.07 2 25.07 2 25.08 2 25.08 2 25.08 2 25.08 2 25.09 2 25.09 2	5.07 25.07 5.07 25.07 5.08 25.08 5.08 25.08 5.08 25.08 5.09 25.09	25.07 25.07 25.08 25.08 25.08 25.09	25.07 25.07 25.08 25.08 25.08 25.09	25.07 25.08 25.08 25.08 25.08 25.09
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25.16 25.16 25.16 25.16 25.17 25.17 25.17 25.17 25.17 25.17 25.18 25.18	25.16 25.16 25.16 25.16 25.17 25.17 25.17 25.17 25.17 25.17 25.18 25.18	25.16 25.16	25.16 25 25.16 25	5.16 25.16 5.16 25.16 5.17 25.17 5.17 25.17 5.17 25.17 5.18 25.18	25.16 25.16 25.17 25.17 25.17 25.18	25.16 25.1 25.16 25.1 25.17 25.1 25.17 25.1 25.17 25.1 25.18 25.1	25.16 25.16 25.17 25.17 25.17 25.17 25.17 25.18										25.16 25.16 25.17 25.17 25.17 25.18						25.16 25.16 25.16 25.16 25.17 25.17 25.17 25.17 25.17 25.17 25.18 25.18			25.16 2 25.16 2 25.17 2 25.17 2 25.17 2 25.17 2 25.17 2 25.18 2	5.16 25.16 5.16 25.16 5.17 25.17 5.17 25.17 5.17 25.17 5.18 25.18	25.16 25.17 25.17 25.17 25.17 25.18	25.16 25.16 25.17 25.17 25.17 25.17 25.18	25.16 25.16 25.17 25.17 25.17 25.18	25.16 25.1 25.16 25.1 25.17 25.1 25.17 25.1 25.17 25.1 25.17 25.1 25.18 25.1	16 25.16 16 25.16 17 25.17 17 25.17 17 25.17 18 25.18	25.16 25.16 25.17 25.17 25.17 25.17 25.18	25.16 25.16 25.17 25.17 25.17 25.18	25.16 2 25.16 2 25.17 2 25.17 2 25.17 2 25.17 2 25.18 2	25.16 25 25.16 25 25.17 25 25.17 25 25.17 25 25.17 25 25.18 25	(16 25.16 (16 25.16 (17 25.17 (17 25.17 (17 25.17 (17 25.17 (18 25.18	25.16 25.16 25.17 25.17 25.17 25.18	25.16 25.16 25.17 25.17 25.17 25.18	25.16 2 25.16 2 25.17 2 25.17 2 25.17 2 25.17 2 25.18 2	5.16 25.16 5.16 25.16 5.17 25.17 5.17 25.17 5.17 25.17 5.18 25.18	25.16 25.17 25.17 25.17 25.17 25.18	25.16 25.16 25.17 25.17 25.17 25.18	25.16 25.17 25.17 25.17 25.17 25.18
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71 26.71 72 26.72 72 26.72	26.71 26.72 26.72	86.71 26.72 86.72 26.72 86.72 26.72	26.71 26.72 26.72	26.71 26.72 26.72	26.71 26.72 26.72	26.71 26.72 26.72	26.71 26.71 26.72 26.72 26.72 26.72	1 26.71 2 26.72 2 26.72										(71 26.7) (72 26.7) (72 26.7)				26.71 26 26.72 26 26.72 26						71 26.7 72 26.7 72 26.7	1 26.71 2 26.72 2 26.72	28.71 2 28.72 2 28.72 2	26.71 26.71 26.72 26.72 26.72 26.72	26.71 26.72 26.72	26.71 26 26.72 26 26.72 26	1 26.71 2 26.72 2 26.72	28.71 2 28.72 2 28.72 2	26.71 26.7 26.72 26.7 26.72 26.7	71 26.71 72 26.72 72 26.72	26.71 26.72 26.72	26.71 26.72 26.72	26.71 26. 26.72 26. 26.72 26.	71 28.71 72 28.72 72 28.72	26.71 : 26.72 : 26.72 :	26.71 26.71 26.72 26.72 26.72 26.72	26.71 26.72 26.72
72 26.72 72 26.72 72 26.72	26.72 26.72 26.72	86.72 26.72 86.72 26.72 86.72 26.72	26.72 26.72 26.72	26.72 26.72 26.72	26.72 26.72 26.72	26.72 26.72 26.72	26.72 26.72 26.72 26.72 26.72 26.72	2 26.72 2 26.72 2 26.72										.72 26.7 .72 26.7 .72 26.7				26.72 26 26.72 26 26.72 26						72 26.73 72 26.73 72 26.73	2 26.72 2 26.72 2 26.72	26.72 2 26.72 2 26.72 2	26.72 26.72 26.72 26.72 26.72 26.72	26.72 26.72 26.72	26.72 26. 26.72 26. 26.72 26.	2 26.72 2 26.72 2 26.72	26.72 2 26.72 2 26.72 2	26.72 26.7 26.72 26.7 26.72 26.7	72 26.72 72 26.72 72 26.72	26.72 26.72 26.72	26.72 26.72 26.72	26.72 26. 26.72 26. 26.72 26.	72 26.72 72 26.72 72 26.72	26.72 : 26.72 : 26.72 :	26.72 26.72 26.72 26.72 26.72 26.72	26.72 26.72 26.72
.73 26.73 .73 26.73 .73 26.73	26.73 26.73 26.73	86.73 26.73 86.73 26.73 86.73 26.73	26.73 26.73 26.73	26.73 26.73 26.73	26.73 26.73 26.73	26.73 26.73 26.73	26.73 26.73 26.73 26.73 26.73 26.73	3 26.73 3 26.73 3 26.73										.73 26.7 .73 26.7 .73 26.7				26.73 26 26.73 26 26.73 26						73 26.71 73 26.71 73 26.71	3 26.73 3 26.73 3 26.73	26.73 2 26.73 2 26.73 2	26.73 26.73 26.73 26.73 26.73 26.73	26.73 26.73 26.73	26.73 26. 26.73 26. 26.73 26.	'3 26.73 '3 26.73 '3 26.73	26.73 2 26.73 2 26.73 2	26.73 26.73 26.73 26.73 26.73 26.73	73 26.73 73 26.73 73 26.73	26.73 26.73 26.73	26.73 26.73 26.73	26.73 26. 26.73 26. 26.73 26.	73 26.73 73 26.73 73 26.73	26.73 : 26.73 : 26.73 :	26.73 26.73 26.73 26.73 26.73 26.73	26.73 26.73 26.73
73 26.73 73 26.73 74 26.74 74 99.74	26.73 26.73 26.74 29.74	86.73 26.73 86.73 26.73 86.74 26.74 86.74 26.74	26.73 26.73 26.74	26.73 26.73 26.74 26.74	26.73 26.73 26.74 29.74	26.73 26.73 26.74 29.74	26.73 26.73 26.73 26.73 26.74 26.74 26.74 26.74	3 26.73 3 26.73 4 26.74 4 26.74										.73 26.7 .73 26.7 .74 26.7 .74 26.7				26.73 26 26.73 26 26.74 26 29.74 26						73 26.7 73 26.7 74 26.7 74 26.7	3 26.73 3 26.73 4 26.74	26.73 2 26.73 2 26.74 2 26.74 2	26.73 26.73 26.73 26.73 26.74 26.74	26.73 26.73 26.74 29.74	26.73 26. 26.73 26. 26.74 26. 26.74 26.	'3 26.73 '3 26.73 '4 26.74	26.73 2 26.73 2 26.74 2 26.74 2	26.73 26.73 26.73 26.73 26.74 26.74 26.74 26.74	73 26.73 73 26.73 74 26.74 74 26.74	26.73 26.73 26.74 26.74	26.73 26.73 26.74 39.74	26.73 26. 26.73 26. 26.74 26. 26.74 26.	73 26.73 73 26.73 74 26.74 74 29.74	26.73 : 26.73 : 26.74 :	26.73 26.73 26.73 26.73 26.74 26.74 26.74 26.74	26.73 26.73 26.74 26.74
.74 28.74 .74 26.74 .74 26.74	26.74 26.74 26.74	26.74 26.74 26.74 26.74 26.74 26.74	26.74 26.74 26.74	26.74 26.74 26.74 26.74	26.74 26.74 26.74 26.74	26.74 26.74 26.74 26.74	26.74 26.74 26.74 26.74 26.74 26.74 26.74 26.74	4 26.74 4 26.74 4 26.74				26.74 26. 26.74 26. 26.74 26.						.74 26.74 .74 26.74 .74 26.74				26.74 26 26.74 26 26.74 26						74 26.74 74 26.74 74 26.74 74 26.74	4 26.74 4 26.74 4 26.74	26.74 2 26.74 2 26.74 2	26.74 26.74 26.74 26.74 26.74 26.74	26.74 26.74 26.74	26.74 26 26.74 26 26.74 26	4 26.74 4 26.74 4 26.74	26.74 2 26.74 2 26.74 2	26.74 26.74 26.74 26.74 26.74 26.74	74 26.74 74 26.74 74 26.74	26.74 26.74 26.74	26.74 26.74 26.74	26.74 26. 26.74 26. 26.74 26.	74 28.74 74 26.74 74 26.74	26.74 26.74 26.74	26.74 26.74 26.74 26.74 26.74 26.74	26.74 26.74 26.74 26.74
.74 26.74 .75 26.75 .75 26.75	26.74 26.75 26.75	86.74 26.74 86.75 26.79 86.75 26.79	26.74 26.75 26.75	26.74 26.75 26.75	26.74 26.75 26.75	26.74 26.75 26.75	26.74 26.74 26.75 26.75 26.75 26.75	4 26.74 5 26.75 5 26.75										.74 26.74 .75 26.75 .75 26.75				26.74 26 26.75 26 26.75 26						74 26.74 75 26.75 75 26.75	4 26.74 5 26.75 5 26.75	26.74 2 26.75 2 26.75 2	26.74 26.74 26.75 26.75 26.75 26.75	26.74 26.75 26.75	26.74 26. 26.75 26. 26.75 26.	4 26.74 5 26.75 5 26.75	26.74 2 26.75 2 26.75 2	26.74 26.74 26.75 26.75 26.75 26.75	74 26.74 75 26.75 75 26.75	26.74 26.75 26.75	26.74 26.75 26.75	26.74 26. 26.75 26. 26.75 26.	74 26.74 75 26.75 75 26.75	26.74 26.75 26.75	26.74 26.74 26.75 26.75 26.75 26.75	26.74 26.75 26.75
.75 26.75 .75 26.75 .75 26.75	26.75 26.75 26.75	86.75 26.79 86.75 26.79 86.75 26.79	28.75 26.75 28.75	26.75 26.75 26.75	26.75 26.75 26.75	26.75 26.75 26.75	26.75 26.75 26.75 26.75 26.75 26.75	5 26.75 5 26.75 5 26.75										.75 26.79 .75 26.79 .75 26.79				26.75 26 26.75 26 26.75 26						75 26.75 75 26.75 75 26.75	5 26.75 5 26.75 5 26.75	26.75 2 26.75 2 26.75 2	26.75 26.75 26.75 26.75 26.75 26.75	26.75 26.75 26.75	26.75 26. 26.75 26. 26.75 26.	'5 26.75 '5 26.75 '5 26.75	26.75 2 26.75 2 26.75 2	26.75 26.75 26.75 26.75 26.75 26.75	75 26.75 75 26.75 75 26.75	26.75 26.75 26.75	26.75 26.75 26.75	26.75 26. 26.75 26. 26.75 26.	75 26.75 75 26.75 75 26.75	26.75 : 26.75 : 26.75 :	26.75 26.75 26.75 26.75 26.75 26.75	26.75 26.75 26.75
76 26.76 .76 26.76 .76 26.76 .76 26.76	26.76 26.76 26.76	26.76 26.76 26.76 26.76 26.76 26.76	26.76 26.76 26.76	26.76 26.76 26.76	26.76 26.76 26.76	26.76 26.76 26.76	26.76 26.76 26.76 26.76 26.76 26.76	6 26.76 6 26.76 6 26.76									26.76 26 26.76 26 26.76 26	.76 26.76 .76 26.76 .76 26.76	6 26.76 6 26.76 6 26.76			26.76 26 26.76 26 26.76 26						76 26.76 76 26.76 76 26.76	6 26.76 6 26.76 6 26.76	26.76 2 26.76 2 26.76 2	26.76 26.76 26.76 26.76 26.76 26.76	26.76 26.76 26.76	26.76 26. 26.76 26. 26.76 26.	6 26.76 6 26.76 6 26.76	26.76 2 26.76 2 26.76 2	26.76 26.71 26.76 26.71 26.76 26.71	76 26.76 76 26.76 76 26.76	26.76 26.76 26.76	26.76 26.76 26.76	26.76 26. 26.76 26. 26.76 26.	76 26.76 76 26.76 76 26.76	26.76 : 26.76 : 26.76 :	26.76 26.76 26.76 26.76 26.76 26.76	26.76 26.76 26.76
.76 26.76 .77 26.77 .77 26.77	26.76 26.77 26.77	26.76 26.77 26.77 26.77 26.77 26.77	26.76 26.77 26.77	26.76 26.77 26.77	26.76 26.77 26.77	26.76 26.77 26.77	26.76 26.76 26.77 26.77 26.77 26.77	6 26.76 7 26.77 7 26.77				26.76 26. 26.77 26. 26.77 26.						.76 26.76 .77 26.77 .77 26.77				26.76 26 26.77 26 26.77 26						76 26.7 77 26.7 77 26.7	5 26.76 5 26.77 7 26.77	26.76 2 26.77 2 26.77 2	26.76 26.76 26.77 26.77 26.77 26.77	26.76 26.77 26.77	26.76 26. 26.77 26. 26.77 26.	6 26.76 7 26.77 7 26.77	26.76 2 26.77 2 26.77 2	26.76 26.77 26.77 26.77 26.77 26.77	76 26.76 77 26.77 77 26.77	26.76 26.77 26.77	26.76 26.77 26.77	26.76 26. 26.77 26. 26.77 26.	76 26.76 77 26.77 77 26.77	26.76 26.77 26.77	26.76 26.76 26.77 26.77 26.77 26.77	26.76 26.77 26.77
		86.77 26.77 86.77 26.77 86.77 26.77					26.77 26.77 26.77 26.77 26.77 26.77	7 26.77 7 26.77 7 26.77										.77 26.7 .77 26.7 .77 26.7				26.77 26 26.77 26 26.77 26						27 26.7 27 26.7 27 26.7		26.77 2 26.77 2 26.77 2	26.77 26.77 26.77 26.77 26.77 26.77					26.77 26.77 26.77 26.77 26.77 26.77	77 26.77 77 26.77 77 26.77	26.77 26.77 26.77	26.77 26.77 26.77	26.77 26. 26.77 26. 26.77 26.	77 26.77 77 26.77 77 26.77	26.77 26.77 26.77	26.77 26.77 26.77 26.77 26.77 26.77	26.77 26.77 26.77
.77 26.77 .78 26.78 .78 26.78	26.77 26.78 26.78	86.77 26.77 86.78 26.78 86.78 26.78	26.77 26.78 26.78	26.77 26.78 26.78	26.77 26.78 26.78	26.77 26.78 26.78	26.77 26.77 26.78 26.78 26.78 26.78	7 26.77 8 26.78 8 26.78										.77 26.7 .78 26.7 .78 26.7				26.77 26 26.78 26 26.78 26						.77 26.75 .78 26.78 .78 26.78	7 26.77 8 26.78 8 26.78	26.77 2 26.78 2 26.78 2	26.77 26.77 26.78 26.78 26.78 26.78	26.77 26.78 26.78	26.77 26. 26.78 26. 26.78 26.	7 26.77 18 26.78 18 26.78	26.77 2 26.78 2 26.78 2	26.77 26.73 26.78 26.71 26.78 26.71	77 26.77 78 26.78 78 26.78	26.77 26.78 26.78	26.77 26.78 26.78	26.77 26. 26.78 26. 26.78 26.	77 26.77 78 26.78 78 26.78	26.77 26.78 26.78 26.78	26.77 26.77 26.78 26.78 26.78 26.78	26.77 26.78 26.78
78 26.78 .78 26.78 .78 26.78 .78 26.78	26.78 26.78 26.78	26.78 26.78 26.78 26.78 26.78 26.78	26.78 26.78 26.78	26.78 26.78 26.78	26.78 26.78 26.78	26.78 26.78 26.78	26.78 26.78 26.78 26.78 26.78 26.78	8 26.78 8 26.78 8 26.78										.78 26.78 .78 26.78 .78 26.78	8 26.78 8 26.78 8 26.78			26.78 26 26.78 26 26.78 26						78 26.78 78 26.78 78 26.78	8 26.78 8 26.78 8 26.78	26.78 2 26.78 2 26.78 2	26.78 26.78 26.78 26.78 26.78 26.78	26.78 26.78 26.78	26.78 26. 26.78 26. 26.78 26.	8 26.78 8 26.78 8 26.78	26.78 2 26.78 2 26.78 2	26.78 26.71 26.78 26.71 26.78 26.71	78 26.78 78 26.78 78 26.78	26.78 26.78 26.78	26.78 26.78 26.78	26.78 26. 26.78 26. 26.78 26.	78 26.78 78 26.78 78 26.78	26.78 : 26.78 : 26.78 :	26.78 26.78 26.78 26.78 26.78 26.78	26.78 26.78 26.78
.rs 26.79 .79 26.79 .79 26.79 .79 26.79	26.79 26.79 26.79 26.79	26.79 26.71 26.79 26.71 26.79 26.71 26.79 26.71	26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79 26.79 26.79 26.79 26.79	9 26.79 9 26.79 9 26.79 9 26.79				26.79 26. 26.79 26. 26.79 26. 26.79 26.					26.79 26 26.79 26 26.79 26 26.79 26	(79 26.7) (79 26.7) (79 26.7) (79 26.7)				26.79 26 26.79 26 26.79 26 26.79 26						79 26.71 79 26.71 79 26.71 79 26.71	9 26.79 9 26.79 9 26.79 9 26.79	26.79 2 26.79 2 26.79 2 26.79 2	26.79 26.79 26.79 26.79 26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79	26.79 26. 26.79 26. 26.79 26. 26.79 26.	9 26.79 9 26.79 9 26.79	26.79 2 26.79 2 26.79 2 26.79 2	26.79 26.79 26.79 26.79 26.79 26.79 26.79 26.79	79 26.79 79 26.79 79 26.79 79 26.79	26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79	26.79 26. 26.79 26. 26.79 26. 26.79 26.	79 26.79 79 26.79 79 26.79 79 26.79	26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79 26.79 26.79 26.79 26.79	26.79 26.79 26.79 26.79
.79 26.79 .80 26.80 .80 26.80	26.79 26.80 26.80	86.79 26.79 86.80 26.80 86.80 26.80	26.79 26.80 26.80	26.79 26.80 26.80	26.79 26.80 26.80	26.79 26.80 26.80	26.79 26.79 26.80 26.80 26.80 26.80	9 26.79 0 26.80 0 26.80										179 26.71 180 26.81 180 26.81				26.79 26 26.80 26 26.80 26						79 26.71 80 26.81 80 26.81	9 26.79 0 26.80 0 26.80	26.79 2 26.80 2 26.80 2	26.79 26.79 26.80 26.80 26.80 26.80	26.79 26.80 26.80	26.79 26. 26.80 26. 26.80 26.	19 26.79 10 26.80 10 26.80	26.79 2 26.80 2 26.80 2	26.79 26.79 26.80 26.80 26.80 26.80	79 26.79 80 26.80 80 26.80	26.79 26.80 26.80	26.79 26.80 26.80	26.79 26. 26.80 26. 26.80 26.	79 26.79 80 26.80 80 26.80	26.79 26.80 26.80	26.79 26.79 26.80 26.80 26.80 26.80	26.79 26.80 26.80
.80 26.80 .80 26.80 .80 26.80	26.80 26.80 26.80	86.80 26.80 86.80 26.80 86.80 26.80	26.80 26.80 26.80	26.80 26.80 26.80	26.80 26.80 26.80	26.80 26.80 26.80	26.80 26.80 26.80 26.80 26.80 26.80	0 26.80 0 26.80 0 26.80										.80 26.81 .80 26.81 .80 26.81				26.80 26 26.80 26 26.80 26						80 26.80 80 26.80 80 26.80	0 26.80 0 26.80 0 26.80	26.80 2 26.80 2 26.80 2	26.80 26.80 26.80 26.80 26.80 26.80	26.80 26.80 26.80	26.80 263 26.80 263 26.80 263	10 26.80 10 26.80 10 26.80	26.80 2 26.80 2 26.80 2	26.80 26.81 26.80 26.81 26.80 26.81	80 26.80 80 26.80 80 26.80	26.80 26.80 26.80	26.80 26.80 26.80	26.80 26. 26.80 26. 26.80 26.	80 26.80 80 26.80 80 26.80	26.80 26.80	26.80 26.80 26.80 26.80 26.80 26.80	26.80 26.80 26.80
.80 26.80 .81 26.81 .81 26.81	26.80 26.81 26.81	26.80 26.80 26.81 26.8 26.81 26.8	26.80 26.81 26.81	26.80 26.81 26.81	26.80 26.81 26.81	26.80 26.81 26.81	26.80 26.80 26.81 26.81 26.81 26.81	0 26.80 1 26.81 1 26.81										.80 26.80 .81 26.81 .81 26.81				26.80 26 26.81 26 26.81 26						.80 26.80 .81 26.81 .81 26.81	0 26.80 1 26.81 1 26.81	26.80 2 26.81 2 26.81 2	26.80 26.80 26.81 26.81 26.81 26.81	26.80 26.81 26.81	26.80 26/ 26.81 26/ 26.81 26/	10 26.80 11 26.81 11 26.81	26.80 2 26.81 2 26.81 2	26.80 26.81 26.81 26.8 26.81 26.8	30 26.80 31 26.81 31 26.81	26.80 26.81 26.81	26.80 26.81 26.81	26.80 26. 26.81 26. 26.81 26.	80 26.80 81 26.81 81 26.81	26.80 26.81 26.81	26.80 26.80 26.81 26.81 26.81 26.81	26.80 26.81 26.81
.61 26.81 .81 26.81 .81 26.81 .92 26.91	26.81 26.81 26.91	25.61 25.6 25.81 25.8 25.81 25.8 26.81 26.8	26.81 26.81 26.81	26.81 26.81 26.81	26.81 26.81 26.81	26.81 26.81 26.81	26.81 26.81 26.81 26.81 26.81 26.81	1 26.81 1 26.81 1 26.81				26.81 26. 26.81 26. 26.81 26.					26.81 26 26.81 26 26.81 26	.81 26.8 .81 26.8 .81 26.8	1 26.81 1 26.81 1 26.81	26.81 26.81 26.81		26.81 26 26.81 26 26.81 26	.61 25.61 .81 26.81 .81 26.81 .91 26.91	26.81 26.81 26.81	26.81 26.81 26.81			.81 26.8 .81 26.8 .81 26.8	1 26.81 1 26.81 1 26.81	26.81 2 26.81 2 26.81 2	26.81 26.81 26.81 26.81 26.81 26.81	26.81 26.81 26.81	26.81 26. 26.81 26. 26.81 26.	11 26.81 11 26.81 11 26.81	26.81 2 26.81 2 26.81 2	26.81 26.8 26.81 26.8 26.81 26.8	20.01 31 26.81 31 26.81	26.81 26.81 26.81	26.81 26.81 26.81	26.81 26. 26.81 26. 26.81 26.	81 26.81 81 26.81 81 26.81	26.81 : 26.81 :	26.81 26.81 26.81 26.81 26.81 26.81	26.81 26.81 26.81
.82 26.82 .82 26.82 .82 26.82	26.82 26.82 26.82	86.82 26.83 26.82 26.83 26.82 26.83	26.82 26.82 26.82	26.82 26.82 26.82	26.82 26.82 26.82	26.82 26.82 26.82	26.82 26.82 26.82 26.82 26.82 26.83	2 26.82 2 26.82 2 26.82 2 26.82										182 26.83 182 26.83 182 26.83				26.82 26 26.82 26 26.82 26						82 26.83 82 26.83 82 26.83	2 26.82 2 26.82 2 26.82	26.82 2 26.82 2 26.82 2	26.82 26.82 26.82 26.82 26.82 26.82	26.82 26.82 26.82	26.82 26. 26.82 26. 26.82 26.	12 26.82 12 26.82 12 26.82	26.82 2 26.82 2 26.82 2	26.82 26.8 26.82 26.8 26.82 26.8	32 26.82 32 26.82 32 26.82	26.82 26.82 26.82	26.82 26.82 26.82	26.82 26. 26.82 26. 26.82 26.	82 26.82 82 26.82 82 26.82	26.82 26.82 26.82	26.82 26.82 26.82 26.82 26.82 26.82	26.82 26.82 26.82
.82 26.82 .82 26.82 .83 26.83	26.82 26.82 26.83	86.82 26.83 86.82 26.83 86.83 26.83	26.82 26.82 26.83	26.82 26.82 26.83	26.82 26.82 26.83	26.82 26.82 26.83	26.82 26.82 26.82 26.83 26.83 26.83	2 26.82 2 26.82 3 26.83										.82 26.83 .82 26.83 .83 26.83				26.82 26 26.82 26 26.83 26						.82 26.83 .82 26.83 .83 26.83	2 26.82 2 26.82 3 26.83	26.82 2 26.82 2 26.83 2	26.82 26.82 26.82 26.82 26.83 26.83	26.82 26.82 26.83	26.82 26. 26.82 26. 26.83 26.	12 26.82 12 26.82 13 26.83	26.82 2 26.82 2 26.83 2	26.82 26.8 26.82 26.8 26.83 26.8	32 26.82 32 26.82 33 26.83	26.82 26.82 26.83	26.82 26.82 26.83	26.82 26. 26.82 26. 26.83 26.	82 26.82 82 26.82 83 26.83	26.82 2 26.82 2 26.83 2	26.82 26.82 26.82 26.82 26.83 26.83	26.82 26.82 26.83
.83 26.83 .83 26.83 .83 26.83	26.83 26.83 26.83	86.83 26.83 86.83 26.83 86.83 26.83	26.83 26.83 26.83	26.83 26.83 26.83	26.83 26.83 26.83	26.83 26.83 26.83	26.83 26.83 26.83 26.83 26.83 26.83	3 26.83 3 26.83 3 26.83										.83 26.83 .83 26.83 .83 26.83				26.83 26 26.83 26 26.83 26						83 26.83 .83 26.83 .83 26.83	3 26.83 3 26.83 3 26.83	26.83 2 26.83 2 26.83 2	26.83 26.83 26.83 26.83 26.83 26.83	26.83 26.83 26.83	26.83 26. 26.83 26. 26.83 26.	13 26.83 13 26.83 13 26.83	26.83 2 26.83 2 26.83 2	26.83 26.8 26.83 26.8 26.83 26.8	13 26.83 13 26.83 13 26.83	26.83 26.83 26.83	26.83 26.83 26.83	26.83 26. 26.83 26. 26.83 26.	83 26.83 83 26.83 83 26.83	26.83 : 26.83 : 26.83 :	26.83 26.83 26.83 26.83 26.83 26.83	26.83 26.83 26.83
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.85 26.85 .85 26.85 .85 26.85	26.85 26.85 26.85	26.85 26.83 26.85 26.83 26.85 26.83	26.85 26.85 26.85	26.85 26.85 26.85	26.85 26.85 26.85	26.85 26.85 26.85	26.85 26.85 26.85 26.85 26.85 26.85	5 26.85 5 26.85 5 26.85										185 26.85 185 26.85 185 26.85				26.85 26 26.85 26 26.85 26						.85 26.85 .85 26.85 .85 26.85	5 26.85 5 26.85 5 26.85	26.85 2 26.85 2 26.85 2	26.85 26.85 26.85 26.85 26.85 26.85	26.85 26.85 26.85	26.85 26. 26.85 26. 26.85 26.	15 26.85 15 26.85 15 26.85	26.85 2 26.85 2 26.85 2	26.85 26.8 26.85 26.8 26.85 26.8	85 26.85 85 26.85 85 26.85	26.85 26.85 26.85	26.85 26.85 26.85	26.85 26. 26.85 26. 26.85 26.	85 26.85 85 26.85 85 26.85	26.85 26.85 26.85	26.85 26.85 26.85 26.85 26.85 26.85	26.85 26.85 26.85
.85 26.85 .85 26.85 .86 26.86	26.85 26.85 26.86	26.85 26.85 26.85 26.85 26.86 26.84	26.85 26.85 26.86	26.85 26.85 26.86	26.85 26.85 26.86	26.85 26.85 26.86	26.85 26.85 26.85 26.85 26.86 26.86	5 26.85 5 26.85 6 26.86										.85 26.8 .85 26.8 .86 26.8				26.85 26 26.85 26 26.86 26						.85 26.85 .85 26.85 .86 26.85	5 26.85 5 26.85 8 26.86	26.85 2 26.85 2 26.86 2	26.85 26.85 26.85 26.85 26.86 26.86	26.85 26.85 26.86	26.85 26. 26.85 26. 26.86 26.	15 26.85 15 26.85 16 26.86	26.85 2 26.85 2 26.86 2	26.85 26.8 26.85 26.8 26.86 26.8	35 26.85 35 26.85 36 26.86	26.85 26.85 26.86	26.85 26.85 26.86	26.85 26. 26.85 26. 26.86 26.	85 26.85 85 26.85 86 26.86	26.85 : 26.85 : 26.86 :	26.85 26.85 26.85 26.85 26.86 26.86	26.85 26.85 26.86
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.86 26.86 .87 26.87 .87 26.87	26.86 26.87 26.87	26.86 26.86 26.87 26.87 26.87 26.87	26.86 26.87 26.87	26.86 26.87 26.87	26.86 26.87 26.87	26.85 26.87 26.87	26.86 26.86 26.87 26.87 26.87 26.87	6 26.86 7 26.87 7 26.87										186 26.81 187 26.81 187 26.81				26.86 26 26.87 26 26.87 26						86 26.80 87 26.81 87 26.81	5 26.86 7 26.87 7 26.87	26.85 2 26.87 2 26.87 2	26.86 26.86 26.87 26.87 26.87 26.87	26.86 26.87 26.87	26.86 260 26.87 260 26.87 260	16 26.86 17 26.87 17 26.87	26.86 2 26.87 2 26.87 2	26.86 26.8 26.87 26.8 26.87 26.8	36 26.86 37 26.87 37 26.87	26.86 26.87 26.87	26.86 26.87 26.87	26.86 26. 26.87 26. 26.87 26.	86 26.86 87 26.87 87 26.87	26.86 26.87 26.87	26.86 26.86 26.87 26.87 26.87 26.87	26.86 26.87 26.87
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.88 26.88 .88 26.88 .88 26.88	26.88 26.88 26.88	26.88 26.83 26.88 26.84 26.88 26.84	26.88 26.88 26.88	26.88 26.88 26.88	26.88 26.88 26.88	26.88 26.88 26.88	26.88 26.88 26.88 26.88 26.88 26.88	8 26.88 8 26.88 8 26.88										.88 26.81 .88 26.81 .88 26.81	8 26.88 8 26.88 8 26.88			26.88 26 26.88 26 26.88 26						88 26.81 88 26.81 88 26.81	8 26.88 8 26.88 8 26.88	26.88 2 26.88 2 26.88 2	26.88 26.88 26.88 26.88 26.88 26.88	26.88 26.88 26.88	26.88 26. 26.88 26. 26.88 26.	18 26.88 18 26.88 18 26.88	26.88 2 26.88 2 26.88 2	26.88 26.81 26.88 26.81 26.88 26.81	38 26.88 38 26.88 38 26.88	26.88 26.88 26.88	26.88 26.88 26.88	26.88 26. 26.88 26. 26.88 26.	88 26.88 88 26.88 88 26.88	26.88 : 26.88 : 26.88 :	26.88 26.88 26.88 26.88 26.88 26.88	26.88 26.88 26.88
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.89 26.89 .89 26.89 .90 26.90	26.89 26.89 26.90	86.89 26.81 36.89 26.81 36.90 26.91	26.89 26.89 26.90	26.89 26.89 26.90	26.89 26.89 26.90	26.89 26.89 26.90	26.89 26.89 26.89 26.89 26.90 26.90	9 26.89 9 26.89 0 26.90										.89 26.81 .89 26.81 .90 26.91				26.89 26 26.89 26 26.90 26						.89 26.81 .89 26.81 .90 26.91	9 26.89 9 26.89 0 26.90	26.89 2 26.89 2 26.90 2	26.89 26.89 26.89 26.89 26.90 26.90	26.89 26.89 26.90	26.89 26. 26.89 26. 26.90 26.	19 26.89 19 26.89 10 26.90	26.89 2 26.89 2 26.90 2	26.89 26.89 26.89 26.89 26.90 26.91	89 26.89 89 26.89 90 26.90	26.89 26.89 26.90	26.89 26.89 26.90	26.89 26. 26.89 26. 26.90 26.	89 26.89 89 26.89 90 26.90	26.89 : 26.89 : 26.90 :	26.89 26.89 26.89 26.89 26.90 26.90	26.89 26.89 26.90
90 26.90 90 26.90 90 26.90	26.90 26.90 26.90	86.90 26.90 86.90 26.90 86.90 26.90 86.90 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26.90 26.90 26.90 26.90 26.90	0 26.90 0 26.90 0 26.90				26.90 26. 26.90 26. 26.90 26.					26.90 26 26.90 26 26.90 26	(90 26.9) (90 26.9) (90 26.9)	0 26.90 0 26.90 0 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26 26.90 26 26.90 26	90 26.90 90 26.90 90 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26: 26.90 26: 26.90 26: 26.90 26:	.90 26.90 .90 26.90 .90 26.90 .90 26.90	0 26.90 0 26.90 0 26.90	26.90 2 26.90 2 26.90 2	26.90 26.90 26.90 26.90 26.90 26.90	26.90 26.90 26.90	26.90 26: 26.90 26: 26.90 26: 26.90 26:	0 26.90 0 26.90 0 26.90	26.90 2 26.90 2 26.90 2	26.90 26.91 26.90 26.91 26.90 26.91	10 26.90 10 26.90 10 26.90	26.90 26.90 26.90	26.90 26.90 26.90	26.90 26. 26.90 26. 26.90 26.	90 26.90 90 26.90 90 26.90	26.90 : 26.90 : 26.90 :	26.90 26.90 26.90 26.90 26.90 26.90	26.90 26.90 26.90
.91 26.91 .91 26.91 .91 26.91	26.91 26.91 26.91	06.91 26.91 26.91 26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91 26.91 26.91 26.91	1 26.91 1 26.91 1 26.91				26.91 26. 26.91 26. 26.91 26.						(91 26.9 (91 26.9 (91 26.9				26.91 26 26.91 26 26.91 26						91 26.9 91 26.9 91 26.9	1 26.91 1 26.91 1 26.91	26.91 2 26.91 2 26.91 2	26.91 26.91 26.91 26.91 26.91 26.91	26.91 26.91 26.91	26.91 26. 26.91 26. 26.91 26.	11 26.91 11 26.91 11 26.91	26.91 2 26.91 2 26.91 2	26.91 26.9 26.91 26.9 26.91 26.9	26.91 26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91 26.91	26.91 26. 26.91 26. 26.91 26.	91 26.91 91 26.91 91 26.91	26.91 26.91 26.91	26.91 26.91 26.91 26.91 26.91 26.91	26.91 26.91 26.91
91 26.91 91 26.91 91 26.91 92 26.92 92 26.92 92 26.92 92 26.92 92 26.92 92 26.92 92 26.92 92 26.92 93 26.93	26.91 26.91 26.91	86.91 26.91 86.91 26.91 86.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26.91 26.91 26.91 26.91 26.91	1 26.91 1 26.91 1 26.91										.91 26.91 .91 26.91 .91 26.91				26.91 26 26.91 26 26.91 26						91 26.9 91 26.9 91 26.9	1 26.91 1 26.91 1 26.91	26.91 2 26.91 2 26.91 2	26.91 26.91 26.91 26.91 26.91 26.91	26.91 26.91 26.91	26.91 26. 26.91 26. 26.91 26.	11 26.91 11 26.91 11 26.91	26.91 2 26.91 2 26.91 2	26.91 26.9 26.91 26.9 26.91 26.9	01 26.91 01 26.91 01 26.91	26.91 26.91 26.91	26.91 26.91 26.91	26.91 26. 26.91 26. 26.91 26.	91 26.91 91 26.91 91 26.91	26.91 : 26.91 : 26.91 :	26.91 26.91 26.91 26.91 26.91 26.91	26.91 26.91 26.91
92 26.92 92 26.92 92 26.92	26.92 26.92 26.92	86.92 26.93 86.92 26.93 86.92 26.93	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26.92 26.92 26.92 26.92 26.92	2 26.92 2 26.92 2 26.92										.92 26.93 .92 26.93 .92 26.93				26.92 26 26.92 26 26.92 26						92 26.93 92 26.93 92 26.93	2 26.92 2 26.92 2 26.92	26.92 2 26.92 2 26.92 2	26.92 26.92 26.92 26.92 26.92 26.92	26.92 26.92 26.92	26.92 26. 26.92 26. 26.92 26.	12 26.92 12 26.92 12 26.92	26.92 2 26.92 2 26.92 2	26.92 26.93 26.92 26.93 26.92 26.93	12 26.92 12 26.92 12 26.92 12 26.92	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26. 26.92 26. 26.92 26.	92 26.92 92 26.92 92 26.92	26.92 26.92 26.92	26.92 26.92 26.92 26.92 26.92 26.92	26.92 26.92 26.92
92 26.92 92 26.92 92 26.92 93 26.92	26.92 26.92 26.92 26.92	86.92 26.93 86.92 26.93 86.92 26.93 86.92 26.93	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26.92 26.92 26.92 26.92 26.92 26.92 26.92	2 26.92 2 26.92 2 26.92 2 26.92 2 26.92				26.92 26. 26.92 26. 26.92 26. 26.92 26.						(92 26.9) (92 26.9) (92 26.9) (92 26.9)	2 26.92 2 26.92 2 26.92 2 26.92	26.92 26.92 26.92 26.92		26.92 26 26.92 26 26.92 26 26.92 26	92 26.92 92 26.92 92 26.92 92 26.92	2 26.92 2 26.92 2 26.92 2 26.92	26.92 26.92 26.92			.92 26.93 92 26.93 .92 26.93 .92 26.93	2 26.92 2 26.92 2 26.92 2 26.92	26.92 2 26.92 2 26.92 2	26.92 26.92 26.92 26.92 26.92 26.92 26.92 26.92	26.92 26.92 26.92	26.92 26. 26.92 26. 26.92 26. 26.92 26.	12 26.92 12 26.92 12 26.92	26.92 2 26.92 2 26.92 2	26.92 26.93 26.92 26.93 26.92 26.93 26.92 26.93	12 26.92 12 26.92 12 26.92 12 26.92	26.92 26.92 26.92	26.92 26.92 26.92	26.92 26. 26.92 26. 26.92 26. 26.92 26.	92 26.92 92 26.92 92 26.92 93 26.92	26.92 : 26.92 : 26.92 :	26.92 26.92 26.92 26.92 26.92 26.92 26.92 26.92	26.92 26.92 26.92
.93 26.93 .93 26.93 .93 26.93	26.93 26.93 26.93	26.93 26.93 26.93 26.93 26.93 26.93	26.93 26.93 26.93	26.93 26.93 26.93	26.93 26.93 26.93	26.93 26.93 26.93	26.93 26.93 26.93 26.93 26.93 26.93	3 26.93 3 26.93 3 26.93				26.93 26. 26.93 26. 26.93 26.						193 26.91 193 26.91 193 26.91	3 26.93 3 26.93 3 26.93	26.93 26.93 26.93		26.93 26 26.93 26 26.93 26	93 26.93 93 26.93 93 26.93	26.93 26.93 26.93	26.93 26.93 26.93			.93 26.91 .93 26.91 .93 26.91	3 26.93 3 26.93 3 26.93	26.93 2 26.93 2 26.93 2	26.93 26.93 26.93 26.93 26.93 26.93	26.93 26.93 26.93	26.93 26. 26.93 26. 26.93 26.	13 26.93 13 26.93 13 26.93	26.93 2 26.93 2 26.93 2	26.93 26.93 26.93 26.93 26.93 26.93	13 26.93 13 26.93 13 26.93	26.93 26.93 26.93	26.93 26.93 26.93	26.93 26. 26.93 26. 26.93 26.	93 26.93 93 26.93 93 26.93	26.93 26.93 26.93	26.93 26.93 26.93 26.93 26.93 26.93	26.93 26.93 26.93
.93 26.93 .94 26.94 .94 26.94	26.93 26.94 26.94	85.93 26.93 85.94 26.94 85.94 26.94	26.93 26.94 26.94	26.93 26.94 26.94	26.93 26.94 26.94	26.93 26.94 26.94	26.93 26.93 26.94 26.94 26.94 26.94	3 26.93 4 26.94 4 26.94										.93 26.90 .94 26.94 .94 26.94				26.93 26 26.94 26 26.94 26						.93 26.93 .94 26.94 .94 26.94	3 26.93 4 26.94 4 26.94	26.93 2 26.94 2 26.94 2	26.93 26.93 26.94 26.94 26.94 26.94	26.93 26.94 26.94	26.93 26. 26.94 26. 26.94 26.	13 26.93 14 26.94 14 26.94	26.93 2 26.94 2 26.94 2	26.93 26.93 26.94 26.9- 26.94 26.9-	03 26.93 04 26.94 04 26.94	26.93 26.94 26.94	26.93 26.94 26.94	26.93 26. 26.94 26. 26.94 26.	93 26.93 94 26.94 94 26.94	26.93 : 26.94 : 26.94 :	26.93 26.93 26.94 26.94 26.94 26.94	26.93 26.94 26.94
94 26.94 94 26.94 94 26.94	26.94 26.94 26.94	65.94 26.94 26.94 26.94 26.94 26.94	26.94 26.94 26.94	26.94 26.94 26.94	26.94 26.94 26.94	26.94 26.94 26.94 26.94	26.94 26.94 26.94 26.94 26.94 26.94 26.94 26.94	4 26.94 4 26.94 4 26.94										04 26.94 04 26.94 04 26.94	4 26.94 4 26.94 4 26.94			26.94 26 26.94 26 26.94 26 26.94 26						94 26.9- 94 26.9- 94 26.9-	4 26.94 4 26.94 4 26.94	26.94 2 26.94 2 26.94 2	26.94 26.94 26.94 26.94 26.94 26.94 26.94 26.94	26.94 26.94 26.94	26.94 26. 26.94 26. 26.94 26. 26.94 26.	14 28.94 14 26.94 14 26.94	26.94 2 26.94 2 26.94 2	26.94 26.9- 26.94 26.9- 26.94 26.9- 26.94 26.9-	26.94 26.94 26.94 26.94	26.94 26.94 26.94	26.94 26.94 26.94	26.94 26. 26.94 26. 26.94 26. 26.94 26.	94 26.94 94 26.94 94 26.94 94 26.94	26.94 : 26.94 : 26.94 :	26.94 26.94 26.94 26.94 26.94 26.94 26.94 26.94	
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96 26.96 96 26.96 96 26.96	26.96 26.96 26.96	26.96 26.98 26.96 26.98 26.96 26.98	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26.96 26.96 26.96 26.96 26.96	6 26.96 6 26.96 6 26.96										.96 26.96 .96 26.96 .96 26.96				26.96 26 26.96 26 26.96 26						96 26.99 96 26.99 96 26.99	6 26.96 6 26.96 6 26.96	26.96 2 26.96 2 26.96 2	26.96 26.96 26.96 26.96 26.96 26.96	26.96 26.96 26.96	26.96 26. 26.96 26. 26.96 26.	16 26.96 16 26.96 16 26.96	26.96 2 26.96 2 26.96 2	26.96 26.94 26.96 26.94 26.96 26.94	96 26.96 96 26.96 96 26.96	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26. 26.96 26. 26.96 26.	96 26.96 96 26.96 96 26.96	26.96 26.96 26.96	26.96 26.96 26.96 26.96 26.96 26.96	26.96 26.96 26.96
96 26.96 96 26.96 96 26.96	26.96 26.96 26.96	85.96 26.94 85.96 26.94 85.96 26.94	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26.96 26.96 26.96 26.96 26.96	6 26.96 6 26.96 6 26.96										.96 26.96 .96 26.96 .96 26.96				26.96 26 26.96 26 26.96 26						96 26.91 96 26.91 96 26.91	8 26.96 8 26.96 8 26.96	26.96 2 26.96 2 26.96 2	26.96 26.96 26.96 26.96 26.96 26.96	26.96 26.96 26.96	26.96 26. 26.96 26. 26.96 26.	16 26.96 16 26.96 16 26.96	26.96 2 26.96 2 26.96 2	26.96 26.94 26.96 26.94 26.96 26.94	96 26.96 96 26.96 96 26.96	26.96 26.96 26.96	26.96 26.96 26.96	26.96 26. 26.96 26. 26.96 26.	96 26.96 96 26.96 96 26.96	26.96 26.96 26.96	26.96 26.96 26.96 26.96 26.96 26.96	26.96 26.96 26.96
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98 26.98 98 26.98 98 26.98 98 26.98 98 26.98 99 26.99	26.98 26.98 26.98	26.98 26.98 26.98 26.98 26.98 26.98	26.98 26.98 26.98 26.98 26.99	26.98 26.98 26.98	26.98 26.98 26.98	26.98 26.98 26.98	26.98 26.98 26.98 26.98 26.98 26.98	8 26.98 8 26.98 8 26.98										198 26.98 198 26.98 198 26.98				26.98 26 26.98 26 26.98 26						98 26.98 98 26.99 98 26.99	8 26.98 8 26.98 8 26.98	26.98 2 26.98 2 26.98 2 26.98 2 26.98 2 26.98 2 26.98 2 26.99 2	26.98 26.98 26.98 26.98 26.98 26.98	26.98 26.98 26.98	26.98 26. 26.98 26. 26.98 26.	18 26.98 18 26.98 18 26.98	26.98 2 26.98 2 26.98 2	26.98 26.91 26.98 26.91 26.98 26.91	98 26.98 98 26.98 98 26.98	26.98 26.98 26.98	26.98 26.98 26.98	26.98 26. 26.98 26. 26.98 26.	98 26.98 98 26.98 98 26.98	26.98 26.98 26.98	26.98 26.98 26.98 26.98 26.98 26.98	26.98 26.98 26.98
.98 26.98 .99 26.99	26.98 26.99	65.98 26.98 26.99 26.99 26.99 26.99	26.98 26.99 26.99	26.98 26.99 26.99	26.98 26.99 26.99	26.98 26.99 26.99	26.98 26.98 26.99 26.99 26.99 26.99	8 26.98 9 26.99 9 26.99										(98 26.94 (99 26.94 (99 26.94				26.98 26 26.99 26 26.99 26						98 26.98 99 26.91 99 26.91	8 26.98 9 26.99 9 26.99	26.98 2 26.99 2 26.99 2	26.98 26.98 26.99 26.99 26.99 26.99	26.98 26.99 26.99	26.98 26. 26.99 26. 26.99 26.	18 26.98 19 26.99 19 26.99	26.98 2 26.99 2 26.99 2	26.98 26.91 26.99 26.91 26.99 26.91	18 26.98 19 26.99 19 26.99	26.98 26.99 26.99	26.98 26.99 26.99	26.98 26. 26.99 26. 26.99 26.	96 26.98 99 26.99 99 26.99	26.98 : 26.99 : 26.99 :	26.98 26.98 26.99 26.99 26.99 26.99	26.98 26.99 26.99

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28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72</td> <td></td> <td></td> <td>28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72</td> <td></td> <td>28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28</td> <td>172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72</td> <td>28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7</td> <td>2 28.72 28 2 28.72 28</td> <td>.72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72</td> <td>28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7</td> <td>2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72</td> <td>28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72</td> <td>28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28</td> <td>772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72</td> <td>28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72</td> <td>28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28</td> <td>12 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72</td> <td>28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72</td> <td>72 72 72 72 72 72 72</td>	2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72	28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28	72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72	28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7	28.72 24 28.72 24 28.72 24 28.72 24 28.72 24 28.72 24 28.72 24 28.72 24 28.72 24					28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72		28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72	28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72			28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72		28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28	172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72 172 28.72	28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7	2 28.72 28 2 28.72 28	.72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72 .72 28.72	28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7 28.72 28.7	2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72 2 28.72	28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72	28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28	772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72 772 28.72	28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72	28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28 28.72 28	12 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72 72 28.72 28.72	28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 28.72 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29.25 29.25 29.25 29.2 29.25 29.25 29.25 29.2 29.25 29.25 29.2 29.25 29.2 29.25 29.25 29.25 29.2 29.25 29.2 29.25 29.25 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.25 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 <td>25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 26 29.26 29.26</td> <td>29,25 2 29,25 2 29,25 2 29,25 2 29,25 2 29,25 2 29,25 2 29,26 2</td> <td>9.25 29.25 9.25 29.25 9.25 29.25 9.25 29.25 9.25 29.25 9.26 29.25 9.26 29.26</td> <td>2925 2925 2925 2925 2925 2926</td> <td>2925 2925 2925 2925 2925 2925 2926</td> <td>29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2</td> <td>5 2925 5 2925 5 2925 5 2925 5 2925 5 2925 6 2926</td> <td></td> <td></td> <td></td> <td></td> <td>29.25 29.25 29.25 29.25 29.25 29.25 29.26</td> <td></td> <td></td> <td>29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2</td> <td>25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 26 29.25 26 29.26</td> <td></td> <td></td> <td>29.25 29 29.25 29 29.25 29 29.25 29 29.25 29 29.25 29 29.25 29</td> <td>25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 26 29.25</td> <td></td> <td>29.25 29.25 29.25 29.25 29.25 29.25 29.26</td> <td>29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.26 2 29.26 2</td> <td>29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2</td> <td>15 29.25 15 29.25 15 29.25 15 29.25 15 29.25 16 29.25 16 29.26</td> <td>29.25 29.25 29.25 29.25 29.25 29.25 29.26</td> <td>29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.26 2</td> <td>29.25 29.22 29.25 29.22 29.25 29.22 29.25 29.22 29.25 29.22 29.25 29.22 29.26 29.24</td> <td>5 2925 5 2925 5 2925 5 2925 5 2925 5 2925 6 2926 6 2926</td> <td>29.25 29.25 29.25 29.25 29.25 29.25 29.26</td> <td>29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.26 2 29.26 2</td> <td>29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2</td> <td>8 29.25 8 29.25 8 29.25 8 29.25 8 29.25 8 29.25 8 29.25</td> <td>22 25 29 25 29 25 29 25 29 25 29 25 29 26 29 26 20 20 20 20 20 20 20 20 20 20 20 20 20 20 2</td> <td>29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2</td> <td>5 29.25 5 29.25 5 29.25 5 29.25 5 29.25 6 29.26 6 29.26</td> <td>29.25 29.25 29.25 29.25 29.25 29.25 29.26</td> <td>29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2</td> <td>125 125 125 125 125 125 125 125 125</td>	25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 26 29.26 29.26	29,25 2 29,25 2 29,25 2 29,25 2 29,25 2 29,25 2 29,25 2 29,26 2	9.25 29.25 9.25 29.25 9.25 29.25 9.25 29.25 9.25 29.25 9.26 29.25 9.26 29.26	2925 2925 2925 2925 2925 2926	2925 2925 2925 2925 2925 2925 2926	29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2	5 2925 5 2925 5 2925 5 2925 5 2925 5 2925 6 2926					29.25 29.25 29.25 29.25 29.25 29.25 29.26			29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2	25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 26 29.25 26 29.26			29.25 29 29.25 29 29.25 29 29.25 29 29.25 29 29.25 29 29.25 29	25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 25 29.25 26 29.25		29.25 29.25 29.25 29.25 29.25 29.25 29.26	29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.26 2 29.26 2	29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2	15 29.25 15 29.25 15 29.25 15 29.25 15 29.25 16 29.25 16 29.26	29.25 29.25 29.25 29.25 29.25 29.25 29.26	29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.26 2	29.25 29.22 29.25 29.22 29.25 29.22 29.25 29.22 29.25 29.22 29.25 29.22 29.26 29.24	5 2925 5 2925 5 2925 5 2925 5 2925 5 2925 6 2926 6 2926	29.25 29.25 29.25 29.25 29.25 29.25 29.26	29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.25 2 29.26 2 29.26 2	29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2	8 29.25 8 29.25 8 29.25 8 29.25 8 29.25 8 29.25 8 29.25	22 25 29 25 29 25 29 25 29 25 29 25 29 26 29 26 20 20 20 20 20 20 20 20 20 20 20 20 20 20 2	29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2	5 29.25 5 29.25 5 29.25 5 29.25 5 29.25 6 29.26 6 29.26	29.25 29.25 29.25 29.25 29.25 29.25 29.26	29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.25 29.2 29.26 29.2	125 125 125 125 125 125 125 125 125
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29.34 29.3 29.34 29.3 29.34 29.3 29.34 29.3 29.34 29.3	4 29.34 4 29.34 4 29.34 4 29.34 4 29.34	29.34 29.34 29.34 29.34 29.34	29.34 2 29.34 2 29.34 2 29.34 2 29.34 2	29.34 29. 29.34 29. 29.34 29. 29.34 29. 29.34 29.	14 29.34 14 29.34 14 29.34 14 29.34 14 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29.34 29.34 29.34 29.34											29.34 29.34 29.34 29.34 29.34			29.34 2 29.34 2 29.34 2 29.34 2 29.34 2								29.34 2 29.34 2 29.34 2 29.34 2 29.34 2	29.34 29.3 29.34 29.3 29.34 29.3 29.34 29.3 29.34 29.3	34 29.34 34 29.34 34 29.34 34 29.34 34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29. 29.34 29. 29.34 29. 29.34 29. 29.34 29. 29.24 29.	34 29.34 34 29.34 34 29.34 34 29.34 34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 2 29.34 2 29.34 2 29.34 2 29.34 2 29.34 2	29.34 29. 29.34 29. 29.34 29. 29.34 29. 29.34 29.	34 29.34 34 29.34 34 29.34 34 29.34 34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29.34 29.34 29.34 29.34	29.34 29 29.34 29 29.34 29 29.34 29 29.34 29 29.34 29	9.34 29.3 9.34 29.3 9.34 29.3 9.34 29.3 9.34 29.3	34 29,34 34 29,34 34 29,34 34 29,34 34 29,34	29.34 29.34 29.34 29.34 29.34	29.34 29.34 29.34 29.34 29.34
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29.35 29.3 29.35 29.3 29.35 29.3 29.35 29.3 29.36 29.3	5 29.35 5 29.35 5 29.35 6 29.36	29.35 29.35 29.35 29.36	29.35 2 29.35 2 29.35 2 29.35 2 29.36 2	29.35 29. 29.35 29. 29.35 29. 29.36 29.	15 29.35 15 29.35 15 29.35 16 29.36	29.35 29.35 29.35 29.36	29.35 29.35 29.35 29.36	29.35 29.35 29.35 29.36											29.35 29.35 29.35 29.36			29.35 2 29.35 2 29.35 2 29.35 2 29.36 2								29.35 2 29.35 2 29.35 2 29.35 2 29.36 2	29.35 29.3 29.35 29.3 29.35 29.3 29.35 29.3 29.36 29.3	35 29.35 35 29.35 35 29.35 36 29.36	29.35 29.35 29.35 29.36	29.35 29.35 29.35 29.36	29.35 29. 29.35 29. 29.35 29. 29.36 29.	35 29.35 35 29.35 35 29.35 36 29.36	29.36 29.36 29.36 29.36	29.35 29.35 29.35 29.36	29.35 2 29.35 2 29.35 2 29.35 2 29.36 2	29.35 29. 29.35 29. 29.35 29. 29.35 29. 29.36 29.	35 29.35 35 29.35 35 29.35 36 29.36	29.35 29.35 29.35 29.36	29.35 29.35 29.35 29.36	29.35 29 29.35 29 29.35 29 29.35 29 29.36 29	9.35 29.3 9.35 29.3 9.35 29.3 9.36 29.3	35 29.35 35 29.35 35 29.35 36 29.36	29.35 29.35 29.35 29.36	29.35 29.35 29.35 29.36
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29.36 29.3 29.36 29.3 29.36 29.3 29.36 29.3 29.36 29.3	6 29.36 6 29.36 6 29.36 6 29.36 6 29.36	29.36 29.36 29.36 29.36 29.36	29.36 2 29.36 2 29.36 2 29.36 2 29.36 2	89.36 29: 29.36 29: 29.36 29: 29.36 29: 29.36 29:	13.30 16 29.36 16 29.36 16 29.36	29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36											29.36 29.36 29.36 29.36 29.36			29.36 2 29.36 2 29.36 2 29.36 2 29.36 2	1.36 29.3 1.36 29.3 1.36 29.3 1.36 29.3	36 29.36 36 29.36 36 29.36 36 29.36						29.36 2 29.36 2 29.36 2 29.36 2	19.36 29.3 19.36 29.3 19.36 29.3 19.36 29.3	36 29.36 36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29. 29.36 29. 29.36 29. 29.36 29. 29.36 29.	x 29.36 36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 2 29.36 2 29.36 2 29.36 2	29.36 29. 29.36 29. 29.36 29. 29.36 29. 29.36 29.	36 29.36 36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29 29.36 29 29.36 29 29.36 29 29.36 29	9.36 29.3 9.36 29.3 9.36 29.3 9.36 29.3	36 29.36 36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36
29.36 29.3 29.36 29.3 29.36 29.3 29.36 29.3	6 29.36 6 29.36 6 29.36 6 29.36 6 29.36	29.36 29.36 29.36 29.36 29.36	29.36 2 29.36 2 29.36 2 29.36 2 29.36 2	29.36 29: 29.36 29: 29.36 29: 29.36 29: 29.36 29:	16 29.36 16 29.36 16 29.36 16 29.36	29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36											29.36 29.36 29.36 29.36			29.36 2 29.36 2 29.36 2 29.36 2 29.36 2		36 29.36 36 29.36 36 29.36 36 29.36						29.36 2 29.36 2 29.36 2 29.36 2	29.36 29.3 29.36 29.3 29.36 29.3 29.36 29.3	36 29.36 36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36	29.36 29. 29.36 29. 29.36 29. 29.36 29.	36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 2 29.36 2 29.36 2 29.36 2	29.36 29. 29.36 29. 29.36 29. 29.36 29.	36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36 29.36	29.36 29 29.36 29 29.36 29 29.36 29 29.36 29	9.36 29.3 9.36 29.3 9.36 29.3 9.36 29.3	36 29.36 36 29.36 36 29.36 36 29.36	29.36 29.36 29.36 29.36	29.36 29.36 29.36 29.36
29.36 29.3 29.37 29.3 29.37 29.3 29.37 29.3	6 29.36 7 29.37 7 29.37 7 29.37 7 29.37	29.36 29.37 29.37 29.37	29.36 2 29.37 2 29.37 2 29.37 2 29.37 2	89.36 29. 89.37 29. 89.37 29. 89.37 29.	6 29.36 17 29.37 17 29.37 17 29.37	29.36 29.37 29.37 29.37	29.36 29.37 29.37 29.37 29.37	29.38 29.37 29.37 29.37											29.36 29.37 29.37 29.37			29.36 2 29.37 2 29.37 2 29.37 2								29.36 2 29.37 2 29.37 2 29.37 2	29.36 29.3 29.37 29.3 29.37 29.3 29.37 29.3	36 29.36 37 29.37 37 29.37 37 29.37	29.36 29.37 29.37 29.37 29.37	29.36 29.37 29.37 29.37 29.37	29.36 29. 29.37 29. 29.37 29. 29.37 29.	36 29.36 37 29.37 37 29.37 37 29.37	29.36 29.37 29.37 29.37	29.36 29.37 29.37 29.37	29.36 2 29.37 2 29.37 2 29.37 2	29.36 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	36 29.36 37 29.37 37 29.37 37 29.37	29.36 29.37 29.37 29.37	29.36 29.37 29.37 29.37 29.37	29.36 29 29.37 29 29.37 29 29.37 29 29.37 29	9.36 29.3 9.37 29.3 9.37 29.3 9.37 29.3	36 29.36 37 29.37 37 29.37 37 29.37	29.36 29.37 29.37 29.37	29.36 29.37 29.37 29.37
29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3	7 29.37 7 29.37 7 29.37 7 29.37 7 29.37	29.37 29.37 29.37 29.37 29.37	29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	17 29.37 17 29.37 17 29.37 17 29.37 17 29.37	29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37											29.37 29.37 29.37 29.37			29.37 2 29.37 2 29.37 2 29.37 2 29.37 2								29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37	29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37	29.37 29 29.37 29 29.37 29 29.37 29 29.37 29	9.37 29.3 9.37 29.3 9.37 29.3 9.37 29.3 9.37 29.3	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37
29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3	7 29.37 7 29.37 7 29.37 7 29.37 7 29.37	29.37 29.37 29.37 29.37 29.37	29.37 2 29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	17 29.37 17 29.37 17 29.37 17 29.37 17 29.37	29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37											29.37 29.37 29.37 29.37 29.37			29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	1.37 29.3 1.37 29.3 1.37 29.3 1.37 29.3 1.37 29.3							29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	20.37 20.3 20.37 20.3 20.37 20.3 20.37 20.3 20.37 20.3	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	2937 2937 2937 2937 2937	29.37 29.37 29.37 29.37 29.37	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	97 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 2 29.37 2 29.37 2 29.37 2 29.37 2	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29.	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29 29.37 29 29.37 29 29.37 29 29.37 29	9.37 29.3 9.37 29.3 9.37 29.3 9.37 29.3 9.37 29.3	37 29.37 37 29.37 37 29.37 37 29.37 37 29.37	29.37 29.37 29.37 29.37 29.37	29.37 29.37 29.37 29.37 29.37
29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3 29.38 29.3	7 29.37 7 29.37 7 29.37 7 29.37 7 29.37 8 29.38	29.37 29.37 29.37 29.37 29.38	29.37 2 29.37 2 29.37 2 29.37 2 29.37 2 29.38 2	20.37 29. 20.37 29. 20.37 29. 20.37 29. 20.37 29.	17 29.37 17 29.37 17 29.37 17 29.37 17 29.37 18 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29.37 29.37 29.37 29.38		29.37 25 29.37 25 29.37 25 29.37 25 29.38 25									29.37 29.37 29.37 29.37 29.38			29.37 2 29.37 2 29.37 2 29.37 2 29.37 2 29.38 2	1.37 20.3 1.37 20.3 1.37 20.3 1.37 20.3 1.38 20.3	57 20.37 37 20.37 37 20.37 37 20.37 38 20.38						29.37 2 29.37 2 29.37 2 29.37 2 29.38 2	29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3 29.37 29.3	37 29.37 37 29.37 37 29.37 37 29.37 38 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.38 29.	97 29.37 37 29.37 37 29.37 37 29.37 37 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29.37 29.37 29.37 29.38	29.37 2 29.37 2 29.37 2 29.37 2 29.37 2 29.38 2	29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.37 29. 29.38 29.	37 29.37 37 29.37 37 29.37 37 29.37 38 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29 29.37 29 29.37 29 29.37 29 29.37 29 29.38 29	0.37 20.3 0.37 20.3 0.37 20.3 0.37 20.3 0.38 20.3	37 29.37 37 29.37 37 29.37 37 29.37 38 29.38	29.37 29.37 29.37 29.37 29.38	29.37 29.37 29.37 29.37 29.38
29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3	8 29.38 8 29.38 8 29.38 8 29.38 8 29.38	29.38 29.38 29.38 29.38 29.38	29.38 2 29.38 2 29.38 2 29.38 2 29.38 2	29.38 29: 29.38 29: 29.38 29: 29.38 29: 29.38 29:	18 29.38 18 29.38 18 29.38 18 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38											29.38 29.38 29.38 29.38			29.38 2 29.38 2 29.38 2 29.38 2 29.38 2								29.38 2 29.38 2 29.38 2 29.38 2	29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29. 29.38 29. 29.38 29. 29.38 29.	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 2 29.38 2 29.38 2 29.38 2	29.38 29. 29.38 29. 29.38 29. 29.38 29. 29.38 29.	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29 29.38 29 29.38 29 29.38 29 29.38 29	9.38 29.3 9.38 29.3 9.38 29.3 9.38 29.3	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38
29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3	8 29.38 8 29.38 8 29.38 8 29.38 8 29.38	29.38 29.38 29.38 29.38 29.38	29.38 2 29.38 2 29.38 2 29.38 2 29.38 2	29.38 29. 29.38 29. 29.38 29. 29.38 29.	18 29.38 18 29.38 18 29.38 18 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38											29.38 29.38 29.38 29.38			29.38 2 29.38 2 29.38 2 29.38 2								29.38 2 29.38 2 29.38 2 29.38 2	29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3	38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38	29.38 29. 29.38 29. 29.38 29. 29.38 29.	38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 2 29.38 2 29.38 2 29.38 2 29.38 2	29.38 29. 29.38 29. 29.38 29. 29.38 29.	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29 29.38 29 29.38 29 29.38 29 29.38 29	9.38 29.3 9.38 29.3 9.38 29.3 9.38 29.3	38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38
29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3	8 29.38 8 29.38 8 29.38 8 29.38 8 29.38	29.38 29.38 29.38 29.38	29.38 2 29.38 2 29.38 2 29.38 2 29.38 2	29.38 29: 29.38 29: 29.38 29: 29.38 29: 29.38 29:	18 29.38 18 29.38 18 29.38 18 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38											29.38 29.38 29.38 29.38 29.38			29.38 2 29.38 2 29.38 2 29.38 2 29.38 2		38 29.38 38 29.38 38 29.38 38 29.38						29.38 2 29.38 2 29.38 2 29.38 2 29.38 2	29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3 29.38 29.3	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29. 29.38 29. 29.38 29. 29.38 29. 29.38 29.	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 2 29.38 2 29.38 2 29.38 2 29.38 2	29.38 29. 29.38 29. 29.38 29. 29.38 29. 29.38 29.	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29 29.38 29 29.38 29 29.38 29 29.38 29	9.38 29.3 9.38 29.3 9.38 29.3 9.38 29.3	38 29.38 38 29.38 38 29.38 38 29.38 38 29.38	29.38 29.38 29.38 29.38 29.38	29.38 29.38 29.38 29.38 29.38
29.38 29.3 29.38 29.3 29.39 29.3 29.39 29.3 29.39 29.3	8 29.38 8 29.38 9 29.39 9 29.39 9 29.39	29.38 29.38 29.39 29.39 29.39	29.38 2 29.38 2 29.39 2 29.39 2 29.39 2 29.39 2	20.38 290 20.38 290 20.39 290 20.39 290 20.39 290	18 29.38 18 29.38 19 29.39 19 29.39 19 29.39	29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39		29.38 25 29.38 25 29.39 25 29.39 25 29.39 25 29.39 25									29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39	29.38 2 29.38 2 29.39 2 29.39 2 29.39 2 29.39 2	1.38 20.3 1.38 20.3 1.39 20.3 1.39 20.3 1.39 20.3	8 20.38 38 20.38 39 20.39 39 20.39 39 20.39	29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39	23.38 23.38 23.39 23.39 29.39			29.38 2 29.38 2 29.39 2 29.39 2 29.39 2	20.38 20.3 20.38 20.3 20.39 20.3 20.39 20.3 20.39 20.3	38 29.38 38 29.38 39 29.30 39 29.30 39 29.30	29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39	29.38 29. 29.38 29. 29.39 29. 29.39 29. 29.39 29. 29.39 29.	88 29.38 38 29.38 39 29.39 39 29.39 39 29.39	29.38 29.38 29.39 29.39 29.39	29.38 29.38 29.39 29.39 29.39	29.38 2 29.38 2 29.39 2 29.39 2 29.39 2 29.39 2	29.38 29. 29.38 29. 29.39 29. 29.39 29. 29.39 29.	38 29.38 38 29.38 39 29.39 39 29.39 39 29.39	29.38 29.38 29.30 29.30 29.30	29.38 29.38 29.39 29.39 29.39	20.38 20 20.38 20 20.39 20 20.39 20 20.39 20 20.39 20	9.38 20.3 9.38 29.3 9.39 29.3 9.39 29.3 9.39 29.3	38 29.38 38 29.38 39 29.39 39 29.39 39 29.39	29.38 29.38 29.30 29.30 29.30	29.38 29.38 29.39 29.39 29.39
29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3	9 29.39 9 29.39 9 29.39 9 29.39	29.39 29.39 29.39 29.39 29.39	29.39 2 29.39 2 29.39 2 29.39 2 29.39 2	29.39 29. 29.39 29. 29.39 29. 29.39 29. 29.39 29.	19 29.39 19 29.39 19 29.39 19 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39											29.39 29.39 29.39 29.39 20.39			29.39 2 29.39 2 29.39 2 29.39 2								29.39 2 29.39 2 29.39 2 29.39 2	19.39 29.3 19.39 29.3 19.39 29.3 19.39 29.3	39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29. 29.39 29. 29.39 29. 29.39 29. 29.39 29.	39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 2 29.39 2 29.39 2 29.39 2 29.39 2	29.39 29. 29.39 29. 29.39 29. 29.39 29.	39 29.39 39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.30	29.39 29.39 29.39 29.39 29.39	29.39 29 29.39 29 29.39 29 29.39 29 29.39 29	9.39 29.3 9.39 29.3 9.39 29.3 9.39 29.3	39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39
29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3	9 29.39 9 29.39 9 29.39 9 29.39	29.39 29.39 29.39 29.39 29.39	29.39 2 29.39 2 29.39 2 29.39 2 29.39 2	29.39 29. 29.39 29. 29.39 29. 29.39 29. 29.39 29.	9 29.39 9 29.39 9 29.39 9 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39											29.39 29.39 29.39 29.39			29.39 2 29.39 2 29.39 2 29.39 2								29.39 2 29.39 2 29.39 2 29.39 2	29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3	39 29.30 39 29.30 39 29.39 39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39	29.39 29. 29.39 29. 29.39 29. 29.39 29.	30 29.39 30 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 2 29.39 2 29.39 2 29.39 2 29.39 2	29.39 29. 29.39 29. 29.39 29. 29.39 29.	39 29.39 39 29.39 39 29.39 39 29.39	29.30 29.30 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29 29.39 29 29.39 29 29.39 29 29.39 29	9.39 29.3 9.39 29.3 9.39 29.3 9.39 29.3	39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39
29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3	9 20.39 9 20.39 9 20.39 9 20.39	29.39 29.39 29.39 29.39	29.39 2 29.39 2 29.39 2 29.39 2 29.39 2	29.39 29: 29.39 29: 29.39 29: 29.39 29: 29.39 29:	9 29.39 9 29.39 9 29.39 9 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39											29.39 29.39 29.39 29.39 29.39			29.39 2 29.39 2 29.39 2 29.39 2 29.39 2								29.39 2 29.39 2 29.39 2 29.39 2	29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3 29.39 29.3	39 29.39 39 29.30 39 29.30 39 29.30 39 29.30	29.39 29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 29. 29.39 29. 29.39 29. 29.39 29.	39 29.39 39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39	29.39 2 29.39 2 29.39 2 29.39 2 29.39 2	29.39 29. 29.39 29. 29.39 29. 29.39 29. 29.39 29.	39 29.39 39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.30 29.30 29.30	29.39 29.39 29.39 29.39	29.39 29 29.39 29 29.39 29 29.39 29 29.39 29	9.39 29.3 9.39 29.3 9.39 29.3 9.39 29.3	39 29.39 39 29.39 39 29.39 39 29.39 39 29.39	29.39 29.39 29.39 29.39	29.39 29.39 29.39 29.39 29.39
29.39 29.3 29.40 29.4 29.40 29.4 29.40 29.4 29.40 29.4	9 29.39 0 29.40 0 29.40 0 29.40	29.39 23.40 23.40 23.40 23.40	29.39 2 29.40 2 29.40 2 29.40 2 29.40 2 29.40 2	20.39 29. 29.40 29. 29.40 29. 29.40 29. 29.40 29.	19 29.39 10 29.40 10 29.40 10 29.40	29.39 29.40 29.40 29.40 29.40	29.39 29.40 29.40 29.40 29.40	29.39 29.40 29.40 29.40 29.40											29.39 29.40 29.40 29.40			29.30 2 29.40 2 29.40 2 29.40 2 29.40 2	1.39 20.3 1.40 29.4 1.40 29.4 1.40 29.4 1.40 29.4	20 20.30 40 29.40 40 29.40 40 29.40						29.39 2 29.40 2 29.40 2 29.40 2 29.40 2	20.30 20.3 20.40 29.4 20.40 29.4 20.40 29.4 20.40 29.4	39 20.39 40 29.40 40 29.40 40 29.40 40 29.40	29.39 29.40 29.40 29.40 29.40	29.39 29.40 29.40 29.40 29.40	29.39 29. 29.40 29. 29.40 29. 29.40 29. 29.40 29.	9 29.39 40 29.40 40 29.40 40 29.40 40 29.40	29.39 29.40 29.40 29.40	29.39 29.40 29.40 29.40 29.40	29.39 2 29.40 2 29.40 2 29.40 2 29.40 2	29.39 29. 29.40 29. 29.40 29. 29.40 29. 29.40 29.	39 29.39 40 29.40 40 29.40 40 29.40 40 29.40	29.39 29.40 29.40 29.40	29.39 29.40 29.40 29.40	20.39 29 29.40 29 29.40 29 29.40 29 29.40 29	9.40 29.4 9.40 29.4 9.40 29.4 9.40 29.4 9.40 29.4	39 22,39 40 23,40 40 23,40 40 23,40 40 23,40	29.39 29.40 29.40 29.40	29.39 29.40 29.40 29.40 29.40
29.40 29.4 29.40 29.4 29.40 29.4 29.40 29.4 29.40 29.4	0 29.40 0 29.40 0 29.40 0 29.40	20.40 20.40 20.40 20.40 20.40	29.40 2 29.40 2 29.40 2 29.40 2 29.40 2	23.40 23. 23.40 23. 23.40 23. 23.40 23. 23.40 23.	10 29.40 10 29.40 10 29.40 10 29.40 10 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40											29.40 29.40 29.40 29.40 29.40			29.40 2 29.40 2 29.40 2 29.40 2 29.40 2	0.40 20.4 0.40 20.4 0.40 20.4 0.40 20.4	40 20.40 40 20.40 40 20.40 40 20.40 40 20.40						29.40 2 29.40 2 29.40 2 29.40 2 29.40 2	23.40 23.4 23.40 29.4 23.40 29.4 23.40 29.4 23.40 29.4	40 29.40 40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29. 29.40 29. 29.40 29. 29.40 29. 29.40 29.	40 29.40 40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 2 29.40 2 29.40 2 29.40 2 29.40 2	29.40 29. 29.40 29. 29.40 29. 29.40 29. 29.40 29.	40 29.40 40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40	29.40 29 29.40 29 29.40 29 29.40 29 29.40 29	9.40 29.4 9.40 29.4 9.40 29.4 9.40 29.4	40 23.40 40 23.40 40 23.40 40 23.40 40 23.40	29.40 29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40
29.40 29.4 29.40 29.4 29.40 29.4 29.40 29.4	0 29.40 0 29.40 0 29.40 0 29.40	29.40 29.40 29.40 29.40	29.40 2 29.40 2 29.40 2 29.40 2	19.40 29. 19.40 29. 19.40 29. 19.40 29.	0 29.40 0 29.40 0 29.40 0 29.40	29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40											29.40 29.40 29.40 29.40			29.40 2 29.40 2 29.40 2 29.40 2								29.40 2 29.40 2 29.40 2 29.40 2	29.40 29.4 29.40 29.4 29.40 29.4 29.40 29.4	40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40	29.40 29. 29.40 29. 29.40 29. 29.40 29.	40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40	29.40 2 29.40 2 29.40 2 29.40 2 29.40 2	29.40 29. 29.40 29. 29.40 29. 29.40 29.	40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40	29.40 29 29.40 29 29.40 29 29.40 29 29.40 29	9.40 29.4 9.40 29.4 9.40 29.4 9.40 29.4	40 29.40 40 29.40 40 29.40 40 29.40	29.40 29.40 29.40 29.40	29.40 29.40 29.40 29.40 29.40
29.40 29.4 29.40 29.4 29.40 29.4 29.41 29.4	0 29.40 0 29.40 0 29.40 1 29.41	29.40 29.40 29.40 29.41	29.40 2 29.40 2 29.40 2 29.41 2	30.40 29. 30.40 29. 30.40 29. 30.41 29. 30.42 29. 30.42 29.	10 29.40 10 29.40 10 29.40 11 29.41	29.40 29.40 29.40 29.41	29.40 29.40 29.40 29.41	29.40 29.40 29.40 29.41											29.40 29.40 29.40 29.41			29.40 2 29.40 2 29.40 2 29.41 2								29.40 2 29.40 2 29.40 2 29.41 2	29.40 29.4 29.40 29.4 29.40 29.4 29.41 29.4	40 29.40 40 29.40 40 29.40 41 29.41	29.40 29.40 29.40 29.41	29.40 29.40 29.40 29.41	29.40 29. 29.40 29. 29.40 29. 29.41 29.	40 29.40 40 29.40 40 29.40 41 29.41	29.40 29.40 29.40 29.41	29.40 29.40 29.40 29.41	29.40 2 29.40 2 29.40 2 29.41 2	29.40 29. 29.40 29. 29.40 29. 29.41 29.	40 29.40 40 29.40 40 29.40 41 29.41	29.40 29.40 29.40 29.41	29.40 29.40 29.40 29.41	29.40 29 29.40 29 29.40 29 29.41 29	9.40 29.4 9.40 29.4 9.40 29.4 9.41 29.4	40 29.40 40 29.40 40 29.40 41 29.41	29.40 29.40 29.40 29.41	29.40 29.40 29.40 29.41
29.41 29.4 29.41 29.4 29.41 29.4 29.41 29.4 29.41 29.4	1 29,41 1 29,41 1 29,41 1 29,41 1 29,41	29.41 29.41 29.41 29.41 29.41	29.41 2 29.41 2 29.41 2 29.41 2 29.41 2 29.41 2	20.41 29. 29.41 29. 29.41 29. 29.41 29. 29.41 29.	1 29.41 1 29.41 1 29.41 1 29.41 1 29.41 1 29.41 1 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41 29.41		29.41 25 29.41 25 29.41 25 29.41 25 29.41 25									20.41 20.41 20.41 20.41 20.41			29.41 2 29.41 2 29.41 2 29.41 2 29.41 2	1.41 29.4 1.41 29.4 1.41 29.4 1.41 29.4							20.41 2 20.41 2 20.41 2 20.41 2 20.41 2	20.41 20.4 20.41 20.4 20.41 20.4 20.41 20.4 20.41 20.4	41 29.41 41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41 29.41	20.41 20. 20.41 20. 20.41 20. 20.41 20. 20.41 20.	1 29.41 1 29.41 1 29.41 1 29.41 1 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 2 29.41 2 29.41 2 29.41 2 29.41 2	29.41 20. 29.41 20. 29.41 20. 29.41 20. 29.41 20.	41 29.41 41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29 29.41 29 29.41 29 29.41 29 29.41 29 29.41 29	9.41 29.4 9.41 29.4 9.41 29.4 9.41 29.4 9.41 29.4	41 20.41 41 20.41 41 20.41 41 20.41 41 20.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41 29.41
29.41 29.4 29.41 29.4 29.41 29.4 29.41 29.4	1 29.41 1 29.41 1 29.41 1 29.41	29.41 29.41 29.41 29.41	29.41 2 29.41 2 29.41 2 29.41 2 29.41 2	89.41 29. 89.41 29. 89.41 29. 89.41 29.	1 29.41 1 29.41 1 29.41 1 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41											29.41 29.41 29.41 29.41			29.41 2 29.41 2 29.41 2 29.41 2	0.41 29.4 0.41 29.4 0.41 29.4 0.41 29.4							29.41 2 29.41 2 29.41 2 29.41 2	29.41 29.4 29.41 29.4 29.41 29.4 29.41 29.4	41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 29. 29.41 29. 29.41 29. 29.41 29.	11 29.41 11 29.41 11 29.41 11 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 2 29.41 2 29.41 2 29.41 2	29.41 29. 29.41 29. 29.41 29. 29.41 29.	41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 29 29.41 29 29.41 29 29.41 29 29.41 29	9.41 29.4 9.41 29.4 9.41 29.4 9.41 29.4	41 29.41 41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41
29.41 29.4 29.41 29.4 29.41 29.4 29.41 29.4	1 29.41 1 29.41 1 29.41 1 29.41 1 29.41	29.41 29.41 29.41 29.41	29.41 2 29.41 2 29.41 2 29.41 2 29.41 2	89.41 29. 89.41 29. 89.41 29. 89.41 29.	1 29.41 1 29.41 1 29.41 1 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41											29.41 29.41 29.41 29.41			29.41 2 29.41 2 29.41 2 29.41 2								29.41 2 29.41 2 29.41 2 29.41 2	89.41 29.4 89.41 29.4 89.41 29.4 89.41 29.4	41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 29. 29.41 29. 29.41 29. 29.41 29.	41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 2 29.41 2 29.41 2 29.41 2 29.41 2	29.41 29. 29.41 29. 29.41 29. 29.41 29.	41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41	29.41 29 29.41 29 29.41 29 29.41 29 29.41 29	9.41 29.4 9.41 29.4 9.41 29.4 9.41 29.4	41 29.41 41 29.41 41 29.41 41 29.41	29.41 29.41 29.41 29.41	29.41 29.41 29.41 29.41
29.41 29.4 29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4	1 29.41 2 29.42 2 29.42 2 29.42 2 29.42	20.41 20.42 20.42 20.42	20.41 2 20.42 2 20.42 2 20.42 2 20.42 2	29.41 29. 29.42 29. 29.42 29. 29.42 29.	i1 29.41 i2 29.42 i2 29.42 i2 29.42 i2 29.42	29.41 29.42 29.42 29.42	29.41 29.42 29.42 29.42	29.41 29.42 29.42 29.42											29.41 29.42 29.42 29.42			29.41 2 29.42 2 29.42 2 29.42 2 29.42 2								29.41 2 29.42 2 29.42 2 29.42 2	29.41 29.4 29.42 29.4 29.42 29.4 29.42 29.4	41 29.41 42 29.42 42 29.42 42 29.42 42 29.42	29.41 29.42 29.42 29.42 29.42	29.41 29.42 29.42 29.42 29.42	29.41 29. 29.42 29. 29.42 29. 29.42 29.	41 29.41 42 29.42 42 29.42 42 29.42	29.41 29.42 29.42 29.42	29.41 29.42 29.42 29.42	29.41 2 29.42 2 29.42 2 29.42 2 29.42 2	29.41 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	41 29.41 42 29.42 42 29.42 42 29.42 42 29.42	29.41 29.42 29.42 29.42	29.41 29.42 29.42 29.42 29.42	29.41 29 29.42 29 29.42 29 29.42 29 29.42 29	9.41 29.4 9.42 29.4 9.42 29.4 9.42 29.4	41 20.41 42 20.42 42 20.42 42 20.42 42 20.42	29.41 29.42 29.42 29.42	29.41 29.42 29.42 29.42 29.42
29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4	2 20.42 2 29.42 2 29.42 2 29.42 2 29.42 2 29.42	29.42 29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	2 29.42 12 29.42 12 29.42 12 29.42 12 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42		25.42 25 29.42 25 29.42 25 29.42 25 29.42 25 29.42 25									29.42 29.42 29.42 29.42 29.42	20.42 20.42 20.42 20.42 20.42 20.42	29.42 29.42 29.42 29.42 29.42 29.42	25.42 2 29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	0.42 29.4 0.42 29.4 0.42 29.4 0.42 29.4 0.42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	20.42 29.42 29.42 29.42 29.42	20.42 20.42 20.42 20.42 20.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2 29.43	0.42 29.4 19.42 29.4 19.42 29.4 19.42 29.4 19.42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2 29.43	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29,42 29,42 29,42 29,42 29,42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29 29.42 29 29.42 29 29.42 29 29.42 29 29.42 29	9.42 29.4 9.42 29.4 9.42 29.4 9.42 29.4 9.42 29.4	42 20,42 42 20,42 42 20,42 42 20,42 42 20,42 42 20,42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42
29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2 29.42	29.42 29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	89.42 29. 89.42 29. 89.42 29. 89.42 29. 89.42 29. 89.42 29.	29.42 12 29.42 12 29.42 12 29.42 12 29.42 12 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42											29.42 29.42 29.42 29.42 29.42			29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	0.42 29.4 0.42 29.4 0.42 29.4 0.42 29.4 0.42 29.4							29.42 2 29.42 2 29.42 2 29.42 2	29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4 29.42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	29.42 42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42 29.42	29.42 29 29.42 29 29.42 29 29.42 29 29.42 29 29.42 20	9.42 29.4 9.42 29.4 9.42 29.4 9.42 29.4 9.42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42
2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2840 284 2841 284 2841 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 2844 284 284 284 284 284 284 284 284 284	0 3.4.0 0 3.4.0 0 3.4.0 0 2.4.0 0 2.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 3.4.0 0 2.4.0 1 2.4.1 1 3.4.1 1 3.4.1 1 3.4.1 1 3.4.1 1 3.4.1 1 3.4.1 1 3.4.1 2 3.4.2 3 3.4.1 2 3.4.2 3 3.4.1 3 3.4.1 2 3.4.2 3 3.4.2 3 3.4.2 3 3.4.2 3 3.4.2 3	29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	NA42 20 NA43 20	2 29.42 12 29.42 12 29.42 12 29.42 12 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42											29.42 29.42 29.42 29.42			29.42 2 29.42 2 29.42 2 29.42 2 29.42 2).42 29.4).42 29.4).42 29.4).42 29.4).42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42						29.42 2 29.42 2 29.42 2 29.42 2	89.42 29.4 89.42 29.4 89.42 29.4 89.42 29.4 89.42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.	42 29.42 42 29.42 42 29.42 42 29.42 42 <u>29.42</u>	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 2 29.42 2 29.42 2 29.42 2 29.42 2	29.42 29. 29.42 29. 29.42 29. 29.42 29. 29.42 29.		29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29 29.42 29 29.42 29 29.42 29 29.42 29	9.42 29.4 9.42 29.4 9.42 29.4 9.42 29.4 9.42 29.4	42 29.42 42 29.42 42 29.42 42 29.42 42 29.42	29.42 29.42 29.42 29.42 29.42	29.42 29.42 29.42 29.42 29.42
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Gains due to site improvement

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Selected Methodology = Site specific (required for planning applications) Type of peatland = Acid Bog

Reduction in GHG emissions due to improvement of site		Expecte	ed result			Minimu	m result			Maximu	m result	
	Degraded Bog	Felled Forestry	Borrow Pits	Foundations &	Degraded Bog	Felled Forestry	Borrow Pits	Foundations &	Degraded Bog	Felled Forestry	Borrow Pits	Foundations &
. Description of site				Hardstanding				Hardstanding				Hardstanding
Period of time when effectiveness of the improvement can be guaranteed (years)	0	0	22	25	0	0	21	25	0	0	23	25
Area to be improved (ha)	0	0	0	0	0	Ő	0	0	0	0 0	0	0
Average air temperature at site (°C)	7.5	7.5	7.5	7.5	3.9	3.9	3.9	3.9	11.2	11.2	11.2	11.2
Depth of peat drained (m)	0.68	0.68	1.05	0.68	0.50	0.50	1.00	0.50	1.00	1.00	1.10	1.00
Depth of peat above water table before improvement (m)	0.00	0.00	0.20	0.00	0.00	0.00	0.10	0.00	0.00	0.00	0.30	0.00
Depth of peat above water table after improvement (m)	0.00	0.00	0.30	0.00	0.00	0.00	0.40	0.00	0.00	0.00	0.20	0.00
2. Losses with improvement												
Flooded period (days year ⁻¹)	178	178	178	178	178	178	178	178	178	178	178	178
Time required for hydrology and habitat to return to its previous state on restoration	0	0	3	0	0	0	2	0	0	0	4	0
(years)	-	-	-	-		-			-			
Improved period (years)	0	0	19	25	0	0	19	25	0	0	19	25
Methane emissions from improved land	0.400	0.400	0.000	0.400	0.477	0.477	0.010	0.477	0.500	0.500	0.045	0.500
Site specific methane emission from improved soil on acid bogs (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.490	0.490	0.002	0.490	0.477	0.477	-0.019	0.477	0.503	0.503	0.045	0.503
Site specific methane emission from improved soil on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.559	0.559	0.026	0.559	0.556	0.556	0.004	0.556	0.561	0.561	0.078	0.561
IPCC annual rate of methane emission on acid bogs (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040
IPCC annual rate of methane emission on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219
Selected annual rate of methane emission (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.490	0.490	0.002	0.490	0.477	0.477	-0.019	0.477	0.503	0.503	0.045	0.503
CH ₄ emissions from improved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Carbon dioxide emissions from improved land												
Site specific CO ₂ emission from improved soil on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	-0.13	-0.13	10.92	-0.13	-1.09	-1.09	14.00	-1.09	0.85	0.85	7.30	0.85
Site specific CO ₂ emissions from improved soil on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	4.27	4.27	31.94	4.27	2.25	2.25	43.47	2.25	6.35	6.35	18.39	6.35
IPCC annual rate of carbon dioxide emission on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
IPCC annual rate of carbon dioxide emission on fens (t CO_2 ha ⁻¹ yr ⁻¹)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Selected annual rate of carbon dioxide emission on ons $(CO_2 na^{-1} yr^{-1})$	-0.13	-0.13	10.92	-0.13	-1.09	-1.09	14.00	-1.09	0.85	0.85	7.30	0.85
CO ₂ emissions from improved land (t CO ₂)												
	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from improved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
3. Losses without improvement	0	0	0	0	0	0	0	0	0	0	0	0
Flooded period (days year ⁻¹) Time required for hydrology and habitat to return to its previous state on restoration	-	-		-	-	-	-	-	-	-	0	-
(vears)	0	0	3	0	0	0	2	0	0	0	4	0
Improved period (years)	0	0	19	25	0	0	19	25	0	0	19	25
Methane emissions from unimproved land												
Site specific methane emission from unimproved soil on acid bogs (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.490	0.490	0.032	0.490	0.477	0.477	0.123	0.477	0.503	0.503	0.015	0.503
Site specific methane emission from unimproved soil on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.559	0.559	0.076	0.559	0.556	0.556	0.206	0.556	0.561	0.561	0.028	0.561
IPCC annual rate of methane emission on acid bogs (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
IPCC annual rate of methane emission on fens (t CH_4 -C ha^{-1} yr^{-1})	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Selected annual rate of methane emission of $CH_4 - Cha^{-1}$ yr ⁻¹)	0.490	0.490	0.032	0.490	0.477	0.477	0.123	0.477	0.503	0.503	0.015	0.503
CH ₄ emissions from unimproved land (t CO_2 equiv.)	0.490	0.490	0.032	0.490	0.477	0.477	0.123	0.477	0.503	0.505	0.015	0.503
7	0	0	0	0	0	0	0	0	0	0	0	0
Carbon dioxide emissions from unimproved land Site specific CO ₂ emission from unimproved soil on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	-0.13	-0.13	6.32	-0.13	-1.09	-1.09	1.29	-1.09	0.85	0.85	11.90	0.85
							-					
Site specific CO ₂ emissions from unimproved soil on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	4.27	4.27	16.31	4.27	2.25	2.25	4.34	2.25	6.35	6.35	34.02	6.35
IPCC annual rate of carbon dioxide emission on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
IPCC annual rate of carbon dioxide emission on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
Selected annual rate of carbon dioxide emission (t CO ₂ ha ⁻¹ yr ⁻¹)	-0.13	-0.13	6.32	-0.13	-1.09	-1.09	1.29	-1.09	0.85	0.85	11.90	0.85
CO ₂ emissions from unimproved land (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from unimproved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
RESULTS									1			
4. Reduction in GHG emissions due to improvement of site												
Total GHG emissions from improved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from unimproved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Reduction in GHG emissions due to improvement (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Additional CO ₂ payback time of windfarm due to site improvement												
coal-fired electricity generation (months)	0	0	0	0	0	0	0	0	0	0	0	0
grid-mix of electricity generation (months)	0	0	0	0	0	0	0	0	0	0	0	0
fossil fuel - mix of electricity generation (months)		0				•	0	0				

Click here to move to Payback Time Click here

Gains due to site improvement

Variants due to and minutovement. Note: Note, CO₂ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).

Note: Methane emissions from acid bogs. Equation derived by regression analysis against 57 measurements (Nayak et al. 2009). The equation derived was $R_{\rm obs}$ = (1/1000) (500 × cpc)(-1234 × (WN100)) + ((3.529 × 7) - 36.67)) where $R_{\rm obs}$ is the annual rate of CH4, emissions (CH4, C (ha) ⁺ yr ⁻), <i>T</i> = average annual in temporature (C ²) and <i>W</i> is the water table depth (m). The equation shows a significant correlation with measurements (r ² = 0.54, <i>P</i> > 0.05). The equation shows a significant correlation with measurements (r ² = 0.54, <i>P</i> > 0.05), and an average error of 27 (H4, CH arry "Lignificance on defined due to lack of replicates - Smith et al, 1997).	
Note: Methane emissions from fens. Equation derived by regression analysis against experimental data from 35 measurements (Naya ket al. 2009). The equation derived ways a against experimental data from 35 measurements (Naya ket al. 2009). The equation derived ways and the Naya Ket and Naya	
$\begin{split} R_{co2} &= (3.667/1000) \times ((6700 \times exp(-0.26 \times exp(-0.0515 \times ((Wx100)-50)))) + ((72.54 \times 7) - 800)) \\ where R_{co2} is the annual rate of CO_2 emissions (t CO_2 (ha)^1 yr'), \\ T = average annual peat temperature (°C) and \\ W is the water table depth (m). The equation shows a significant correlation with measurements (r2 = 0.53 P > 0.05). \\ Evaluation against 29 independent experiments shows a significant association (r2 - 0.21; P>0.05) and an average error of 3023 t CO_2 har 'yr 'which is non-significant (C>05) (Smith et al. 1997). \end{split}$	
Note: Carbon dioxide emissions from fins. Equation derived by regression analysis against 44 measurements (Nayak et al. 2009). The equation derived by regression analysis against 44 (2009) , The equation derived by (Wx100)-50)))+(153.23 x 7)) where R_{coc} is the annual rate of CO ₂ emissions (t CO ₂ (ha) ³ yr ³), T a verage annual peat temperature (°C) and Wis the water table depth (m). The equation betwes a significant correlation with measurements (r ² = 0.42, $P > 0.05$). The equation betwes a significant correlation with measurements (r ² = 0.42, $P > 0.05$), and an average entror of 2108 t CO ₂ ha ³ yr ⁴ (significance not defined due to lack of replicates-Smith et al., 1997)	

Note: Methane emissions from acid bogs. As above Note: Methane emissions from fens. As above

Note: CO₂ emissions from acid bogs. As above Note: CO₂ emissions from fens. As above

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Frequently Asked Questions

Click here to email question to

GENERAL	
	lydrologist, EnviroCentre Ltd)
Comment:	I could see the benefit of protected feature on the all the sheets, but it this means we cannot even copy the equations for testing sensitivity of a parameter without changing the entire sheet. The
	protection should be removed as it reduces the usefulness of the tool.
Response:	
	(ydrologist, EnviroCentre Ltd). We adde start the balt the balt are a sub-start of average and a sub-start and the balt of a sub-start and the balt of
Comment:	We miss the carbon payback table that used to be at the bottom of every carbon gain/loss component. Our clients like to see how quickly they can payback C emitted due to individual components.
Posponeo:	This is useful in planning and should be replaced. This feature has been replaced
Response:	
CORE INPUT DATA	
Cameron McIver (Came	ron Feology I (d)
Question:	The note on "extra capacity required for backup (%)" suggests there is a choice of % capacity or % output - I'm not clear how you know which you have chosen.
Response:	The note is misleading. The number that should be entered is the percentage of the actual output of the windfarm (WWh yr ") that is required for backup. Text has been added to the note to clarify
Stephen Lockett (AECO	
Question:	
	Average extent of drainage around drainage features at site (m)
	We have reviewed the guidance but are still unsure of what this variable means. We have used a standard input of 100m but the sheet appears to be extremely sensitive to this variable and we
	have limited confidence on the value chosen. The note in the cell refers to obtaining data on the ground water level but I am unsure how this relates to extent of drainage around drainage features.
Response:	Average extent of drainage around each drainage feature can be measured following the method by Stewart and Lance (1991). In order to determine the extent of drainage, the undrained water
	table depth, and the 95% confidence interval of the measurements are needed.
	Possible approach:
	1. Install a series of dipwells or boreholes both upslope and downslope from the drainage feature.
	2. In the first instance, assume that all dipwells are from undrained areas of the site. This incorrect assumption is used to initialise the iterative process that calculated the water table depth of the
	undrained soil.
	3. For a particular sampling occasion, calculate the mean water table depth and 95% confidence interval from all the available data.
	4. Assume all dipwells with water table depths deeper than the calculated mean water table depth plus the 95% confidence interval are within the area that is drained by a ditch and so exclude these
	from the calculation.
	5. Calculate a new mean water table depth and 95% confidence interval using only data from undrained area.
	6. Repeat the process until the calculation of the mean water table depth and 95% confidence interval has stabilised, and no further data points need to be excluded. This gives the water table depth
	of the undrained soil.
	7. The distance from the drain to the first dipwell where the water table depth of the undrained soil occurred (to within the 95% confidence interval) can then be assumed to be the total extent of the
	drainage impact.
Question:	Our drainage strategy is to mimic the existing drainage patterns as closely as possible by intercepting surface run-off and discharging at regular intervals downstream of the tracks back onto natural
Deenenaci	ground. As such, is there an argument this value could be effectively zero? No – removing water increases the drainage of the site, and this needs to be accounted for. However, if you are following existing drainage patters, it will be easier to determine the extent of
Response:	No – removing water increases the drainage or the site, and this needs to be accounted for. However, if you are rollowing existing drainage patters, it will be easier to determine the extent or drainage because the draina see already established.
Question:	oralinage because the oralins are already established. For our example site there is a significant difference in pay back when using site specific and IPCC default values (ranging from 3 to 15 years). Would you be able to provide a brief description of
Question.	what is being ignored when selecting IPCC default?
Response:	The IPCC default takes no account of the previous condition of the site. It provides the result for a typical acid bog or fen across Europe.
rtooponoo.	Therefore, if you are working with an unusually pristine peat or a badly drained peat, you would expect the result to be very different to the average.
Tanya Ogilvy (SEPA)	
Question:	
Response:	
5c. Volume of peat dra	ined
Stephen Lockett (AECO	
Question:	Our new drainage will be surface swales above the ground water table so should not have any effect on the ground water table.
Response:	If the surface swales will just convey storm water that would not otherwise have percolated into the soil, these swales will have no impact on the water table of the soil profile, but will only impact the
	water that would have runoff the surface, causing erosion. However, if the swales also reduce the amount of water entering the soil profile, then they could have an impact on the wetness of the soil.
	This should really be accounted for in the calculation. However, there is nothing to describe this in the carbon calculator, so you would be justified in neglecting this effect but need to indicate this in
	the notes.
5e. Emission rates from	
Stephen Lockett (AECO	
Question:	Rate of carbon dioxide emission
	We would expect the rate of emission in undrained soil to be worse than the rate in drained soil. This is only the case when the ground water level is very shallow. Does the output define 'drained only undrained soil to be worse than the rate in drained soil to be worse that undrained soil to be worse that the trained to be worse that the trained soil to be worse that the rate in drained soil to be worse that the trained soil to be worse that the rate in drained soil to be worse that when the trained to be worse that the trained to be worse that the trained soil to be worse that when the trained to be worse that when the trained to be worse that the trained soil to be worse that when the trained soil to be worse that the trained soil to be worse that when the trai
Deenenee	soil as soil which is being drained by our engineering activities and 'undrained soil' as excavated soil which was dry to start with?
Response:	
	I think the confusion comes about due to the definition of terms.
	This the consistence on the salvour due to the deminion on terms. The 'drained soil' refers to the soil after it has been drained for the windfarm development. The 'undrained soil' refers to the soil before it was drained for the development. This doesn't refer to the
	The drained solit relets to the solitater in his been drained for the windram development. The unionance solitates to the solitater in was drained in the development. The does in the to the solitates to the solitates to the solitates in the solitates and the solit
	status of the site vertice the development. Agreed, where a trained are relets to a site that has already been unamed on years, more or the lable calibon would already have been lost, and so losses due to the windfarm construction would be much less than the losses from an "undrained site" where the peat was still in pristine condition.
	Not, and so losses due to the windiant construction would be much less than the losses from all undialitied site where the peak was sain in pristine condition. Worksheet Se calculates the rate of emissions of CO2 and CH4 for the soil
	1. when drained (ie dry sol);

In a drained (dry) soil, we expect high rates of CO2 emissions and low rates of CH4 emissions.

In an undrained (wet) soil, we expect high rates of CH4 emissions and low rates of CO2 emissions.

These rates are then used in sheet 5d to calculate the net GHG emissions (in CO2 equivalents) attributable to the windfarm development. This is taken as the difference between the losses following drainage for the development and the losses that were occurring before the soil was drained for the development. Because the net emissions are usually higher in the drained (dry) soil than in the undrained (wet) soil, the net emissions due to draining the site usually come out as positive. If we were to compare a "drained site" and an "undrained site" in sheet 5d, the net CO2 emissions calculated for the drained site would be much less than for the undrained site because a smaller volume of soil is being further drained by the development.

CHANGES IN VERSION 2.1.0			
	Colle	Change	Thanks to
<u>Norksheet</u> Core input data	<u>Cells</u> C31, E31, F31	<u>Change</u> Redundant input for soil pH removed	Thanks to Ffion Causer, Natural Power
orestry input data	c)-/ -)-/ ·)-	Different areas of forestry included	N/A
Construction input data		Different areas of construction included	· · · ·
. Windfarm CO ₂ emission savings		Different areas of forestry included	
. CO2 loss due to turbine life		Different areas of construction included	
a. Volume of peat removed		Different areas of construction included	
ii. Forestry CO2 loss - detail		Different areas of forestry included	
a. C sequest. in trees (3PG)		Different areas of forestry included	
d. Wind speed ratios		Different areas of forestry included	
CHANGES IN VERSION 2.2.0			
<u>orksheet</u>	<u>Cells</u>	<u>Change</u>	Thanks to
onstruction input data . Windfarm CO2 emission saving	C28, C29 F49	"Volume cement" changed to "Volume concrete" =IF(F19=1,365*24*F11*F10*G21/100,SUM(l49,L49,O49,R49,U49)) changed to	Marianne Brownlee, Arcus Renewable Energ Cameron McIver, Cameron Ecology Ltd
-		=IF(D19=1,365*24*F11*F10*G21/100,SUM(I49,L49,O49,R49,U49))	
HANGES IN VERSION 2.3.0			
<u>/orksheet</u> a. Volume of peat removed	<u>Cells</u> F23	<u>Change</u> =IF('Core input data'!C48=1,'Core input data'!C51,'Construction input data'!D17) changed to =IF('Core input	Thanks to Stuart McGowan, Golder Associates
a. volome of pear temoved	125	data!/C48=1, 'Core input data!/C49, 'Construction input data!/D17)	Stourt incolowing dolder Associates
a. Volume of peat removed	G23,H23	Similar to above	
a. Volume of peat removed	F24	=IF('Core input data'!C48=1,'Core input data'!C52,'Construction input data'!D18) changed to =IF('Core	
a. Volume of peat removed	G24,H24	input data'!C48=1,'Core input data'!C50,'Construction input data'!D18) Similar to above	
CHANGES IN VERSION 2.4.0			
Verlaheet	Calla		Theol
<u>Worksheet</u> 5c. Volume of peat drained	<u>Cells</u> F ₃₃	<u>Change</u> =(\$C9+F31+\$C9)*(\$C9+F32+\$C9)-(F31*F32)	Thanks to Stuart McGowan, Golder Associates
e. volume of pear uranieu	' 33	=(\$C9+F31+\$C9)^(\$C9+F32+\$C9)-(F31^F32) (nanged to =ir(F23>0,(\$C9+F31+\$C9)^(\$C9+F32+\$C9)- (F31*F32),0)	Stoart Micdowari, Golder Associates
c. Volume of peat drained	G33-T33	Similar to above	
CHANGES IN VERSION 2.5.0			
<u>orksheet</u>	<u>Cells</u>	Change	Thanks to
ii. Forestry CO2 loss - detail	F55	=F50 ^{-x} F53/F54 changed to =IF(F50>0,F50*F53/F54,0)	Jenny Sneddon, AMEC
i. Forestry CO2 loss - detail	G55-T55	Similar to above	
i. Forestry CO2 loss - detail	F46 G46-T46	=IF(F35="Yes", F44*F45, o) changed to =IF(F35="Yes",IF(F39>o, F44*F45, o),o)	
i. Forestry CO2 loss - detail i. Forestry CO2 loss - detail	G46-146 F63	Similar to above =(F57*'Core input data'!\$E41)-F62 changed to =IF(F55>0,(F57*'Core input data'!\$C41)-F62,0)	
i. Forestry CO2 loss - detail	G63-T63	Similar to above	
i. Forestry CO2 loss - detail	G38	='Forestry input data'!\$F39 changed to ='Forestry input data'!\$H39	
i. Forestry CO2 loss - detail	J38,M38,P38,S38	Similar to above	
i. Forestry CO2 loss - detail i. Forestry CO2 loss - detail	H38 K38,N38,Q38,T38	='Forestry input data'!\$H39 changed to ='Forestry input data'!\$F39 Similar to above	
i. Forestry CO2 loss - detail	D66	=D17+D24+D32-D47-D63 changed to =D17+D24+D32-E47-E63	
i. Forestry CO2 loss - detail	G66, J66, M66, P66, S66	Similar to above	
ii. Forestry CO2 loss - detail ii. Forestry CO2 loss - detail	E66	=E17+E24+E32-E47-E63 changed to =E17+E24+E32-D47-D63 Similar to above	
ii. Forestry CO2 loss - detail c. Volume of peat drained	H66, K66, N66, Q66, T66 C54	Similar to above ='Core input data'!C68 changed to ='Core input data'!C70	SEPA
c. Volume of peat drained	C54 D54, E54	Similar to above	
c. Volume of peat drained	D48	='Core input data'!C\$65 changed to ='Core input data'!E\$65	
c. Volume of peat drained	E48	Similar to above	
c. Volume of peat drained	G33	=IF(G23>0,(\$C9+G31+\$C9)*(\$C9+G32+\$C9)-(G31*G32),0) changed to =IF(G23>0,(\$d9+G31+\$d9)*(\$d9+G32+\$d9)-(G31*G32),0)	
c. Volume of peat drained	J33,M33,P33,S33	$= \Pi(02320)(809+031+809)^{(809+032+809)-(031^{0}32)(0)}$ Similar to above	
c. Volume of peat drained	H ₃₃	=IF(H23>0,(\$C9+H31+\$C9)*(\$C9+H32+\$C9)-(H31*H32),0) changed to	
. Volume of peat drained	J33,M33,P33,S33	=IF(H23>0,(\$e9+H31+\$e9)*(\$e9+H32+\$e9)-(H31*H32),0) Similar to above	
CHANGES IN VERSION 2.6.0	J33,INI33,F 33, J33	Sinnar to above	
/orksheet	<u>Cells</u>	Change	Thanks to
ayback Time and CO2 emissions	D ₃₃		Sarah Lister, Natural Power
ayback Time and CO2 emissions	D34,D35	Similar to above	
ayback Time and CO2 emissions	E33 Fay Far	=E\$31/E9 changed to =E\$31/D9	
ayback Time and CO2 emissions ayback Time and CO2 emissions	E34, E35 D31	Similar to above =D19+D25 changed to =D19+E25	
ayback Time and CO2 emissions	E31	=E19+E25 changed to =E19+D25	
CO2 loss by DOC & POC loss	C11	Contents deleted	Ffion Causer, Natural Power
CO2 loss by DOC & POC loss	D11, E11	Similar to above	
CO2 loss by DOC & POC loss	C26	=(C9+C12+C13+C14+C15+(C10+C17+C18+C19+C20)/C21)/3.66 changed to	
. CO2 loss by DOC & POC loss	D26,E26	=((C9+C12+C13+C14+C15)/3.66)+(((C10+C17+C18+C19+C20)/C21)*(12/16)) Similar to above	
o I need to use this tool	· · · · · · · · · · · · · · · · · · ·	Wording changed to clarify that the tool SHOULD be used with highly organic soils, but COULD also be	SEPA
and a state of the	<i>c</i>	used with sites undergoing drainage or deforestation	
ore input data	C12	Set to 25 and fixed to comply with planning applications for Section 36 (planning period = 25 years)	
ore input data	Row 25	Average depth of peat at site not used - therefore removed	
Windfarm CO ₂ emission saving	D48	Set to AVERAGE(G48, J48, M48, P48, S48) to ensure a value is provided	
Windfarm CO2 emission saving	E37 E37-Lloz	24*365*\$D11 changed to 24*365*E11 Similar to above	Sarah Lister, Natural Power
Windfarm CO2 emission saving e. Emission rates from soils	F37-U37 C34	Similar to above =C28/(C27*10000) changed to =MAX(C28/(C27*10000),C33)	Ffion Causer, Natural Power
e. Emission rates from soils	C34 D34, E34	=C20/C2/~10000/changed to =IMAA(C20/C2/~10000),C33/ Similar to above	
CHANGES IN VERSION 2.7.0			
/orksheet	<u>Cells</u>	Change	Thanks to
. CO2 gain - site improvement	C63	=-12*C61/'1. Windfarm CO2 emission saving'!\$D54 changed to =-12*C60/'1. Windfarm CO2 emission	Sarah Lister, Natural Power
		savinq'!\$D54	
	D63-N63	Similar to above =-12*C62/'1. Windfarm CO2 emission saving'!\$D54 changed to =-12*C60/'1. Windfarm CO2 emission	
	C64	=-12*C62/1. Windfarm CO2 emission saving !\$D54_changed to =-12*C60/1. Windfarm CO2 emission saving!!\$D54	
	D64-N64	Similar to above	
ore input data	C74	Volume of additional peat excavated added to make the calculation more generalised	Rob McCall, Countryside Council for Wales
	E74, G74	Similar to above	
	C75 E75, G75	Area of additional peat excavated added to make the calculation more generalised Similar to above	
	-/J/~/J	Similar to above	

		saving!!\$D54	
	D64-N64	Similar to above	
Core input data	C74	Volume of additional peat excavated added to make the calculation more generalised	Rob McCall, Countryside Council for Wal
	E74, G74	Similar to above	
	C75	Area of additional peat excavated added to make the calculation more generalised	
	E75, G75	Similar to above	
a. Volume of peat removed	Row 64 - 67	Extra lines added to show the additional peat excavated in this sheet	
	C70	=C14+C27+C39+C62 changed to =C14+C27+C39+C62+C65	
	D70, E70	Similar to above	
	C71	$=C_{13}+F_{26}+F_{38}+C_{61}$ changed to $=C_{13}+F_{26}+F_{38}+C_{61}+C_{66}$	
Core input data	B72	"Depth of cable trenches" change to "Average depth of peat cut for cable trenches (m)" to avoid	
		overestimation of peat affected by cable trenches in shallow peats	
ore input data	Row 91	New input: Water table depth in borrow pit before restoration	Sarah Lister, Natural Power
	Row 95	New input: Water table depth around foundations and hardstanding before restoration	
. CO2 gain - site improvement	Row 15	Deleted	
	C15 (previously C16)	='Core input data'!C45 changed to ='Core input data'!C91	
	l15, M15	Similar to above	
	D15 (previously D16)	='Core input data'!C50 changed to ='Core input data'!C95	
	J15, N15	Similar to above	
d. CO2 loss from drained peat	C43	=C8*(C35+C36)*((C42*C34))/365 changed to =C8*(C35+C36)*((C42*(365-C34)))/365	University of Aberdeen
	D43, E43	Similar to above	
. CO2 loss due to turbine life	C9	='Core input data'!C21*C12*'Core input data'!C14*'1. Windfarm CO2 emission saving'!D48/100 changed	Adrian Barnes, WSP Environment & Ene
	-	to ='Core input data'!C21*C12*'Core input data'!C14	
	D9,E9	Similar to above	

CHANGES IN VERSION 2.7.2

Worksheet	Cells	Change	Comment	Thanks to
8. CO2 gain - site improvement	C13	='Core input data'!C80 changed to =IF('Core input data'!C81>'Core input data'!C82,'Core input		Ffion Causer, Natural Power
		data'!C8o,o)		
	G13, K13	Similar to above		
	D13	='Core input data'!C85 changed to =IF('Core input data'!C86>'Core input data'!C87,'Core input data'!C85,	0)	
	H13,L13	Similar to above		
	E13	='Core input data'!C90 changed to =IF('Core input data'!C91>'Core input data'!C92,'Core input		
		data'!C90,0)		
	l13, M13	Similar to above		
	F13	='5c. Volume of peat drained'!C34/10000 changed to =IF('Core input data'!C95>'Core input data'!C96,'5c.		
	-	Volume of peat drained'!C34/10000,0)		
	J13, N13	Similar to above		

CHANGES IN VERSION 2.8.0

		-		
<u>Worksheet</u> 5c. Volume of peat drained	<u>Cells</u> Rows 67 - 76	<u>Change</u> Inserted rows to included additional excavated peat in volume of peat drained	<u>Comment</u> Include additional excavated peat in volume of peat drained	Thanks to Susana Sebastian, SEPA
	C67-C68; D67-D68; E67-E68	Title lines	in volume of peat drained	
	C69	='Core input data'!C74		
	D69,E69	Similar to above		
	C70	='Core input data'!C75		
	D70,E70	Similar to above		
	C71	=IF(C70>0,C69/C70,0)		
	D71,E71 C72	Similar to above =SQRT(C70/PI())		
	C/2 D72,E72	Similar to above		
	C73	=C72+C9		
	D73,E73	Similar to above		
	C74	=(PI()*C73*C73)-C70		
	D74,E74	Similar to above		
	C75	=C74*C71		
	D75,E75	Similar to above		
	C79 D79,E79	=C18+C34+C57+C64		
	C80	=C19+C35+C58+C65 changed to =C19+C35+C58+C65+C75		
	D80,E80	Similar to above		
ii. Forestry CO2 loss - detail	F62	=F60*F61 changed to =F60*F61*F55	Calculation of emissions associated	Susana Sebastian, SEPA
			to the transport of wood to	
			biomass plant should account for	
	G62-T62	Similar to above	number of trips to plant	
Forestry input data	C23	Units changed from g CO ₂ km ⁻¹ to g CO ₂ km ⁻¹ t ⁻¹		
Core input data	Row 25	Insert input for average depth of peat at site	Limit improvements following	Susana Sebastian, SEPA
3. CO2 gain - site improvement	Row 15 C15	Insert average depth of peat at site ='Core input data'!C25	restoration to the depth of the peat	
	D15-N15 (excl. E15, I15 & M15)			
	E15	='Core input data'!C46		
	l15,M15	Similar to above		
	C16	Core input data'!C82 changed to =IF('Core input data'!C82 <c15,'core data'!c82,c15)<="" input="" td=""><td></td><td></td></c15,'core>		
	D16-N16	Similar to above		
	C17	='Core input data'!C83 changed to =IF('Core input data'!C83 <c15,'core data'!c83,c15)<="" input="" td=""><td></td><td></td></c15,'core>		
	D17-N17	Similar to above		
	C21 D21-N21	C12-C20 changed to =IF(C12-C20>0,C12-C20,0) Similar to above		
Core input data	Rows 85, 91, 97		Improvements in C sequestration	Rob McCall, NRW
3. CO2 gain - site improvement	C12	='Core input data'!C12 changed to ='Core input data'!C85	should continue for as long as the	,
	D12-N12 (excl. E12, I12 & M12)) Similar to above	improvement can be guaranteed.	
Payback Time and CO2 emissions	Row 37		Include calculation of ratio of soil	Rob McCall, NRW
	C ₃₇	=IF(C26<0,-(C17+C18)/C26,0)	losses to gains	
	D637,E37	Similar to above		Current Coherting CEDA
Payback Time and CO2 emissions	Row 38 C38	Insert ratio of C emissions to power generation =((C20+C26)*1000000)/(C12*1000)	Include calculation of C emissions to power generation	Susana Sebastian, SEPA
	D637,E37	Similar to above	to power generation	
5. Loss of soil CO2	D11	=D8+D9 changed to =MIN(D8+D9,E8+E9)	Correct use of minimum and	Peter Batten
	E11	=E8+E9 changed to =MAX(D8+D9,E8+E9)	maximum wrt water table depth at	
e. Emission rates from soils	D31	='Core input data'!E24 changed to ='Core input data'!G24	very low depths	
	E31	='Core input data'!G24 changed to ='Core input data'!E24		
	D33	='Core input data'!E28 changed to ='Core input data'!G28		
COs asin site improvement	E ₃₃	='Core input data'!G28 changed to ='Core input data'!E28	Correct use of minimum and	la Smith University of
3. CO2 gain - site improvement	G17	=IF('Core input data'!E83 <g15,'core changed="" data'!e83,g15)="" data'!g83,g15)<="" data'!g83<g15,'core="" input="" td="" to="IF('Core"><td>Correct use of minimum and maximum depth of water table</td><td>Jo Smith, University of Aberdeen</td></g15,'core>	Correct use of minimum and maximum depth of water table	Jo Smith, University of Aberdeen
	H17-J17	Similar to above	after restoration	/ Delucell
	K17	=IF('Core input data'!G83 <k15, 'core="" changed="" data'!g83,k15)="" input="" input<="" td="" to="IF('Core"><td></td><td></td></k15,>		
		data'!E83 <k15,'core data'!e83,k15)<="" input="" td=""><td></td><td></td></k15,'core>		
	L17-N17	Similar to above		
3. CO2 gain - site improvement	G12	='Core input data'!E85 changed to ='Core input data'!G85	Correct use of min/max period	Jo Smith, University of Aberdeer
	H12-J12	Similar to above	when restoration can be restored	
	K12	='Core input data'!G85 changed to ='Core input data'!E85		
	L12-N12	Similar to above		
3. CO2 gain - site improvement	C34	=IF('Core input data'!\$C\$112=2,'8. CO2 gain - site improvement'!C30,'8. CO2 gain - site improvement'!C32) changed to =IF('Core input data'!\$C\$112=2,IF('Core input data'!\$C\$23=1,C30,C31),IF('Core input data'!\$C\$23=1,C32,C33)	Correct selection of emission factor when soil type is fen	Elizabeth Keen, Peter Brett Associates LLP
		Similar to above		
	D34-N34			
	D34-N34 C53	=IF('Core input data'!\$C\$112=2,'8. CO2 gain - site improvement'!C49,'8. CO2 gain - site improvement'!C51)		
		=IF('Core input data'!\$C\$112=2,'8. CO2 gain - site improvement'!C49,'8. CO2 gain - site improvement'!C51)		

CHANGES IN VERSION 2.9.0

<u>Worksheet</u> Core input data	<u>Cells</u> B94 B95	<u>Change</u> "Water table depth in borrow pit before restoration (m)" changed to "Depth of water table in borrow pit before restoration with respect to the restored surface (m)" "Water table depth in borrow pit after restoration (m)" changed to "Depth of water table in borrow pit after restoration with respect to the restored surface (m)"		Thanks to Clare Wharmby - Carbon Forecast
8. CO2 gain - site improvement	C47	=(23*16/12)*C\$13*C\$40*C46*(C\$19/365) changed to =(23*16/12)*C\$13*C\$40*C46*(C\$38/365)	Error in formula using the improved flooded period instead of the unimproved flooded period	Elizabeth Keen - Peter brett Associates

	D47-N47	Similar to above		
7c. Average stand data	Rows 13-29	Stand data extended from 17 year to o years	If forest stand is less than 17 years old, the calculations fail	Brenda Park - AMEC
	Rows 168-86	Similar to above		
7ii. Forestry CO2 loss - detail	F31	=IF(F29>0,IF(F27="Deep Peat",(VLOOKUP(F29,'7c. Average stand		
		data'!\$D\$87:\$G\$118,3)),(VLOOKUP(F29,'7c. Average stand data'!\$D\$30:\$G\$63,3))),0) changed to		
		=IF(F29>0,IF(F27="Deep Peat",(VLOOKUP(F29,'7c. Average stand		
	G31-T31	data'!\$D\$68:\$G\$118.२1).(VLOOKUP(F29.'7c. Average stand data'!\$D\$1२:\$G\$6२.२1)).o) Similar to above		
7ii. Forestry CO2 loss - detail	G ₃₅	=IF('Forestry input data'!\$F\$33=1,"Yes", "No") changed to =IF('Forestry input data'!\$D\$33=1,"Yes", "No")	Use of felled wood as biofuel not	Jo Smith - University of
			correctly read in min and max	Aberdeen
			calculations	
	H35,J35,K35,M35,N35,P35,Q3	5 Similar to above		
	,S35,T35			
7ii. Forestry CO2 loss - detail	F16	='7a. C sequest. in trees (3PG)'!\$F\$24_changed to =IF(F12>0,'7a. C sequest. in trees (3PG)'!F\$24,0)	Avoid #NA	Claire Frost - AECOM
	G16-T16	Similar to above		
Forestry input data	Note: Emissions from felling	"the emissions are 6657 g CO $_2$ m ⁻³ " changed to "the emissions are 6675 g CO $_2$ m ⁻³ "		Jonathon Davison - Mott
	and timber removal.			MacDonald
Forestry input data	Note: Emissions associated	"3933000 g CO ₂ km ⁻¹ (range 3850000 – 4015000 g CO ₂ km ⁻¹ - average = 39.33 g CO ₂ km ⁻¹ t ⁻¹)" changed to		Jonathon Davison - Mott
	with transportation	"39.33 g CO ₂ km ⁻¹ t ⁻¹ (range 38.5 – 40.15 g CO ₂ km ⁻¹ t ⁻¹ - average = 39.33 g CO ₂ km ⁻¹ t ⁻¹)"		MacDonald
Payback Time and CO ₂ emissions	C ₃₇	=IF(C26<0,-(C17+C18)/C26,"No gains!")	Ensure no restoration is highlghted	Sarah Lister, Natural Power
	D637,E37	Similar to above	as no gains rather than appearing	
Payback Time and CO2 emissions	C38	=((12/44)*(C20+C26)*1000000)/(C12*1000)	Express ratio as CO2 rather than C	Sarah Lister, Natural Power
	D637,E37	Similar to above	emissions to power generation	

Appendix 6.E Carbon Calculator - Justification for Values Used

6E1

Appendix 6.E – Enoch Hill Wind Farm - Justification for Values Used in Carbon Calculator

Input data	Enoch Hill Wind Farm			Comments/Assumptions
	Expected	Minimum	Maximum	
Wind Farm Characteristics	6			
Dimensions				
No. of turbines	19	19	19	Number of turbines included in Proposed Development.
Lifetime of wind farm	25	25	25	Standard lifetime used by Nayak et al.
Power rating of turbines	3.3MW	3.3MW	3.3MW	3.3MW is the candidate turbine in the ES as outlined in Chapter 4.
Capacity factor	27%	21.7%	33.6%	Average capacity factor in Scotland between 2009-2014 ¹ is 27%. Minimum and maximum values inserted as a range.
Extra capacity required for back up	5	0	5	Following the guidance provided by Nayak <i>et al</i> , UK Energy in brief 2013 ² confirms that wind energy accounts for less than 20% of total national electricity generation therefore 0% could be used however 5% has been used to reflect a worst case scenario 0% is entered as a minimum value.
Additional emissions due to thermal inefficiency of back up generation (%)	10	10	10	Default used by Nayak <i>et al.</i>
Carbon dioxide emissions from turbines life	Ca	lculate w.r.t installed c	apacity	Total CO₂ emission calculated using installed capacity (default equation provided in spreadsheet).
Peatland Characteristics befo	re wind developr			
Average annual air temperature at site (°C)	7.5	3.9	11.2	Average annual temperature taken for Eskadalemuir Met Office station 1981- 2010 ³ . Expected value calculated using average of minimum and maximum average temperatures. Maximum and minimum chosen as a range.

¹ <u>https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/437811/et6_1.xls_Renewable_electricity_capacity_and generation (ET 6.1)</u> Last accessed 03/07/2015

² https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/224130/uk_energy_in_brief_2013.PDF Last accessed 13/12/13

³ <u>http://www.metoffice.gov.uk/climate/uk/averages/19812010/sites/eskdalemuir.html</u> Last accessed 06/10/2014



Input data	Enoch Hill Wind Farm			Comments/Assumptions
	Expected	Minimum	Maximum	
Average peat depth at site	0.68	0.5	1.0	Expected value calculated as average value of all 1,581 peat depth measurements taken at site. Minimum and maximum values chosen as a range. See Peat Management Plan (PMP) ES Appendix 6.A for calculations.
Content of dry peat % by weight	55	49	62	Calculated using typical values provided in carbon balance spreadsheet.
Average extent of drainage around drainage features at site (m)	7.5	5	10	No site specific measurements available, precautionary values used.
Average water table depth at site (m)	0.3	0.2	0.4	Expected value is average across all 1,581 measurements taken at site where water table depth is estimated to be equivalent to catotelm thickness. Detailed water table depth measurements were not taken.
Dry soil bulk density (gcm ^{·3})	0.25	0.20	0.45	Due to lack of site specific information, indicative figures from National Soil Inventory of Scotland have been used.
Characteristics of bog plants				
Time required for regeneration of bog plants after restoration (years)	3	2	5	Estimated values, based on condition of the current vegetation.
Carbon accumulation due to C fixation by bog plants in undrained peat (tC ha ⁻¹ yr ⁻¹)	0.25	0.12	0.31	Default values provided by Nayak <i>et al.</i>
Forestry Plantation Character	istics			
Enter simple data				
Area of forestry plantation to be felled (ha)	0	0	0	No forestry felling is expected.
Average rate of carbon sequestration in timber	n/a	n/a	n/a	
Counterfactual emission facto	ors			
Coal-fired plant emission factor tCO ₂ MWh ⁻¹	0.907	0.907	0.907	Provisional values for 2013 published in Chapter 5 of DUKES 2014 ⁴ .
Grid mix emission factor tCO_2MWh^{-1}	0.454	0.454	0.454	Provisional values for 2013 published in Chapter 5 of DUKES 2014.
Fossil fuel mix emission factor tCO_2MWh^{-1}	0.701	0.701	0.701	Provisional values for 2013 published in Chapter 5 of DUKES 2014.
Borrow Pits				
Number of Areas	1	1	1	Three potential borrow pit search areas have been identified as described in Chapter 4 of the ES. However only one area is on true peat (>0.5m in depth).

⁴ <u>https://www.gov.uk/government/statistics/digest-of-united-kingdom-energy-statistics-dukes-2014-printed-version</u> Last accessed 06/06/2014



Input data	Enoch Hill Wind Farm			Comments/Assumptions
	Expected	Minimum	Maximum	
Average length of area (m)	100	50	150	
Average width of areas (m)	100	50	150	
Average depth of peat removed from area (m)	1.05	1.00	1.10	Average peat depth in borrow pit - see PMP (ES Appendix 6.A).
Foundations and hard-standing	ng area associate	ed with each turbine		
Average length of turbine foundations (m)	27.5	25	27.5	An excavation area of 27.5m square is expected (and worst case).
Average width of turbine foundations (m)	27.5	25	27.5	As above.
Average depth of peat removed from turbine foundations (m)	0.95	0.75	1.25	Average peat depth values taken from peat excavation calculations across all 19 turbine locations. See PMP, ES Appendix 6.A for calculations. Minimum and maximum entered as a range.
Average length of hard standing	50	50	50	Hardstandings are 50 x 25m. Additional area not required for excavation as not deep.
Average width of hard standing	25	25	25	As above.
Average depth of peat removed from hardstanding (m)	0.69	0.5	1.0	Average peat depth values taken from peat excavation calculations done for the PMP for turbine and hardstanding locations. See PMP, ES Appendix 6.A for calculations. Minimum and maximum entered as a range.
Access tracks				
Total length of access tracks (m)	12,900	12,900	12,900	As outlined in ES Chapter 4 , the total value Includes new cut and floating track length as outlined in Chapter 4 of ES.
Existing tracks length (m)	n/a	n/a	n/a	No upgrading of existing track on this site.
Length of access tracks that is floating road (m)	1,900	1,800	2,000	Expected value is taken from PMP (ES Appendix 6.A). Minimum and maximum entered as a range to allow for variations following detailed site investigation.
Floating road width (m)	6	6	6	As per Figure 4.3 in ES.
Floating road depth (m)	0.5	0.5	0.5	As per Figure 4.3 in ES.
Length of floating road that is drained (m)	1,900	1,800	2,000	Assume the full length of floating road is drained, will be confirmed following detailed ground investigation.
Average depth of drains associated with floating roads (m)	0.5	0.5	0.5	Assume drain depth of 0.5m.



Input data	In	put	data
------------	----	-----	------

Enoch Hill Wind Farm

Comments/Assumptions

	Expected	Minimum	Maximum	
Length of access track that is excavated road (m)	11,000	10,500	11,500	Total new track length as outlined in ES Chapter 4 allowing for 1.9km of floating road. Minimum and maximum entered as a range to allow for variations following detailed site investigation.
Excavated road width (m)	6	6	6	As per Figure 4.3 in ES.
Average depth of peat excavated from road (m)	0.58	0.50	0.70	Average peat depth value calculated from peat depth measurements along new track used. See PMP, ES Appendix 6.A for calculations. Minimum and maximum entered as a range.
Length of access track that is rock filled road (m)	0	0	0	All new track is expected to be excavated road.
Rock filled road width (m)	0	0	0	
Rock filled road depth (m)	0	0	0	
Length of rock filled road that is drained (m)	0	0	0	
Average depth of drains associated with rock filled roads (m)	0	0	0	
Cable Trenches				
Length of any cable trench on peat that does not follow access track and is lined with a permeable material (m)	0	0	0	Assume full length of cable route to follow access track.
Depth of cable trench	0	0	0	
Additional peat excavated (no	ot accounted for a	above)		
Volume of additional peat excavated (m3)	20,258	19,500	21,000	Total volume of excavated peat for primary and secondary compound, control building, met masts and passing places along access tracks.
Area of additional peat excavated (m ²)	34,400	33,050	35,595	Area of infrastructure as per site layout and described in ES Chapter 4 (minimum and maximum figures calculated assuming peat depth of 0.59m calculated from volume above). See PMP, ES Appendix 6.A for calculations.
Peat Landslide hazard				
Peat landslide hazard risk assessment				Measures have been taken to limit risk. See Peatslide Hazard and Risk Assessment (ES Appendix 6.B).
Improvement of C sequestrat	ion at site by bloo	cking drains, restorati	ion of habitat etc.	
Improvement of degraded bog				
Area of degraded bog to be improved (ha)	0	0	0	n/a



Input data	Enoch Hill Wind Farm			Comments/Assumptions
	Expected	Minimum	Maximum	
Water table depth in degraded bog before improvement (m)	n/a	n/a	n/a	n/a
Water table depth in degraded bog after improvement (m)	n/a	n/a	n/a	n/a
Time required for hydrology and habitat of bog to return to its previous state on restoration (years)	n/a	n/a	n/a	n/a
Period of time when effectiveness of the improvement in degraded bog can be guaranteed (years)	n/a	n/a	n/a	n/a
Improvement of felled plantation				
Area of felled plantation to be improved (ha)	0	0	0	There will be no felled plantation within the Development Site.
Water table depth in felled area before improvement (m)	0	0	0	
Water table depth in felled area after improvement (m)	0	0	0	
Time required for hydrology and habitat of felled plantation to return to its previous state on restoration (years)	0	0	0	
Period of time when effectiveness of the improvement in felled plantation can be guaranteed (years)	0	0	0	
Restoration of peat removed from borrow pits				
Area of borrow pits to be restored (ha)	5	4	5	As outlined in the PMP provided in ES Appendix 6.A . Minimum and maximum entered as a range.
Depth of water table in borrow pit before restoration with respect to the restored surface (m)	0.3	0.2	0.4	Estimated water table depth in borrow pit before restoration. Using average water table depth.
Depth of water table in borrow pit after restoration with respect to the restored surface (m)	0.3	0.2	0.4	Restored water table depth expected (estimated to be restored to previous value).
Time required for hydrology and habitat of borrow pit to return to its previous state on restoration (years)	3	2	4	Estimated time input for the expected case, minimum and maximum entered as a range.
Period of time when effectiveness of the restoration of peat removed from borrow pits can be guaranteed (years)	22	23	21	The restoration measures are expected to last the lifetime of the wind farm (i.e. following restoration to previous state).
Removal of drainage from foundations and hardstanding				Assume no removal of drainage.



Input data	Enoch Hill Wind Farm			Comments/Assumptions
	Expected	Minimum	Maximum	
Water table depth around foundations and hardstanding before restoration	0	0	0	
Water table depth around foundations and hardstanding after restoration	0	0	0	
Time to completion of backfilling, removal of any surface drains and full restoration of the hydrology (years)	0	0	0	
Restoration of site after deco	mmissioning			
Will you attempt to block any gullies that have formed due to the wind farm?	Yes	Yes	No	Assumes that any gullies caused by construction of the wind farm would be blocked to maintain habitats except worst case scenario (maximum column
Will you attempt to block all artificial ditches and facilitate rewetting?	No	No	No	
Will the habitat of the site be	restored on deco	ommissioning		
Will you control grazing on degraded areas?	Yes	Yes	Yes	If required.
Will you manage areas to favour reintroduction of species	No	No	No	



Construction Input Data

Number of turbines in this area	19	19	19	Number of turbines included in proposed development.
Turbine foundations				
Depth of hole dug when constructing foundations	0.3	0.3	0.3	Based on Figure 4.13 in the ES.
Approximate geometric shape of hole dug when constructing foundations	Rectangular	Rectangular	Rectangular	Circular or square geometry not available as an option.
Length at surface (m)	27.5	25	27.5	Based on Figure 4.13 in the ES, adjusted dimensions for a rectangula geometry.
Width at surface (m)	27.5	25	27.5	Based on Figure 4.13 in the ES, adjusted dimensions for a rectangula geometry.
Length at bottom (m)	25	25	25	Based on Figure 4.13 in the ES, adjusted dimensions for a rectangula geometry.
Width at bottom (m)	25	25	25	Based on Figure 4.13 in the ES, adjusted dimensions for a rectangula geometry.
Hardstanding				
Depth of hole dug when constructing hardstanding	0.6	0.6	0.6	Based on Figure 4.4 in the ES and details in Chapter 4.
Approximate geometric shape of hole dug when constructing hardstanding	Rectangular	Rectangular	Rectangular	
Length at surface (m	50	50	50	Based on Figure 4.4 in the ES.
Width at surface (m)	25	25	25	Based on Figure 4.4 in the ES.
Length at bottom (m)	50	50	50	Based on Figure 4.4 in the ES.
Width at bottom (m)	25	25	25	Based on Figure 4.4 in the ES.
Is piling used?	No	No	No	Based on Figure 4.4 in the ES.
Volume of concrete used per turbine base (m3)	750	500	750	Calculated from area of turbine foundations and depth of excavation Range given to allow for a range of candidate turbines, with 750m ³ being the largest.