RWE Renewables UK Onshore Wind

Lorg Wind Farm

Peat Landslide Risk Assessment

This report was prepared by WSP Environment & Infrastructure Solutions UK Limited (formerly known as Wood Environment & Infrastructure Solutions UK Limited), company registration number 02190074, which is carrying out these services as a subcontractor and/or agent to Wood Group UK Limited

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Executive summary

Purpose of this report

This report has been produced for the purpose of presenting the findings of a desk-based review of site information, peat survey results and the Peat Landslide Risk Assessment conducted in accordance with the Scottish Government best practice guide.

Desk Study

The Development Site is located at approximate central Ordnance Survey National Grid reference 266238, 600967 approximately 11.5km south-southeast of New Cumnock in East Ayrshire and 13km southwest of Sanquhar in Dumfries and Galloway. The Development Site boundary straddles the boundary of the two counties and covers an area of approximately 1,242 hectares comprising very steeply undulating upland predominantly used for sheep and cattle grazing.

A Digital Terrain model (DTM) indicates that the Development Site lies at an elevation of between 255m above Ordnance Datum (AOD) and 642m AOD. The Development Site contains a number of promontories including Altry Hill, Fortypenny Hill, High Countham, Black Hill, Cairn Hill and Coranbae Hill in the southeast and Alhang, Alwhat, Brown Hill, Ewe Hill, Lorg Hill and Mid Rig in the northwest. The topography of the Development Site through the centre comprises a very steep sided 'U' shaped glacial valley with very steep slopes. In the location of the turbine arrays in the southeast and northwest the topography comprises a shallow sloped basin. The DTM indicates that the slope angles range between 0° and 55°.

The National Soil Map of Scotland (1:250,000) indicates that the northwest is dominated by peaty podzols on the mid and upper slopes with the valley bottoms dominated by mineral gleys. In the centre of the Development Site the steep mid and lower slopes are dominated by mineral podzols and in valley bottom is shown to comprise peaty gleys and brown soils. In the southeast the soils are shown to comprise peaty gleys across the hill tops and with peat dominating the far southeast.

The NatureScot Carbon and Peatland 2016 map indicates that the soils throughout the central and northwest parts of the Development Site are predominantly soils that are mostly carbon-rich with some deep peat (Class 3) and mineral soils (Class 0). Areas unlikely to include carbon-rich soils (Class 4) are identified on the hill tops. In the southeast the soils are dominated by carbon-rich and deep peat with all cover priority peatland habitats (Class 1). In addition, small areas of no recorded peatland habitat (Class 5) are indicated over the hill tops in the far southeast of the Development Site.

British Geological Survey (BGS) mapping indicates that the northwest and southeast of the Development Site are dominated by peat along the lower shallower slopes between the hill tops. The remainder of the Development Site is shown to be underlain by thin or absent deposits over the hill tops and glacial deposits including Glacial Till and Hummocky Glacial Deposits across the mid and lower slopes.

The central and southeast of the Development Site forms the upper catchment of the Water of Ken and the northwest beyond the Alwhat / Alhang col forms the upper reaches of the Afton Water which drains into Afton Reservoir approximately 0.5km northwest of the Development Site. The Development Site contains several small named and unnamed tributaries to the Water of Ken and Afton Water. The SEPA Water Classification Hub indicates that the Water of Ken is classified as having an overall status of Poor and the Afton Water is classified as having an overall status of Good Ecological Potential.

A review of available historical and contemporary imagery has been undertaken which has identified features including peaty-debris slides, gripping, gullies, flushes, pools and hagging.

Field Surveys

A programme of peat depth surveys has been undertaken by WSP (previously Wood) in general accordance with the Scottish Government guidance. In total, peat depth surveys undertaken at the Development Site have comprised 4,158 peat depth measurements which have revealed peat depths ranging between 0.00m and 3.80m. A total of 2,415 (~58%) recorded peat depths ≥0.5m and the calculated mean of all peat depths ≥0.5m was 1.08m.

The peat depth data obtained during the surveys has been used to generate an interpolated peat depth map for the Development Site which indicates that it contains three principal bogs. These are located in the southeast within the lower lying and flatter slopes around the Fans of Altry, in the northwest in the lower lying slopes between Ewe Hill, Brown Hill, Alwhat and Alhang and also through the Afton Water valley in the far northwest of the Development Site.

During the peat surveys a number of geomorphological features including peat grips, relic peaty-debris slides, slope creep terraces, translational failures, tension cracks and a possible deep seated landslide were identified. In addition, natural surface and sub-surface drainage and erosion related features were identified including peat pipes, pipe collapses, gullies, flushes, springs, haggs and active scarps.

Peat Landslide Risk Assessment

An assessment of peat landslide risk has been undertaken in general accordance with the Scottish Government best practice guide. The likelihood of peat instability occurring has been determined from a review of the contributing hazard factors including slope angle, peat depth, slope curvature, natural drainage, artificial drainage, pre-failure indicators and geology. In addition, a semi-quantitative peat slope stability assessment has been undertaken using the 'Infinite Slope' method to support the likelihood assessment.

The results of the likelihood assessment indicate that the Proposed Development is predominantly within areas of Negligible or Unlikely peat slide susceptibility. However, areas of Likely or greater peat slide susceptibility have been identified along some access tracks in the northwest and southeast, at borrow pit A and at the turbine and/or the crane pads for T1, T2, T3, T6, T7, T9, T10, T11 and T14. These general relate to areas with factor of safety values <1.4 and/or slopes with susceptible peat depths and slope angles, the presence of, or conditions likely to be conducive to, the presence of hazardous natural drainage.

An assessment of peat landslide consequences on key receptors including human receptors, public infrastructure, property, surface water, cultural and heritage sites and ecology has been undertaken to support the risk assessment. It is noted that the consequence of a peat landslide in the northwest of the Development Site are greatest through the Afton Water catchment as impacts within the catchment are likely to result in pollution of the reservoir by suspended solids and sudden increases in nutrient content given the distance to the receptor.

The result of the peat landslide risk assessment indicate that the Proposed Development is predominantly in areas of Negligible to Low Risk of peat slide failure. However, areas of Moderate and High risk have been identified throughout the mid and upper slopes of the Afton Water catchment in the northwest of the Development Site. This includes at temporary compound A, borrow pit A, the blade laydowns for T11 and T13 and along the access tracks to T11, T13 and T15. In the southeast areas of Moderate risk have been identified along some of the access tracks and at the blade laydown for T3. In addition a number of small areas of High risk have been identified at the head of the Alhang Burn to the east of T13 and upslope of temporary compound A.

In general the Moderate and High risks in the northwest of the Development Site are principally driven by the higher consequence of a slide on the Afton Reservoir which is a source of public drinking water.

Recommendations

A post-consent detailed ground investigation is recommended to assist in detailed assessment of peat slope stability in the most sensitive areas of the Proposed Development. It is recommended that ground investigation information is used to check/verify the peat slope stability assessments.

It is also recommended that primary mitigation measures are considered to relocate infrastructure from areas susceptible to peat landslides followed by mitigation to reduce peat landslide risks particularly where crossing peat pipes, flushes, peat grips and drainage ditches. The mitigation measures employed should aim to minimise additional loading or undercutting of susceptible peat covered slopes (especially convex slopes), maintain the current drainage of the peat, avoid ponding of surface water and where necessary redirect drainage to a purpose-built drainage network. In addition, monitoring of slopes may be required where a detailed ground investigation of the proposed infrastructure confirms that sensitive slopes may be moderately susceptible to peat landslides.

In conjunction with the above, a geotechnical risk register should be developed and maintained by a Geotechnical Engineer throughout the life cycle of the Proposed Development. During construction, a Geotechnical Clerk of works should also be present on site to monitor sensitive slopes for movement and to manage any changes to the peat landslide risks.

Contents

1. Introduction

1.1 Background

WSP Environment and Infrastructure UK Limited (WSP) has been commissioned by RWE Renewables UK Onshore Wind ("the Applicant") to prepare a Peat Landslide Risk Assessment (PLRA) in support of the Section 36 Application for the proposed Lorg Wind Farm ("the Proposed Development").

In December 2015, a planning application for a wind farm at the Development Site was submitted to Dumfries and Galloway Council (DGC) and East Ayrshire Council (EAC) under the Town and Country Planning (Scotland) Act 1997 (as amended). The wind farm was originally proposed to comprise fifteen turbines, but over the course of the Environmental Impact Assessment and in consultation with statutory consultees and other stakeholders the Proposed Development was revised down to nine turbines in the southeast of the Development Site. The nine turbine layout ('the Consented Development') was granted consent by DGC and EAC in 2019. The Applicant is applying to the Scottish Government for consent under Section 36 of the Electricity Act 1989 for the construction and operation of the Proposed Development on the site of the Consented Development. The revisions to the layout are principally an increase in the number of the turbines to include a western array and additional access tracks as detailed in Section 1.3.

A previous assessment of the Consented Development undertaken by Amec Foster Wheeler Environment & Infrastructure UK Limited (now WSP) identified that the Development Site contains blanket peat and peaty soils as well as slope angles greater than 2 degrees. As such, in accordance with Scottish Government best practice guidance[1] Figure 1.1 (Scottish Government, 2017) a Peat Landslide Risk Assessment is required to support the Environmental Impact Assessment (EIA) and section 36 Application for the Proposed Development.

1.2 Scope and Purpose

The purpose of this report is to present the findings of a desk-based review of site information, peat survey results and a PLRA that has been conducted in accordance with the Scottish Government best practice guide[1]. The peat landslide risk assessment comprises the following scope of work:

- a review of desk-based information including geological, soil, hydrological and hydrogeological data;
- a description of the findings and results of site reconnaissance and peat depth surveys;
- identification of salient geomorphological features related to processes of peat erosion, drainage and mass movement;
- identification and assessment of potential peat landslide hazards;
- preliminary quantitative slope stability assessment by infinite slope analysis using geotechnical parameters derived from literature sources; and,
- peat landslide risk assessment using the principles set out in the best practice guide.

[1] Scottish Government (2017) Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments

1.3 Proposed Development

The Proposed Development comprises the following principal components:

- Up to 15 wind turbines split over two arrays in the northwest and southeast of the Development Site;
- Access tracks connecting between infrastructure elements and the operational Afton Wind Farm adjacent to the west of the Development Site;
- Hard standing areas including crane pads, blade laydowns and storage areas;
- Borrow pits (to be located within the two borrow pit search areas);
- Two permanent anemometer masts;
- Two construction compounds; and
- On-site electrical infrastructure including a wind farm control building and a Scottish Power Energy Networks (SPEN) 132/33kV substation and underground cabling between these buildings and the turbines.

The Proposed Development layout is shown on **Figure 2.0** in **Appendix A**.

1.4 Assessment Methodology

The assessment methodology uses a qualitative assessment of the peat slide and bog flow hazards supported by field observations and a deterministic approach supported by field observations and published literature. The preliminary risk assessment is based on the following approach:

- a desk-based review of site information;
- Phase 1 peat depth survey and site reconnaissance of the developable area;
- Phase 2 peat depth survey of the Proposed Development layout;
- identification of the hazards and consequences;
- preliminary slope stability analysis based on literature sources; and,
- peat landslide risk assessment.

The risk assessment uses the results of the qualitative and deterministic approaches to allocate levels of peat landslide risk for peat slides and bog flows spatially across the Development Site in accordance with the risk level in the best practice guidance.

1.5 Sources of Information

The following sources of information have been used in conjunction with available information listed in the bibliography:

- Ordnance Survey mapping;
- Publicly available aerial photography;
- British Geological Survey (BGS) digital geological mapping;
- James Hutton Institute soil maps;
- Scotland's Environment website;

- NatureScot website;
- Digital Terrain Models (DTM);
- East Ayrshire Council Private Water Supply data;
- Dumfries and Galloway Council Private Water Supply data; and,
- Lorg Wind Farm, Peatslide Hazard and Risk Assessment, Amec Foster Wheeler, June 2017.

1.6 Project Team

The field surveys undertaken by WSP (including by Amec Foster Wheeler) were led by the author (Benjamin Amaira) and issuer (Richard Bagnall) of the peat landslide risk assessment accompanied by a team of surveyors that included various disciplinary backgrounds such as geotechnical engineers, geo-environmental engineers, civil engineers and ecologists. The experience of peat surveying team ranged from 3 year post graduate experience and 1-2 peat surveys to more than 10 years-experience and surveys of multiple sites with complex geomorphology.

The peat landslide risk assessment has been carried out and reviewed by geo-environmental and geotechnical engineers with significant experience of undertaking peat landslide risk assessments on sites across Scotland. Details of their experience are provided in **Appendix C**.

1.7 Assumptions and Limitations

The following assumptions and limitations apply to the content of this peat landslide risk assessment:

- This assessment has been prepared and written in the context of the Proposed Development layout, guidance, and literature sources available at the time of writing. New information, improved practices and changes in guidance or significant alterations to the layout may necessitate a re-interpretation of the assessment in whole or in part after its original submission.
- It should be recognised that the peat surveys and interpolations based on the site surveys undertaken to date provide information characterising the variation of peat depths and that different conditions may be present between survey locations.
- No ground investigation or samples of peat have been obtained for geotechnical testing during field surveys. Where observations relating to the peat substrate are presented these relate solely to the conditions at the exposure and it should be recognised that different conditions may be present at the Development Site.

2. Peat Instability

Peat is an organic material formed by the accumulation of plant matter at various stages of decomposition, formed over many thousands of years. The characteristics of peat vary widely depending on, but not limited to, the nature of plant material that the peat is derived from, the degree of decomposition and the type of peat bog. A peat landslide represents the most extreme and rapid process by which peat bogs are degraded and that pose a risk to the Proposed Development and neighbouring environmental and human receptors.

In Scotland, the Scottish Government defines peat and deep peat as follows (Scottish Government, 2017):

- **Peaty soils**: soils with an organic horizon <0.5m thick;
- **Peat**: soils with an organic surface horizon greater than 0.5m in thickness and an organic matter content exceeding 60%; and
- **Deep peat**: a peat as defined above, with a depth greater than 1.0m.

There are two distinct types of peat, termed acrotelmic and catotelmic peat. The interface between the two layers is controlled by the position of the water-table. The upper layer of the peat (the acrotelm) is typically fibrous and comprises the living and partially decomposed peat forming plant matter. The thickness of the acrotelm is typically controlled by seasonal variations in the water-table that creates cycles of aerobic and anaerobic conditions near the surface. The catotelm is situated below the minimum average depth of the water-table (Evans and Warburton, 2010). This results in permanent anaerobic decomposition of the plant matter and the formation of less fibrous amorphous peat.

The term ‘peat landslide’ is a broad term referring to two major groups of peat slope mass movement (or failure), ‘bog burst’ and ‘peat slides’. Dykes and Warburton (2007) developed a classification scheme for mass movements of peat to define the terminology used to describe the types of peat slope failure. The following forms of peat mass movements have been defined by Dykes and Warburton (2007):

- Bog bursts and bog flows – failure by breakout of liquid catotelmic peat differentiated by the type of bog (raised bogs or blanket bogs respectively);
- Peat slides and bog slides – translational sliding of intact peat along a failure surface, differentiated by the failure plane being at the base or within the peat, respectively;
- Peaty-debris slides – translational failure of a slope covered with blanket peat where the failure occurs beneath the peat-substrate interface; and
- Peat flows – failure of any other peat bog type (e.g. fen peat).

Dykes and Warburton (2007) and Evans and Warburton (2010) indicate that bog bursts and flows are characteristic of deep peat with depths typically in the range of 1.5m to 6.5m situated on shallow slopes in the range of 2 to 8 degrees. Peat slides and bog slides have typically been reported on steeper slopes in the range of 5 to 15 degrees but in shallower thicknesses of peat in the range of 1m to 3m in thickness. However, as described in Evans and Warburton (2010) a limited number of bursts and slides have been reported outside of these ranges.

A peat landslide is the result of the combination of preparatory factors and trigger factors that either reduce the shear strength of the peat or increase the shear stress on the peat covered slope (Evans and Warburton, 2010). These factors directly or indirectly relate to changes in the

hydrology of the peat that can occur rapidly or over a long period of time, and that include natural and anthropogenic (man-made) factors such as (Scottish Government, 2017):

- Increases in the mass situated on the slope (e.g. peat accumulation, seasonal water-table variations and the mass of planted trees);
- Reduction in shear strength through changes in the peat or substrate (e.g. drying and desiccation cracking);
- Loss of surface vegetation (e.g. burning);
- Increased buoyancy through impeded drainage, pooling, pipe networks and rapid rewetting of desiccation cracks; and,
- Commercial afforestation of peat resulting in lowering of the water-table and deep desiccation cracking.

In addition, Evans and Warburton (2010) indicate there are a number of pre-conditions that predispose a slope to failure that relate to the hydrological processes within the peat. These include:

- Impedance of drainage below the peat caused by impermeable clays or iron pans in the substrate;
- A convex slope or break in slope that can concentrate flows;
- Proximity to drainage features such as flushes, peat pipes and streams; and,
- Connectivity between the surface drainage and an impervious peat-substrate interface.

Where the combination of preparatory and pre-failure conditions occur, a peat landslide may be triggered on susceptible slopes by a number of possible trigger factors. The trigger factors can be natural or anthropogenic and are typically related to those that rapidly cause changes in the pore-water pressure, reduce shear strength or rapidly increase the mass on the slope. These factors include:

- Intense rainfall or snow melt and rapid migration to the peat-substrate interface;
- Ground accelerations due to earthquakes, vibrations from vehicles and blasting;
- Incision of the peat slope by streams and rivers, peat turve cutting and excavations during construction causing a rapid reduction in support at the toe of the slope;
- Rapid loading of the peat by landslide debris sliding onto susceptible peat slopes;
- Loading of the peat by heavy plant, digging and tipping; and,
- Alteration of natural drainage routes resulting in focussed drainage on susceptible slopes.

3. Site Setting

3.1 Site Description

The Development Site is located approximately 11.5km south-southeast of New Cumnock in East Ayrshire and 13km southwest of Sanquhar in Dumfries and Galloway and straddles the boundary of the two counties. The Development Site is located at approximate central Ordnance Survey National Grid reference 266238, 600967 and covers an area totalling approximately 1,242 hectares (ha).

The Development Site location and layout are presented as **Figures 1.0** and **2.0** in **Appendix A**, respectively

The Development Site is dominated by very steeply undulating upland topography, predominantly used for sheep and cattle grazing. In the central area is the abandoned Lorg Farmhouse that is accessed from the south via the Holm of Dalquhairn Bridge along the western bank of the Water of Ken. The lowland area around the farmhouse is dominated by grazing pasture with a number of sheep pens and dry stone walled fields.

On the south facing slopes of Lorg Hill and the eastern slopes of Ewe Hill a number of bedrock outcrops and scree slopes are present including Green Cleugh, Rough Craig, Glede Craig, Long Craig and Craigfad that are identified on Ordnance Survey mapping.

The ground on the lower slopes of Ewe Hill, Lorg Hill, Altry Hill, Brown Hill and the northern slope of Coranbae Hill were noted to be generally firm and grassy. The summits of most hill tops were noted to be mossy with possible shallow peat and standing water present on the summit of Ewe Hill. On the flatter ground between the summits in the northwest and southeast of the Development Site peat was identified in exposures on stream banks and scarps.

A number of small burns are present across the Development Site including the Lorg Burn, Alwhat Burn, Altry Burn and Pulmulloch Burn, all of which are deeply incised for at least part of their course. The Water of Ken flows southward through the centre of the Development Site.

A series of photographs depicting the Development Site are presented as target notes in **Appendix B**.

3.2 Published Geology

Pedology

The National Soil Map of Scotland (1:250,000) (The James Hutton Institute, 2020) indicates that the northwest of the Development Site including the upper slopes of the hill tops are dominated by peaty podzols. The soils on the lower slopes and valley bottoms in the northwest are shown to comprise mineral gleys. In the centre of the Development Site the steep mid and lower slopes of Ewe Hill and Altry Hill are dominated by mineral podzols and in valley bottom along the Water of Ken the soils are shown to comprise peaty gleys and brown soils. In the southeast of the Development Site the soils are shown to comprise peaty gleys or peaty podzols over the highest hill tops and the far southeast is shown to be dominated by peat.

The 1:25,000 Soil Map of Scotland (The James Hutton Institute, 2020) provides partial coverage of the Development Site south of Craigstewart. The map indicates that peat is present in the far southeast of the Development Site from the lower slopes of Craigstewart east and southeast to Cairn Hill and Black Hill. In addition, the southeast of the Development Site is shown to contain peaty podzols and peaty gleys around the summits of Black Hill, Cairn Hill, Coranbae Hill and

Craigstewart as well as along the Altry Burn. Areas of mineral gleys and brown soils are identified along the mid-slope of Coranbae Hill, at the head of the Altry Burn, along the Small Burn and adjacent to the Water of Ken.

A summary of the soils at principal elements of the Proposed Development are summarised in **Table 3.1** below. The 1:250,000 Soil Map of Scotland is presented as **Figure 3.0** in **Appendix A**.

The NatureScot Carbon and Peatland 2016 map (SNH, 2016) is presented as **Figure 4.0** in **Appendix A**. The map indicates that the soils throughout the central and north-western areas of the Development Site are predominantly Class 3 (mostly carbon-rich with some deep peat) and Class 0 (mineral soils). Areas of Class 4 (areas unlikely to include carbon-rich soils) are identified on the tops of Alhang and Alwhat hills. The map also indicates that to the southeast of Altry Hill the soils are dominated by Class 1 soils (carbon-rich and deep peat with all cover priority peatland habitats) over the eastern slopes of Altry Hill to Fortypenny Hill, High Countam, Cairn Hill and Coranbae Hill. In addition, the Development Site also contains a number of small areas of Class 5 (no peatland habitat recorded) over the top of Cairn Hill and the mid-slope of Black Hill.

Table 3.1 Summary of the Soil Map of Scotland

Soil Type	Proposed Development
Blanket peat	T2, T4, T5, T6, T7, T8, T9
Peaty gleys	T1, T3, T10, SPEN substation, borrow pit B, meteorological mast B
Peaty podzols	T12, T13, T14, T15, meteorological mast A
Mineral gleys	T11, Borrow pit A, temporary construction compound A, western control building
Mineral podzols	Temporary construction compound B

Superficial Geology

British Geological Survey (BGS) mapping indicates that the northwest and southeast of the Development Site are dominated by peat. In the northwest peat is shown within the lower ground between Brown Hill, Alwhat and Alhang and between Alwhat and Millaneoch Hill. In the southeast, peat is shown in the lower ground and shallow slopes between High Countam, Fortypenny Hill, Altry Hill, Craigstewart, Cairn Hill and Black Hill.

In the centre of the Development Site along the lower valley sides of Lorg Burn and in the far north along the Water of Ken, superficial deposits are shown to comprise Hummocky Glacial Deposits comprising of sand and gravel and Alluvium of silt, sand and gravel. In addition, Glacial Till is shown to surround the Alluvium and Hummocky Glacial Deposits along the lower valley slopes of the Water of Ken, Altry Burn, Small Burn, Pulmulloch Burn and Alwhat Burn. On the hill tops, the superficial deposits are shown to be thin or absent.

The BGS digital geology map of superficial deposits is presented as **Figure 5.0** in **Appendix A**.

Solid Geology

BGS mapping indicates that the Development Site is bisected through the centre by an unnamed geological fault shown to strike northeast to southwest, and which passes approximately 300m northwest of Lorg farmhouse. The fault is shown to be a thrust fault with the hanging wall shown to the northwest of the fault, the offset distance is not given.

To the north of the geological fault the Development Site is predominantly underlain by Kirkcolm Formation comprising wacke that extends from Ewe Hill northwest to Millaneoch Hill. In the central area of the Development Site the bedrock is recorded as the Moffat Shale Group and Crawford Group comprising mudstone and chert, respectively. To the south of the fault the Development Site is underlain by the Portpatrick Formation comprising wacke.

BGS mapping also indicates that the Development Site is underlain by dykes of microdiorite, microgranite and micrograndiorite which generally trend northeast to southwest across Ewe Hill and Lorg Hill.

The BGS digital geology map of solid geology is presented as **Figure 6.0** in **Appendix A**.

3.3 Topography

The Ordnance Survey (OS) Terrain 5 Digital Terrain model (DTM) indicates that the Development Site is situated at an elevation of between approximately 255m above Ordnance Datum (AOD) and 642m AOD. The lowest elevations are identified along the Water of Ken and the maximum elevation is located at the summit of Alhang in the northwest of the Development Site.

The topography of the Development Site around Lorg farmhouse comprises a very steep sided 'U' shaped glacial valley which trends northeast to southwest through the centre of the Development Site. The steepest slopes are located along the western slopes of Altry Hill, the southern slopes of Lorg Hill and the eastern slopes of Ewe Hill. The topography along the Afton Water in the far northwest of the Development Site also comprises a 'U' shaped valley.

At the locations of the two turbine arrays in the southeast and northwest of the Development Site, the topography comprises a shallow sloped basin. In the southeast the turbine area is bound by the promontories of Altry Hill, Fortypenny Hill, High Countham Black Hill, Cairn Hill and Coranbae Hill located to the west, north, east and south of the turbine array, respectively. In the northwest the turbine array is bound by Alhang, Alwhat, Brown Hill, Ewe Hill and Mid Rig to the west, north, east and south, respectively.

The OS Terrain 5 DTM has been used to generate a slope angle analysis which indicates that the Development Site contains slope angles between 0º and 55º. The steepest slopes are recorded on the slopes of Ewe Hill, Lorg Hill, Altry Hill and Mid Height surrounding Temporary Compound B, at the location of Borrow Pit B and to the west of T12 and T15.

The slope angle analysis based on the OS Terrain 5 DTM is presented as **Figure 7.0** in **Appendix A**.

3.4 Hydrology

Ordnance Survey mapping reveals that the Development Site forms the upper catchment of the Water of Ken which is a tributary to Loch Ken and the River Dee located approximately 25km south of the Development Site. In addition, the far northwest of the Development Site beyond the west of the Alwhat / Alhang col forms the upper reaches of Afton Water which drains into Afton Reservoir approximately 0.5km north of the Development Site. Afton Water drains into the River Nith approximately 11km to the north-northwest of the Development Site.

OS mapping identifies a number of named tributaries to the Water of Ken which flows generally south-westward through the central area of the Development Site. These tributaries include the Alwhat Burn, Green Cleugh Burn, Spout Burn and Lorg Burn which drain the northwest of the Development Site. The southeast of the Development Site is drained to the Water of Ken by the Altry Burn, Small Burn and Pulmulloch Burn. In addition, to these named burns the Development Site is also drained by a number of unnamed surface watercourses and mapped drainage ditches such as around the location of Fans of Altry, Small Cleugh and Rough Cleugh.

In the far northwest of the Development Site beyond the Alwhat / Alhang col, the Alhang Burn is shown to drain the ground to the west and northwest of Alwhat and Alhang hills and joins the Afton Water which flows northward to the Afton Reservoir. The northside of Alwhat hill is shown to drain to Afton Water and Afton Reservoir northward via the Alwhat Burn. In the far west of the Development Site the low ground between Alhang and Millaneoch Hill as well as the south-eastern slopes of Alhang hill are drained southward by Holm Burn to the Water of Ken. Gills Burn is shown to drain the southern slopes of Alhang hill and Mid Rig in the western part of the Development Site.

The SEPA Water Classification Hub website indicates that the Water of Ken is classified as having an overall status of Poor in 2020. Afton Water (including the Afton Reservoir) is classified as having an overall status of Good Ecological Potential in 2020.

The locations of the surface water features are presented in **Figure 2.0** in **Appendix A**.

3.5 Hydrogeology

Scotland's Environment website indicates that the Proposed Development is underlain by a Class 2C low productive aquifer, where limited groundwater flow occurs in the near-surface weathered zone and within secondary fractures and other discontinuities. As a result, the bedrock can locally yield only small amounts of groundwater with short and localised flow paths.

The Scotland's Environment website also indicates that to the southeast of the Alwhat / Alhang col the Development Site is underlain by the Galloway groundwater body that has an overall classification of Good. To the northwest of the col the groundwater body is recorded as the Upper Nithsdale groundwater body that has an overall classification of Poor.

3.6 Water Supply Abstractions

Dumfries and Galloway Council has provided details of eleven private water supplies (PWSs) located within 4km of the Development Site. In addition, East Ayrshire Council provided a list of PWSs within its administrative boundary. However, of those with coordinates none were identified within 4km of the Development Site. Although not identified in the records provided by the Local Authorities the presence of a PWS at Lorg Farmhouse has been confirmed with the landowner[2]. **Table 3.2** below summarises the locations of the PWSs identified within 4km of the Development Site.

The nearest PWSs to the Development Site are shown on **Figure 15.0** in **Appendix A**.

Table 3.2 Private Water Supply locations

Supply Name	Easting	Northing	Supply Source	Distance from Development Site Boundary
Lorg Farmhouse	266755	601110	Spring	On site
Holm Of Dalquhairn	265529	599007	Spring	0.9km south
Auchrae	265150	596516	Spring	3.0km south
Blairoch Cairnhead	270107	597237	Surface runoff	2.1km south east
Corlae Farmhouse	265830	597704	Borehole	1.75km south

[2] It has been confirmed that Lorg Farmhouse would not be occupied during the construction, operation or decommissioning of the Proposed Development.

Supply Name	Easting	Northing	Supply Source	Distance from Development Site Boundary
Corlae Byre	265868	597730	Borehole	1.75km south
Corlae Byre	265866	597712	Borehole	1.75km south
Craigengillan Cottage	265125	597134	Spring	2.5km south
Craigiethorn Croft	265812	598116	Borehole	1.5km south
Dalgonar	270015	603101	Stream	2.25km north east
Polskeoch Scar Valley	268669	602310	Spring	0.75km north east
Upper Holm	265551	599313	Spring	0.75km south

Notes
Coordinates for PWS's that have not had their source location recorded according to East Ayrshire Council record are assumed to be at or near the property they supply.

Although Local Authority data indicates the presence of PWSs within the vicinity of the Development Site, there is only one at Lorg farmhouse with the potential to be directly affected by a peat landslide originating from the Proposed Development. This is due to the local topography, peat depths and/or their location upstream of the Development Site.

3.7 Designated Sites

Scotland's Environment website indicates that there are no designated ecologically or geologically important sites within the Development Site boundary or within 3km of the boundary.

3.8 Historical Mapping

A review of the available online historical mapping provided by the National Library of Scotland Map Images website indicates that there are no recorded place or feature names that are likely to relate to a historical peat slide. In addition, there have been no obvious major changes to the course of any surface watercourses draining the Development Site which would potentially indicate that a peat slide had occurred. The only feature of relevance is the Altry Loch which is shown as an open surface water feature on historical mapping but a marshy wetland in current OS mapping.

3.9 Imagery and Photography

Historical Imagery

An online search of the National Collection of Aerial Photography (NCAP) has been undertaken to identify any indications of historical peat landslides. The earliest available aerial imagery is dated from 1988. However, the available photography is in black and white and at a small scale therefore any features would be hard to identify if revegetated unless they were of a significant size.

The historical aerial imagery available within Google Earth Pro has also been reviewed for indications of any historical peat landslides. The available imagery ranges in date from 1985 to the present day but only the imagery from 2006, 2008, 2011, 2018 and 2019 are at a resolution small enough to identify features. A review of the available imagery identifies the following:

- Peaty-debris slides along the Altry Burn, on the north slope of Coranbae Hill and Ewe Hill and on the southwest slopes of Lorg Hill;
- Gripping (as identified in contemporary imagery below);
- Gullies, flushes and haggs (as identified in contemporary imagery below);

The features identified are included in the geomorphological map presented as **Figure 11.0** and **11.1** in **Appendix A.**

Contemporary Imagery

Ordnance Survey MasterMap Imagery and Google Earth Pro aerial imagery dated 2022 and June 2019, respectively, have been reviewed for the Development Site. The OS MasterMap Imagery is presented as **Figure 8.0** in **Appendix A**. An inspection of the aerial imagery reveals the following features:

- flushes and possible flushes;
- peat gripping;
- hagging;
- gullies;
- possible pipe collapses;
- pools;
- peat cutting (turbary);
- peaty-debris slides; and,
- scree slopes.

The geomorphological features identified in the aerial imagery and encountered during the peat surveys are presented in **Figure 11.0** and **11.1** in **Appendix A.**

Public Photography

An online search of the Geograph Project Limited website (https://www.geograph.org.uk/) has been performed to identify images of the Development Site. The Development Site contains numerous images providing information on the topography and geomorphology. A summary of the pertinent photography is provided in Error! Reference source not found..**3** below and their locations are shown on **Figure 11.0** and **11.1** in **Appendix A.**

Table 3.3 Public photography records

Map ID	NGR	Direction	Description	Image Reference Number
P1	NX 6891 9938	North	Looking north along the Development Site boundary north from Black Hill towards hagging and flushing between Black Hill and High Countam.	6742923
P2	NS 678 013	East-northeast	Looking upstream along the valley of the Water of Ken at the lower slopes of Altry Hill.	1011713

P3	NS 670 009	Southwest	Looking down the valley through the centre of the Development Site along the Water of Ken showing the topography, river terraces, hummocks and the dominance of mineral soils	436621
P4	NS 6677 0057	East-southeast	Looking down from Ewe Hill to the valley of the Water of Ken showing the hummocky terrain, topography of Altry Hill and the dominance of mineral soils.	4503302
P5	NS 664 010	Southwest	An oblique aerial image looking down the valley along the Water of Ken showing the topography, outcrops on Ewe Hill, dominance of mineral soils in the valley bottom and peat soils across the flatter hill tops.	3545376
P6	NS 65048 02267	East	Looking along the boundary between EAC and DGC showing peat forming vegetation in the flatter ground between Alwhat and Meikledodd Hill.	6775031
P7	NS 6533 0234	Northeast	Looking towards Meikledodd Hill from Brown Hill showing signs of peat erosion features or scarps on the upper slopes of Meikledodd Hill.	6775035
P8	NS 6440 0170	N/A	A pool located at the Source of the Afton Water	4828555
P9	NS 6437 0156	N/A	A pool located near the Source of the Afton Water	4828554
P10	NS 6439 0153	Northeast	Looking across the col from Alhang to Alwhat showing the pools at the Source of the Afton Water.	4828551

Notes
The image reference number refers to the URL image reference. To view the image enter the image reference number at the end of the following website URL: https://www.geograph.org.uk/photo/

3.10 Landslide Inventory

A search of the BGS National Landslides Database on the BGS GeoIndex indicates that there have been no recorded landslides within or in the vicinity of the Development Site (i.e. within 2km).

The peat landslide risk assessments undertaken for the adjacent Windy Standard Wind Farm and Afton Wind Farm to the west of the site reveals that there were no peatslides identified by site surveys.

4. Field Surveys

4.1 Methodology

A programme of peat depth surveys have been undertaken at the Development Site over a series of surveys completed by Amec Foster Wheeler and Wood (now WSP), generally in accordance with the Scottish Government guidance document on '*Guidance on Developments on Peatlands: Site Survey (2017)*' and its previous versions.

In August and September 2013, a Phase 1 peat depth survey was undertaken by Amec Foster Wheeler on a 100m by 100m grid across the parts of the Development Site shown to contain peat and peaty soils. The remainder of the Development Site, generally through the Water of Ken valley and steeper slopes was undertaken at 250m by 250m survey intervals. The survey was completed during a period of variable weather with intermittent showers.

The Phase 1 survey was followed by a Phase 2 survey undertaken on the Consented Development in October 2015 by Amec Foster Wheeler. The weather during the Phase 2 survey comprised very heavy rainfall on the 5th October preceded by light showers on the 6th October. The remainder of the survey was characterised by dry and windy weather. At the same time, the Phase 1 survey was extended over the area between Alhang, Alwhat and Mid Rig due to an extension of the Development Site boundary.

Following submission of the Environmental Impact Assessment (EIA), alterations to the design of the wind farm layout resulted in the need for additional probing to support Further Environmental Information (FEI). Further probing was only required in the southeast of the Development Site due to the removal of the turbines in the northwest and relocation of the turbines and associated infrastructure in the southeast of the Development Site. The additional peat survey was undertaken by Amec Foster Wheeler in April 2017 during a period of dry weather.

The Phase 2 survey undertaken on the Consented Development comprised:

- 1 no. probe placed at 50m intervals along new access tracks plus 1 no. probe placed 10m perpendicular to either side of the track where the interpolated Phase 1 peat depth data was >1m in depth;
- 1 no. probe at turbine locations;
- 4 no. probes placed on the edges of the micro-siting allowance (50m) where the peat depth was interpreted to be <1m deep;
- A grid of points at 20m intervals across the micro-siting allowance where the turbine is situated within or close to areas with an interpreted peat depth >1m or where there was no Phase 1 peat depth information;
- Additional points were placed on the crane pads and anemometer masts where required to provide coverage;
- A grid of 10m to 20m intervals at the substation and temporary construction compounds; and,
- A grid of 50m intervals at the borrow pit search area.

A reactive approach to the survey was adopted to collect the most information where peat depths were >1m.

The Phase 1 survey was undertaken by Russian core sampling. This was conducted by initially using a 1m long peat probe to establish that the peat depth was greater than 0.5m in thickness followed by Russian sampling to physically measure the depth of peat and to recover samples for inspection and von Post classification. The Phase 2 survey was conducted by peat probing using an extendable fibre glass peat utility probe. The results at each survey location were recorded using a hand-held GPS device with data entered into GIS.

In March 2021 Wood was commissioned by RWE to undertake supplementary peat surveys on the Development Site to support the layout design and EIA. In June 2021 Wood a undertook supplementary Phase 1 peat depth survey across the northwest of the Development Site through the valley of Afton Water between the north side of Alhang, Millaneoch Hill, Wedder Hill and the forestry surrounding Afton Reservoir. In addition, a supplementary Phase 1 survey was undertaken over Sour Snout, Whigs' Hole and the upper slopes of Black Hill and Cairn Hill. The survey was undertaken at 100m intervals across the survey area.

The supplementary Phase 1 survey was followed in June and July 2022 with a Phase 2 survey on the Proposed Development that comprised:

- 1 no. probe at 50m intervals along all access tracks;
- 1 no. probe 10m perpendicular to each side of the track only where peat depths are >0.5m;
- a 10m grid of points covering the turbine micro-siting buffer where peat depths are >0.5m;
- a 20m grid of points covering the turbine micro-siting buffer where peat depths are <0.5m; and,
- a 15m grid of points at the borrow pit borrow pit search areas and an alternative construction compound location.

The above scope was altered as necessary to increase or decrease the density of peat depth measurements based on the depths encountered at each location as the Phase 2 survey progressed. Where peat depths were found to be <0.5m the intervals were increased.

The peat depth surveys were undertaken using extendable peat utility probes driven into the ground until refusal during periods of dry weather. The results at each survey location were recorded using a hand-held GPS device with data entered into GIS.

4.2 Survey Constraints

Although the Phase 1 peat depth surveys were scoped in accordance with the methodology detailed above, due to the presence of constraints relating to the topography the full scope was not possible along the following slopes:

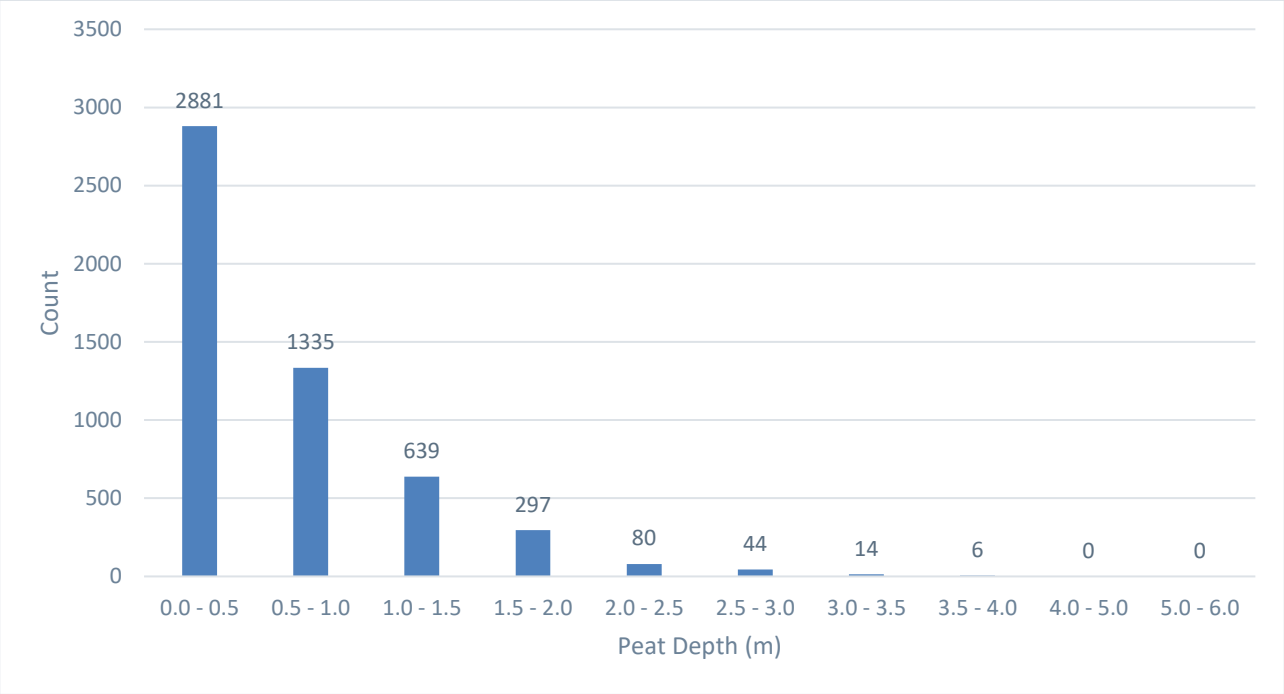
- North-western slopes of Altry Hill;
- Eastern slopes of Ewe Hill;
- Southern slopes of Lorg Hill; and the,
- Southern slope of Alhang.

Where possible the inaccessible slopes were visually assessed for peat and in all cases it was noted that the steepness of the slope and dominant vegetation were not conducive to the formation of peat (as defined in Section 2).

4.3 Peat Depths

In total the peat depth surveys undertaken across the Development Site have comprised 4,158 peat depth measurements which has revealed peat depths ranging between 0.00m and 3.80m. A total of 2,415 (~58%) survey locations have recorded peat depths ≥0.5m and the calculated mean of all peat depths ≥0.5m is 1.08m. **Figure 4.1** below summarises the distribution of peat depth measurements recorded within the Development Site and peat depth data is included in **Appendix D**.

Figure 4.1 Summary of all peat depth data



A composite plan of all peat depth data is presented in **Figures 9.0** to **9.17** in **Appendix A.**

The peat depth data obtained during the surveys has been used to generate an interpolated peat depth map for the Proposed Development. This has been achieved by using ESRI ArcGIS and the Natural Neighbour interpolation method. This method was chosen given the relative simplicity of the weighting compared to other interpolation methods. It also avoids exaggeration of minimal and maximal values and results in a modelled surface that passes through the sample point value. The method also does not produce a pronounced “bulls-eye” effect on the modelled surface. However, unlike other methods it is not possible to barrier the interpolation. It also models depths over the furthest geographic extent and does not extrapolate out from the maximum extents of the sample points to the maximum rectangular extent. This method also calculates cell values across the longest extents of the sample points resulting in interpolations over large distances where there are gaps in the sampling points or they are irregularly distributed.

Figure 10.0 in **Appendix A** shows the interpolated peat depths across the Proposed Development

The interpolated peat depth map indicates that the Development Site contains three principal bogs where deep peats are >0.5m located:

- in the southeast in the Fans of Altry area between High Countam, Black Hill, Cairn Hill, Altry Hill and Craigstewart;
- in the northwest in the lower lying slopes Ewe Hill, Brown Hill, Alwhat and Alhang; and,
- through the Afton Water valley in the far northwest of the Development Site.

The deepest areas of peat have been identified at the head of the Altry Burn and Pulmulloch Burn and to the northeast of the Fans of Altry. In addition, areas of deep peat >1.0m have been identified across the flatter lower slopes in the northwest of the Development Site at the heads of Alwhat Burn and Spout Burn. In the Afton Water valley, areas of deep peat have been identified along the lower slopes adjacent to Afton Water as well as in the lowest part of the col between Alhang and Millaneoch Hill.

4.4 Peat Characteristics

A total of 217 Russian core samples were inspected during the Phase 1 survey undertaken by Amec Foster Wheeler. The coring revealed that the peat has a typical one or two layer profile with relatively few localised positions in the deepest peat exhibiting a triple layer profile and only one location with a four layer profile.

In general, where there was a single layer profile, moisture content values were found to be low (i.e. von Post class B2) and humification values were typically less than H6. Where the peat was found to have two or more layers, the moisture content values were found to be generally B3 with humification values increasing with depths from H2 to H9 in areas with the deepest peat.

Photographs showing examples of the exposures are presented as TN20, 30, 59 and 66 in **Appendix B** and their locations are presented in **Figure 11.0** in **Appendix A**.

4.5 Peat Substrate

The peat surveys revealed that there were few exposures of the underlying peat substrate across the Development Site. In general, where encountered, the exposures inspected during site works were found along streams and gullies, backscars of peaty-debris slides and translational landslides.

Where exposed, the peat substrate was found to comprise either Glacial Till, weathered bedrock or intact bedrock. Where Glacial Till was encountered this was found to comprise a very sandy gravelly silty clay with cobbles and boulders (see Target Note 21 and 59). Weathered bedrock was noted to comprise sandy angular gravels and cobbles (Target Note 30 and 66). Where bedrock was identified this was noted to be typically undulating and irregular.

4.6 Laboratory & In-situ Testing

Due to the inherent material variability, the difficulty in obtaining representative samples of peat and thus obtaining sensible and reproducible geotechnical parameters, samples were not recovered during this investigation. The collection of samples is not considered critical for the purpose of this assessment. While in-situ hand shear vane testing is commonly used to establish the undrained strength of peat, the interpretation of hand vane results is complicated by the presence of fibres and the ease of deformation of the peat during the test (Boylan *et al*, 2008).

4.7 Geomorphology

A visual geomorphological walkover of the Development Site was carried out at, and between, each probe location while conducting peat survey works in order to identify geomorphic features such as:

- Relic peatslides;
- Tension features (e.g. tension cracks);
- Compression features (e.g. compression ridges & peat thrusts);

- Sub-profile drainage features (e.g. peat pipes and pipe collapses);
- Peat creep features (e.g. closed peat grips);
- Erosion features (e.g. scarps, peat haggs and gullies); and,
- Surface drainage features (e.g. flushes).

During the peat surveys geomorphological features were identified throughout the Development Site. A geomorphological map of the Development Site is presented as **Figure 11.0** and **11.1** in **Appendix A** and target note photographs of select features are presented in **Appendix B.**

The most numerous features identified were man-made peat grips and drainage ditches (TN-57) which were found across large areas of the Development Site. These features typically ranged in width and depth from <0.3m to >1.0m and in the most part were found to be moss filled with the main grips found to be open with freely flowing water.

The peat surveys also identified a number of incipient and relic failures including a limited number of peaty-debris slides, slope creep terraces, translational failures, tension cracks and a possible deep seated landslide. In general, slope failures were found along the steepest slopes of Ewe Hill, Meikledodd Hill, Lorg Hill, Altry Hill, Alhang and Alwhat. Translational failures and peaty-debris slides of the superficial deposits are shown in TN's 14, 35, 36 and 50. Some of the slides were caused by over steepening on the outside of stream meanders as shown in TN 21 and 22.

In the southeast of the Development Site potential slope creep was identified at one location as shown in TN 47. This feature is characterised by a series of flat lying terraces extending down the mid slope on the northern side of Coranbae Hill. A possible tension crack was identified near the location of T3 (TN69)

In addition to slope failures, the surveys identified several natural surface and sub-surface drainage and erosion related features including peat pipes, peat pipe collapses, gullies, flushes, springs, haggs and active scarps. In general, these features were encountered on the lower slopes with the deepest peat typically >1.0m in depth such as between the summits of Ewe Hill, west of T11 and down the slope to the north of T2 and T8. Peat pipe collapse features are characterised by TN's 37, 41, 44, 51, and 52 and erosion features are characterised by TN 17, 31, 53 with the worst erosion characterised by TN 54, 55 and 56. Flush features are characterised by TN 26, 32, 34, 38, 60, 62, 65 and 68, the largest of which are found at the source area for the Alwhat Burn, in the Fans of Altry Area and in the col between High Countam and Black Hill.

5. Peat Landslide Hazard Assessment

5.1 Background

The following assessment of peat stability has been undertaken in general accordance with the Scottish Government best practice guide. This method considers the likelihood (i.e. the susceptibility) associated with a particular area of peat multiplied by the consequences of a failure to derive the potential risk. This is expressed as:

Risk = Likelihood x Consequence

The assessment of the peat landslide likelihood has been undertaken for peat slide failure types as defined by the Dykes and Warburton (2006) formal classification scheme[3]. An assessment of the susceptibility of the Development Site to bog flow failures has not been undertaken due to the relative low number of slope and peat conditions across parts of the Development Site that are characteristic of bog flow failure (e.g. very deep peat and shallow slopes). The assessment of likelihood has been undertaken through the identification, assessment and mapping of contributory hazard factors for peat slide failure types supported by a semi-quantitative assessment of peat slide susceptibility using the infinite slope model.

The assessment of peat slide hazards involves the allocation of hazard rating values for the various contributory and pre-condition factors that influence the probability of a peat slide based on the findings of literature research. However, current guidance does not define the hazards that should be assessed nor the ratings that should be applied. In addition, there is no published guide specifically relating to this issue. As such, it is left to the judgement of the assessor to develop their own approach to the assessment of the hazards. A review of literature sources (see Section 5.2) has indicated that the likelihood of a peat slide occurring is a combination of following contributing and pre-condition hazard factors:

- Slope angle;
- Peat depth;
- Slope Curvature;
- Natural Drainage;
- Artificial Drainage;
- Pre-failure Indicators;
- Geology.

The hazards posed by each contributory factor have been individually scored based on their specific relevance to peat instability using both site observations and desk top studies. The hazard assessment relates the importance of the hazard to a scale of 1 to 5 as summarised in **Table 5.1** below.

[3] Bog slides and peat slides are assessed under a single class (peat slide) given that the only difference between the definition of these classes are the position of the failure plane.

Table 5.1 Hazard Scoring

Scale	Description
5	Extremely Serious
4	Serious
3	Substantial
2	Significant
1	Insignificant

A hazard ranking has then been calculated by the combination of each contributing factor thus allowing for the determination of the likelihood of instability as described in Section 6. The scores for each hazard factor are presented in the following sections and summarised in **Figure 12.0** in **Appendix A**.

5.2 Hazard Assessment

The following sections provide discussion on the contributory hazard factors and the method for assessing and scoring the hazards.

Slope Angle

The OS Terrain 5m DTM has been used to assess the slope angles across the Development Site.

Hazard scores have been based on information contained within published literature relating to historical failures in the UK and Ireland over a number of slope angles. Evans and Warburton (2010) summarise the frequency of peat slides and bog flows across various slope angle ranges. Their summary indicates that peat slides are more frequent on slopes between 5 and 20° (predominantly between 5 and ~15°). Therefore, these angles have each been assigned higher scores. The further away the angle is from these ranges, the lower the risk score as a result of the lower potential energy stored on lower slopes, the decreasing frequency of failures outside these ranges and the lower thicknesses of peat typically found on steeper slopes >20°.

Table 5.2 Slope Angle Hazard Scoring

Slope Range (degrees)	Peat Slide Score	Rationale
>20	1	Peat slides are considered unlikely due to the slope angle restricting the potential for significant depths of peat to form.
15-20	4	There are many peat slides recorded in this range of slope angles.
8-15	5	The majority of peat slides described in the literature occur within this range of slope angles.
5-8	3	Although some peat slides have been recorded they are less frequent than steeper slopes.
<5	1	Few peat slides are recorded in the literature below 5 degrees.

Peat Depth

The thickness of peat is a key contributory factor in both the likelihood and mechanism of peat instability. Evans and Warburton (2010) have summarised the frequency of peat slides and bog flows over a range of peat depths. This summary indicates that peat slides are most frequent where the peat is between 1.0m and 2.0m. However, instability has been reported outside of these ranges, up to a depth of 4.5m for peat slides though the frequency of instability decreases significantly at depths >2.5m. Their reasoning for this is that increased peat depth is commonly associated with greater variance in the humification of the peat profile.

Where the peat depth is less than 0.5m, instability is not typically associated with the peat but rather the underlying mineral substrate. However, whilst reduced, a risk may still remain and as such this is reflected in the scoring system. It should also be noted that no peat instability will occur where no peat or organic soil is recorded and landslides in these areas will be associated with deeper seated failures of the superficial deposits (not assessed here).

Table 5.3 Peat Depth Hazard Scoring

Peat Depth Range (m)	Peat Slide Score	Rationale
>3.5	2	The number of peat slides recorded in peat depths >3.5m are limited in number.
2.0 – 3.5	3	While at a lower frequency comparatively to depths between 1.0m and 2.0m some peat slides have been reported up to 3.5m.
1.0 – 2.0	5	Evans and Warburton (2010) indicate that most reported peat slides (~60 no.) occurred in this range of peat depths.
0.5 – 1.0	3	A limited number of peat slides have been reported at these depths
<0.5	1	Failures are classified a peaty debris slide with failure typically in the substrate material. The number of reported slides with peat depths <0.5m are comparatively few in number.

Slope Curvature

The slope curvature has been suggested as important factor in controlling the susceptibility of the slope to failure by a number of investigations of peat landslides by Dykes & Warburton (2006), Boylan and Long (2011) and Dykes (2008). In addition, investigation of recent slides in Ireland, including the Meenbog slide by Dykes (2022) revealed that the investigated slides had commonly occurring features noted in previous accounts of failures. Dykes (2008 & 2022) summarises the frequency of peat landslides on various slope forms which reveals that peat landslides are much more common on convex slopes.

Boylan *et al* (2008) suggests that the mechanism of failure on convex slopes is potentially the presence of notably thicker and weaker peat upslope of the break with the peat below being well-drained. In the event of failure it retrogressively progresses upslope with little resistance provided by the lower slopes. On concave slopes Boylan *et al* conclude that the characteristics of a failure are different as they tend to slide slowly as it is checked by the flatter lower slope and upwelling of peat into ridges. The failure finally tears, thrusting the upper peat on top of the intact peat surface below the concave break and the failure progresses. However, of the failures investigated on concaved slopes, evidence of previous slides downslope of the failure were identified and these may have been a more significant factor in causing the slide than the slope form.

The slope curvature hazard scores have been calculated from the OS Terrain 5 DTM and determined in GIS using profile slope curvature analysis to quantify the slope curvature across the Development Site. The DTM was aggregated into 25m cells equating to approximately one sixteenth of the mean slope length across the Development Site. The curvature break values for the hazard assessment have been established using standard deviations (std dev) as detailed in **Table 5.4** below. This provides a curvature surface from which to attribute hazard rating scores that correlates well with the findings of the site reconnaissance and slope breaks mapped in Figure **11.0** and **11.1** in **Appendix A**.

Table 5.4 Slope Curvature Hazard Scoring

Slope Form (break values)	Peat Slide Score	Rationale
Concave (>+0.5 std dev)	2	Dykes (2022) indicates that peat slides have been identified on concaved slopes but make up only a quarter of the recorded failures and are potentially checked by downslope peat.
Rectilinear (>=-0.5 to <=+0.5 std dev)	3	Dykes (2022) indicates that peat slide failures on these slopes make up half of recorded failures.
Convex (<-0.5 std dev)	5	Dykes (2022) indicates that peat slides are regularly recorded on convex slopes.

Natural Drainage

Peat hydrology and hydrogeology is complex and differing hydrogeological conditions within the acrotelm and catotelm are demonstrated in a number of studies (Warburton *et al*, 2004). In general, surface water flows are concentrated through the upper more fibrous acrotelm with flow depths up to 0.2m bgl reported. Catotelmic hydrogeology appears to be dominated by vertical seepage and concentration of flows along peat pipes.

The presence of peat pipes concentrates sub-surface flows through conduits within, or at the base of the peat profile. Peat pipes are a ubiquitous feature of upland peat and have been found to be a contributory factor in a number of peat slides reported in the literature. These features supply rainwater to the slide site or substrate (Warburton *et al*, 2003 and Nichol, 2009) and are therefore considered one of the greatest hazards.

A review of the slope conditions at the identified pipe locations indicates that they are more prevalent in the southeast and central northwest on the upper and lower slopes. In addition, the pipes are generally more prevalent in the vicinity of artificial drainage channels and ditches and where peat depths are approximately 1.0m in thickness. These conditions generally accord with the major controls on pipe frequency postulated by Holden (2005). As peat pipes are difficult to identify in the field especially where there is no observable surface expression of the pipe (e.g. depressions, sinks and rises) the Development Site has been divided into slope facets containing similar peat depths, drainage and slope positions and the appropriate score from **Table 5.5** has been applied.

The presence of surface drainage features such as flushes and bog pools may give rise to increased vertical migration of surface water through the catotelm leading to increased basal moistening or liquefaction of basal peat (Evans & Warburton, 2010) resulting in decreased shear strength. In addition, increasing moisture content and waterlogging of the peat will also increase the loading on the slope and basal/substrate pore water pressures. Mills (2003) attributes the

presence of drainage features such as flushes discharging to the top of the slide as being a contributory factor in several reported peat slides.

The scores summarised in **Table 5.5** reflect the importance of the drainage feature in supplying rainfall directly to the failure site.

Table 5.5 Natural Drainage Hazard Scoring

Natural Drainage Hazard	Peat Slide Score	Rationale
Peat Pipes	5	A significant drainage pathway, often associated with peat instability. Surface water and rainfall can be rapidly transmitted to the peat / substrate interface in a storm event.
Flushes	4	Flushes have been found to be a contributory factor in peat slides and bog flows under specific circumstances (i.e. blocking drainage lines or draining onto a slope). Flushes allow the storage and transmission of rainfall and increase the mass of the peat.
Bog Pool Complex	3	Bog pools are likely to transmit and store large quantities of water at or close to the peat substrate interface resulting in basal moistening and increased buoyancy.
Hummock and hollow complexes	2	Shallow pooling of water is unlikely to result in the rapid transmission of rainwater from the surface to the peat substrate interface but will result in increased loading.
Gullies and no obvious surface features	1	Surface pathways for slope drainage are well established, subsurface drainage is unlikely; peat landslides not usually recorded in gullied areas.

Artificial Drainage

It has been demonstrated that the presence of drainage ditches and peat grips across a slope may have contributed to peat landslides in studies by authors such as Carling (1986) and Dykes and Kirk (2006). The mechanisms through which drainage ditches have been reported to have contributed to failure include the under cutting of support from upslope peat and interception and rapid transfer of rainwater to failure sites. Warburton *et al* (2004) indicate that desiccation of the peat in grips may also allow the rapid transfer of rainwater down to the peat / mineral substrate interface where lubrication and increased pore water pressures at the interface can trigger peat slides. In addition, literature evidence suggests that artificial peat drainage is an important influence on the prevalence of peat pipes (discussed above); there are more peat pipes where there is artificial land drainage (Holden, 2005). Peat gripping also interrupts the peat surface removing the confining acrotelm and fragmenting the peat mass.

The scores summarised in **Table 5.6** reflect the three possible scenarios that may direct rainfall to a potential failure site..

Table 5.6 Artificial Drainage Hazard Scoring

Artificial Drainage Hazard	Peat Slide Score	Rationale
Peat grips and ditches aligned across slope	5	Peat grips and ditches aligned across the slope have been demonstrated to be a contributory factor in peat slope failures.
Peat grips and ditches aligned down slope	3	Peat grips and ditches aligned down the slope are unlikely to intersect peat pipes and will transfer rainfall rapidly downslope.
No Artificial Drainage	1	No influence on peat slope stability.

Pre-failure Indicators

Relic failures and pre-failure indicators on a slope provide a strong indication that a slope is pre-disposed to a failure. The hazard rankings for pre-failure indicators are summarised in **Table 5.7**.

Table 5.7 Pre-failure Indicators Hazard Scoring

Feature	Peat Slide Score	Rationale
Relic failures	5	Relic peat slides and peaty-debris slides on a slope may indicate that slopes with similar conditions may be pre-disposed to failure.
Incipient failure features (tension and compression features)	4	Tension and compression features indicate that a failure is potentially imminent or ongoing and that the slope is strongly pre-disposed to failure.
Peat creep and peaty debris slides	3	Soil creep generally occurring in shallower peat and/or lower slope angles may indicate a slope's pre-disposition of rapid failure.
No failure indicators	1	No influence on slope stability.

Geology

In a number of peat slides described in the literature, the substrate characteristics of the slopes have been considered a possible contributory factor. The presence of particular substrate features such as an iron pan within the soil profile below the peat was reported at three peat slides by Acreman (1991, p. 175). In other studies, Glacial Till deposits were reported at peat slides described by Crisp *et al* (1964), Tomlinson and Gardiner (1982) and Carling (1986). A basalt derived regolith and 'rubble' was noted in the study by Wilson and Hegarty (1993). Nichol (2009) noted patches of smooth rockhead at the head of a peat slide within the Scottish Highlands.

The hazard ranking has been determined by site observations and BGS mapping. Although there were some exposures of the substrate at ground level, there is insufficient data to accurately map the distribution and composition of the Glacial Till underlying the peat across the entire site. However, based on the available observations the deposits appear to be predominantly clayey

underlying deep peat and granular underlying shallow peat (<1.0m). As such, the site has been scored on the basis of these observations.

Table 5.8 Geology Hazard Scoring

Geology	Peat Slide Score	Rationale
Glacial Till and Alluvium	5	Deposits comprising mainly clay are likely to provide a discrete interface where reduced drainage and the formation of iron pans may increase the likelihood of a failure.
Impermeable bedrock	3	Impermeable bedrock, particularly those with smooth planar surfaces will provide reduced resistance to a slide.
Permeable bedrock and granular deposits.	1	Significant peat depths are unlikely to form on permeable bedrocks and few slides are associated with granular substrate materials.

5.3 Peat Landslide Stability Assessment

A semi-quantitative peat slope stability assessment has been undertaken in accordance with the methodology detailed within Scottish Government best practice guide (2017). The 'Infinite Slope' method of analysis, after Skempton and DeLory (1957), is the most well established and commonly applied method for the preliminary assessment of peat slope stability.

The factor of safety of a given slope assuming a steady seepage is calculated by comparing the sum of the resisting forces with those of the destabilising/acting forces, given by the following equation:

$$\mathbf{F} = \frac{Shear\ Resistance}{Shear\ Forces} = \frac{c' + (\gamma - m.\gamma w).z.cos^2\beta.tan\phi'}{\gamma.z.sin\beta.cos\beta}$$

Where:

F = Factor of Safety
c' = Effective cohesion
γ = Bulk unit weight of saturated peat
γ_w = Unit weight of water
m = Height of water table as a fraction of the peat depth
z = Peat depth in the direction of normal stress
β = Angle of the slope to the horizontal
ϕ' = Effective angle of internal friction

As a significant number of samples would be required to sufficiently characterise the geotechnical parameters of the peat, testing was not undertaken for the preliminary assessment. As such, the geotechnical parameters for this assessment have been obtained from a review of literature sources. A summary of literature values used to inform the stability analysis are presented in **Table 5.9** below.

Table 5.9 Geotechnical parameters of peat derived from literature review

Reference	Effective cohesion c' (kPa)	Effective angle of friction φ' (°)	Unit weight	Reference
Hanrahan et al (1967)	5.5 – 6.1	36.6 – 43.5	-	Remoulded H4 Sphagnum peat
Hollingshead and Raymond (1972)	4.0	34	-	-
Landva and La Rochelle (1983)	2.4 – 4.7	27.1 - 35.4	-	Sphagnum peat
(H3, mainly fibrous)				
Carling (1986)	6.52	0	10	-
Rowe and Mylleville (1996)	2.5	28	10.2	Fibrous peat
Kirk (2001)	2.7 – 8.2	26.1 – 30.4		Ombrotrophic blanket peat
Warburton et al (2003)	5.0	23	9.68	Basal peat
Warburton et al (2003)	8.74	21.6	9.68	Fibrous peat
Dykes and Kirk (2006)	3.2	30.4	9.61	Acrotelm
Dykes and Kirk (2006)	4.0	28.8	9.71	Catotelm
O'Kelly and Zhang (2014)	0	28.9 - 30.3	-	Pseudo-fibrous peat
Estimated Design Value	**5.0**	**23**	**10**	**-**

The design values given in **Table 5.9** have been adopted on a site wide basis. The water table level is assumed to be at ground level (m = 1) to provide a conservative assessment based on a flooded conditions worst case scenario such as during a high intensity rainfall storm event.

The Factor of Safety (FoS) **F** values for the Development Site have been calculated using GIS to derive the **F** value based on the interpolated peat depth map, DTM and the design values given in **Table 5.9**. In addition, a loaded analysis has been conducted by adding a load of 10 kPa equivalent to the load implied by a 1m high stockpile of peat (for example side cast during road construction) to the shearing forces.

The Factor of Safety results are summarised in **Figure 13.0** in **Appendix A**.

The best practice guidance suggests that F values of <1.0 should indicate slopes that have or may in future experience failure under the modelled conditions and as such are considered areas of

increased risk. However, Boylan *et al* (2008) argue that given the uncertainties in relation to the strength of peat and factors that cause peat landslides a cautious approach should be adopted. Their study indicates that a relatively high **F** value should be used to identify slopes with the potential for instability and as such an **F** value of 1.4 has been used in this assessment.

The results of the infinite slope analysis for the unloaded scenario reveal that under the modelled conditions the entire Development Site contains **F** values >1.4, except for the most extreme slope angles along the Pulmulloch Burn. The results are noted to be consistent with the conditions observed on the Development Site where no relic peat slide failures were identified. In the location of the peaty-debris slides within the Development Site the analysis confirms that these are likely to have been initiated in the substrate rather than within the peat.

The loaded analysis indicates that under loaded conditions large areas of the Development Site contain **F** values <1.4. However, in most cases the areas with **F** values <1.4 are situated along steep slopes with shallow thicknesses of peat such as the valley sides of the Water of Ken valley, north side of Coranbae Hill, south of Alhang and the north side of Alwhat. In general, the lower, shallower slopes with deeper peat depths contain **F** values >1.4 except in areas over steepened by gullies and water course as well as along localised steep slopes around the north of Alhang, west of Alwhat and around Brown Hill.

Although the preliminary stability assessment indicates that areas of the Development Site may be susceptible to failure, there is considerable uncertainty in the geotechnical parameters of peat identified in the literature (Boylan *et al*, 2008) and no site-specific assessment has been undertaken. As such, a conservative approach using relatively high factor of safety has been used in the stability assessment. Therefore, the factor of safety values calculated herein should only be considered as indicative of the potential peat slope stability. A detailed assessment of the peat slope stability should be undertaken using site specific design parameters taken from a ground investigation, particularly where slope angles exceed approximately 3° and peat depths exceed 1.0m.

6. Peat Landslide Risk Assessment

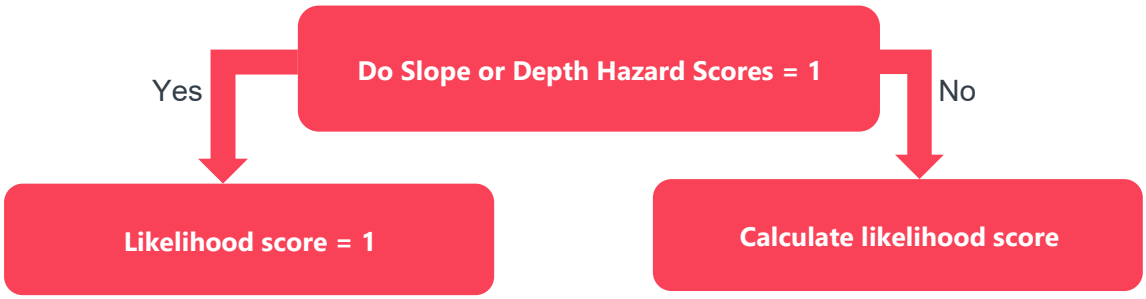
The approach for assessing the risk of a peat landslide occurrence considers the combination of the likelihood of a slide occurring in an area of peat multiplied by the consequences of a failure. This provides a means of identifying areas of the Development Site where there is a potential risk of a slide occurring such that preventative measures may be prioritised at an early stage of the Proposed Development.

6.1 Peat Landslide Likelihood

Hazard scores have been mapped across the Development Site as detailed in Section 5. This has been achieved using GIS to create ranked polygons for each category based on desk-based information and site observations. The polygons have been converted to raster layers using the hazard ranking score and summed to provide a peat landslide likelihood score.

The above method does not take account of conditions where a peat slide is unlikely given the slope angle and peat depth conditions. As such, in order to account for this, the key contributory factors of slope angle and peat depth have been used to weight the hazard assessment as shown in **Figure 6.1** below.

Figure 6.1 Peat landslide likelihood weighting



The above method therefore applies to areas where it is considered that a peat landslide is unlikely due to the absence of peat depths and slope conditions that are considered conducive to peat landslide failure.

Based on this system the hazard scores in this assessment range from 1 (negligible likelihood) to a maximum of 35 (almost certain likelihood). **Table 6.1** outlines the hazard score ranges and how these scores relate to the likelihood score taken forwards in the assessment of peat landslide risk. The scoring system also takes into account the infinite slope analysis described in Section 5.3 to adjust the likelihood scores in areas where the likelihood of failure is increased based on the preliminary geotechnical assessment of peat slope stability. The likelihood scores have been positioned such that at least the most hazardous slope angles and peat depths along with one other extremely serious hazard and one substantial hazard would need to be presented in a given area to result in a Likely or greater likelihood of peat slide failure.

Table 6.1 Peat landslide likelihood scores

Hazard Score	F Value	Likelihood	Likelihood Score
1-10	>1.4	Negligible	1
11-17		Unlikely	2
18-24	>1.0 < 1.4	Likely	3
25-30		Probable	4
31-35	<1.0	Almost Certain	5

The results of the likelihood assessment for peat slide failure types are presented in **Figure 14.0** in **Appendix A**.

The results of the likelihood assessment for peat slide failure indicates that the Proposed Development is predominantly within areas where the peat slide likelihood is Negligible or Unlikely. However, areas with a Likely or greater peat slide susceptibility have been identified as follows:

- Along the slopes of Wedder Hill and Millaneoch Hill;
- At borrow pit A;
- Along the access tracks to T13 and T11 in the northwest;
- Along most of the access track east of borrow pit B; and,
- At crane pads and turbines for T1, T2, T3, T6, T7, T9, T10, T11 and T14

In general areas of Likely of greater peat slide susceptibility, and particularly the areas of Almost Certain likelihood have been identified in areas with factor of safety values <1.4 and on slopes with susceptible peat depths and slope angles. In addition, the presence of confirmed peat pipes (or conditions likely to give rise to their prevalence) as well as a potential incipient slope failure in the southeast of the Development Site have been a significant drivers of the higher susceptibilities in the southeast of the Development Site.

6.2 Consequence

A key step in the peat landslide risk assessment is to identify the potential effects that a peat slide may have on key receptors. The assessment of peat landslide consequences is a qualitative assessment of the effects on key physical and environmental receptors. For the purpose of this assessment the following receptors have been assessed:

- Public infrastructure (road, rail, utilities and public water supplies);
- Property (homes, livestock, commercial forestry, buildings whether occupied or vacant, and the windfarm itself);
- Surface water (rivers and streams including protected ecology);
- Water supplies;
- Cultural and heritage sites; and
- Ecology (rivers & terrestrial, including priority habitats).

In addition to considering the immediate impacts, the potential long-term impacts such as the cost and time taken for recovery of ecosystems and revegetation are also taken into account as part of the assessment of the consequences.

The consequences of a peat landslide on the wind farm infrastructure itself are also considered in the property receptors. However, the consequences to wind farm infrastructure are considered to be relatively minor in comparison to the potential environmental damage, loss of life or the socio-economic impacts caused by damage to public infrastructure and watercourses. A peat landslide is only likely to result in damage to low cost, easily repairable access tracks, hard standings and below ground cables. A slide is unlikely to result in the toppling of a turbine or other structures with deep foundations that may result in significant secondary consequences such as fires, leaks and contamination of watercourses. As such, the consequences are considered to be moderate as summarised in Table 6.3.

Predicting the magnitude of a failure and the run-out distance is very difficult as this depends on the nature of the peat source and the relative proportions of peat to water (Evans and Warburton, 2010). In addition, should a peat slide enter a watercourse, run-out distances and impacts may be observed many kilometres downstream of the source area as was the case at the Derrybrien failure in Co. Galway, Ireland in 2003 (Bragg & Lindsay 2005). In these cases, the impacts may be observed over a significant proportion of the catchment and are likely to remain observable in the relatively long term. However, in many instances minor slumping is localised and little or no impact to receptors is observable.

In order to establish the exposure, information on the key receptors has been assessed in GIS and the likely consequences determined by the location of receptors relative to proposed infrastructure. The assessment considers that any receptor is at risk of an impact from any infrastructure location regardless of distance. However, the assessment does consider the presence of physical barriers such as water courses, valleys and breaks in slope which would abruptly redirect or halt a peat landslide. It should be noted that this is a conservative assessment of the risk.

Consequence scores have been considered for distances up to 500m from the Proposed Development site boundary taking into account the local topography where a slide may run from an onsite location to an offsite receptor.

Tables 6.2 to **6.4** outline the consequence classifications. **Figure 15.0** in **Appendix A** shows the receptors that have been considered in the assessment and illustrates the worst-case consequence scores based on the maximum consequence score from any one of the receptors. It is the maximum consequence score that has been taken forward to the Peat Landslide Risk Assessment.

Table 6.2 Consequences for cultural and ecological receptors

Consequence (Score)	Cultural and Heritage Sites	Ecology (including GWDTE's)
5 - Very High	Potential for damage to Scheduled Monuments of national importance.	Destruction of designated sites. Impacts requiring significant cost and time to restore.
4 - High	-	-
3 - Moderate	Potential for damage to or loss of non-scheduled cultural and heritage sites.	Destruction of sensitive groundwater dependent eco-systems requiring high restoration costs.
2 - Low	-	-

Consequence (Score)	Cultural and Heritage Sites	Ecology (including GWDTE's)
1 – Very Low	No cultural or heritage sites within the potential runout zone.	Destruction of non-designated habitats and ecosystems (e.g. open moorland and farm land).

Table 6.3 Consequences for man-made receptors (including the wind farm)

Consequence (Score)	Public Infrastructure (road, railways, utilities public water supplies)	Property (residential properties, cattle and commercial forestry)
5 - Very High	Damage or blockage of major infrastructure including main line railways, A roads and motorways. Serious damage and potential for death. Long term delays and disruption with very high repair costs and serious social and economic impacts at a regional scale.	Loss of life at a residential property.
4 - High	Damage or blockage of locally significant infrastructure including railways and B roads. Short to medium term delays with high repair costs and social and economic impacts on the local community. High costs to provide temporary measures to maintain supplies / services (e.g. tankered water supply).	-
3 - Moderate	Damage or blockage of C roads. Low repair costs, short term delays and low social and economic impacts on the community.	Damage to fields and pastureland. Loss of livestock. Loss of forestry and damage to plantations. Damage to wind farm infrastructure including the tracks, hard standings and ancillary structures.
2 - Low	Damage or blockage of unclassified roads, tracks and rights of way. Very low repair costs, short term delays and economic impacts on individuals (i.e. residents and landowners).	-
1 – Very Low	The significant impacts of peat slide or bog flow are unlikely to be observed at the receptor.	The significant impacts of peat slide are unlikely to be observed at the receptor.

Table 6.4 Consequences for hydrological receptors

Consequence (Score)	Surface Water	Water Supplies
5 - Very High	Potential for direct impacts on highly sensitive rivers or lochs1 such as Afton Reservoir. Significant impacts including a large reduction of animal populations. Impacts requiring high costs to restock and / or restore. Very high socio-	Potential for significant direct impacts on public water supplies, significant reduction in supplies and/or water quality. High cost impacts such a repair and/or replacement and additional measures to maintain water quality over the long term.

	economic impacts (e.g. long term suspension of fishing).	
4 - High	Potential for indirect impacts on highly sensitivity rivers and lochs via peat slides entering tributaries <7km upstream. Pollution due to the transport of suspended solids to the receptor. Potential for high socio-economic impacts (e.g. reduction in fishing).	Potential for indirect impacts on public water supplies by pollution of the source indirectly via tributaries. Lower cost and short term impacts such as temporary measures to maintain water quality.
3 - Moderate	Potential for direct impacts on low or medium sensitivity rivers and lochs. Potential for lesser impacts on highly sensitive rivers and lochs >7km downstream of the source area due to distance, dilution and deposition. Impacts requiring lesser restoration works and lesser impact on the sensitive rivers and lochs downstream. Moderate to high socio-economic impacts (e.g. short term reduction in fishing on a river of lesser importance).	Potential for damage to residential private water supplies supplying many properties downstream of the Development Site. Lower cost impacts such as replacement/repair and import of tankered water supplies.
2 - Low	Potential for indirect impacts on low or medium sensitivity rivers and lochs via tributaries due to the transport of pollution. Potential for impacts due to peat entering a major drainage ditch. Lesser impact at low or medium rivers or lochs and negligible impacts at sensitive major rivers or lochs downstream.	Potential for damage to private water supplies for few properties requiring low cost and short term replacement/repair and supply of bottled water.
1 – Very Low	Peat entry into a surface water is unlikely	Very low or no potential for impacts on water supplies.

Note
Includes both man-made lochs, reservoirs and dams.

6.3 Peat Landslide Risk Assessment

The overall risk of a peat slide event has been calculated as the product of the likelihood and consequence score. **Table 6.5** shows the associated risk ranking as derived from Table 5.3 in the best practice guidance and provides the indicative risk of a peat slide.

Table 6.5 Risk Ranking

		Consequences				
		Very Low	**Low**	**Moderate**	**High**	**Very High**
Likelihood		**1**	**2**	**3**	**4**	**5**
Negligible	1	1	2	3	4	5
Unlikely	2	2	4	6	8	10
Likely	3	3	6	9	12	15

Probable	4	4	8	12	16	24
Almost Certain	5	5	10	15	20	25

The suggested actions based on the peat landslide risk are summarised in **Table 6.6** below.

Table 6.6 Suggested actions based on Risk Ranking

	Column heading
>20 - High	Avoid Proposed Development at these locations.
10 – 19 - Moderate	Proposed Development should not proceed unless hazard can be avoided or mitigated at these locations, without significant environmental impact, in order to reduce risk ranking to low or negligible.
5 to 9 - Low	Proposed Development may proceed pending further investigation to refine assessment and mitigate hazard through relocation or re-design at these locations.
1 to 4 - Negligible	Proposed Development should proceed with monitoring and mitigation of peat landslide hazards at these locations as appropriate.

The results of the peat landslide risk assessment are presented in **Figure 16.0** in **Appendix A**. The findings indicate that the Proposed Development is in areas of predominantly Negligible to Low Risk of peat slide failure with areas of Moderate risk identified. In the northwest of the Development Site areas of Moderate peat landslide risk have been identified throughout mid and upper slopes of Afton Water and the Alwhat Burn watershed. In particular Moderate risks have been identified at:

- temporary compound A;
- T13 blade laydown;
- T11 blade laydown;
- borrow Pit A; and,
- along the access tracks past temporary compound A to T11, T13 and T15.

In addition to areas of Moderate risk in the northwest localised areas of High risk have been identified at the head of the Alhang Burn to the east of T13 and upslope of temporary compound A. The Moderate risks in the northwest of the Development Site are principally driven by the potential high consequence of a slide on the Afton Reservoir which is a source of public drinking. If a peat slide was to occur and impact the upper reaches of either the Afton Water or Alhang Burn it is perceivable that pollution of the reservoir by suspended solids and sudden increases in nutrient content could impact the reservoir.

The localised areas of High risk are driven by a combination of the high consequences and higher peat landslide susceptibility identified by the infinite slope analysis at the head of the Alhang Burn. However, as noted in Section 5.3, the infinite slope analysis is considered to be a conservative analysis of peat slide susceptibility, particularly as water table levels at surface levels at or near the ground level are considered unlikely to occur on the slopes identified as susceptible.

In the southeast of the Development Site the peat landslide risks are predominantly Negligible to Low. However, the assessment has identified a number of localised areas of Moderate risk where peat landslide susceptibility was considered to be higher due to the presence of either pre-failure

indicators, peat pipes or conditions conducive to the development/presence of peat pipes. In particular Moderate risks have been identified:

- along the access track adjacent to the west of T5;
- along the access track to T2/T8 and T6;
- at the access track between the spurs to T9 and T4/T7; and,
- at the blade laydown for T3

The peat landslide risk assessment has not identified any areas of High peat slide risk in the southeast of the Development Site.

7. Mitigation Measures

As discussed in Section 6, under the current conditions the peat landslide risks at the Development Site are considered to be predominantly Negligible to Low for the majority of the Proposed Development with localised areas of Moderate and High risk driven by peat landslide susceptibility and in the northwest driven by peat landslide consequences. The construction of the Proposed Development and alterations to the Development Site slopes are considered a potential contributory factor that may increase a slope's susceptibility to peat instability resulting in a peat landslide. In general, the construction practices which would be avoided, include:

- stockpiling and side casting of excavated materials on, or at the top of marginally stable peat covered slopes;
- stockpiling, side casting or siting floating roads at or near convex slope breaks;
- loading of susceptible peat by floating roads;
- removal or breaking of acrotelmic peat beneath floating roads;
- removal of support at the toe of peat covered slopes and particularly at the toe of convex slopes; and
- poor drainage practices such as the draining of excavations, and placement of outfalls on to peat covered slopes, blocking of drainage channels and ponding of water.

Further discussion on specific mitigation measures is provided in the sub-sections below.

7.1 General Considerations

Prior to construction, a detailed ground investigation would be undertaken to assist in detailed design of the Proposed Development as well as any slope modification. This would form part of the planning conditions for the Section 36 application and is considered the best opportunity to confirm the peat landslide hazard assessments and to perform detailed assessment of the most susceptible slopes based on site specific parameters, observations and the proposed construction methods.

The ground investigation would aim to provide information on the geotechnical characteristics (e.g. shear strength and bulk density) of the peat as well as the composition and form and underlying mineral substrate to identify any potential failure surfaces. The results of the ground investigation would inform the development of a geotechnical risk register which would be reviewed and updated at each stage of the post-consent phase of the Proposed Development.

Where possible the primary mitigation would be to make use of the micro-siting allowances to further refine the wind farm layout in order to site wind farm infrastructure in areas of the shallowest peat or peaty soils.

In addition to the above, targeted visual and quantitative monitoring of slopes susceptible to failure would be performed during construction and a detailed monitoring programme would be developed for sensitive areas prior to construction. Where visual monitoring is undertaken, this would record any signs of tearing, creeping, heaving, subsidence, recent close of grips and changes to the peat hydrology. Where necessary monitoring would also include quantitative methods such as surface monument monitoring and where necessary measures to support the slope would be implemented.

Construction method statements for wind farm infrastructure in areas of Low or Moderate risk will be developed that will include measures to avoid working in these areas and monitor them during, and shortly following, periods of heavy or sustained rainfall.

7.2 Excavations

Excavations at the Proposed Development will be required at cut tracks, turbine bases, crane pads, blade laydowns, the SPEN substation/control building and the temporary compounds. In areas of peaty-soils, shallow peat depths and Negligible peat landslide risk, normal best practice construction methods may be employed (e.g. Scottish Renewables, Scottish Natural Heritage, SEPA and Forestry Commission guidance).

Where excavations are proposed in areas of Low to Moderate risk further detailed assessment would be considered alongside mitigation measures should further assessment confirm the slopes are potentially susceptible to failure. In general, mitigation measures would aim to maintain current drainage routes or divert it to purpose-built drainage networks to reduce the impact on the peat hydrogeology, hydrology, avoid the surface loading of slopes and support the slopes and excavations where necessary. The mitigation measures would include the following:

- A walkover would be undertaken by a suitably qualified and experienced geotechnical engineer prior to construction to establish the baseline flow regimes, identify existing peat pipes and any further signs of instability to target mitigation;
- Construction activities that require the stripping of peat would be overseen by the geotechnical engineer;
- Construction method statements would include awareness of peat instability and pre-failure indicators and would detail conditions for ceasing works. In addition, site inductions, toolbox talks and training would be incorporated to ensure all site personnel are able to recognise the signs of instability;
- Where necessary a purpose built drainage network that intercepts surface water from flushes, grips and drainage ditches would be constructed. This would be designed with adequate capacity to cater for the expected heavy or prolonged rainfall events;
- Regular inspection of the upslope area of excavations and tracks for ponding caused by the Proposed Development would be undertaken, and where this occurs, measures to drain ponded water to the drainage network would be implemented;
- Where interception of surface water either side of the crane pads and tracks is not proposed, it would be designed in a manner that allows downslope throughflow through the foundation so that ponding upslope is avoided. This would include the installation of free draining material and/or perforated pipes beneath hard standings and tracks where flushes are identified. Where peat pipes, grips and ditches are discovered during construction, flows through the track or crane pad will mimic the natural flows;
- Cut-off drainage ditches upslope of the excavations would be constructed to divert flows to the purpose built drainage network and avoid ponding in excavations. Where ponding in excavations occurs (e.g. from rainfall or groundwater) it should be pumped out to the drainage network;
- Outfalls and drainage onto the peat would be avoided. Where an outfall will drain to an existing channel, measures would be installed to avoid erosion and headward gully formation;

- Drainage channels and flows through tracks and hard standing would be periodically checked during construction, particularly after any storm event to ensure their continuing and effective functionality;
- Excavated spoil, rock and peat will not be stored on slopes with a Moderate risk of peat landslide;
- Where infrastructure undercuts a peat covered slope with a Moderate risk of peat landslide, visual monitoring of the slope will be conducted regularly during construction and measures to support the slope will be implemented as necessary; and,
- Excavations through deep peat would be appropriately designed to prevent collapse of the peat into excavations and the development of tension cracks. Where battering is proposed, regular monitoring of the peat surrounding the excavation for signs of movement and seepage at the substrate interface would be performed daily alongside normal pre-work checks.

In addition, to avoid water ponding upslope of the track, storage locations for excavated spoil, rock and peat should be carefully selected to avoid loading moderately stable slopes or slopes with peat depths >1.0m.

7.3 Floating Roads

Best practice guidance on the design and construction of floating roads on peat is well documented by NatureScot (2015) and Forestry and Land Scotland (2010) and the guidance and methods presented therein would be implemented. The suitability of a slope for construction of a floating road would take into account the peat landslide risks.

Where floating roads are required, the route would be subject to detailed ground investigation including an assessment of the bearing capacity of the peat in relation to the maximum loads it may experience, loading rates and slope stability. In addition, the route of the floating road would be walked to identify the location of possible surface and sub-surface peat drainage features crossing the proposed routes in order to target mitigation measures. These measures would aim to maintain and mimic these drainage routes and avoid focussing them on to susceptible slopes. This may require non-intrusive methods of ground investigation to identify as many of the sub-surface features as possible. Furthermore, the walkover and detailed design of the access tracks will micro-site tracks away from convex breaks in slope and very wet ground.

During construction regular visual and quantitative monitoring of floating tracks on susceptible slopes would be undertaken to identify any potential indications of movements including slippage, failures and tearing of the peat.

In addition to the above, further mitigation measures that would be required include:

- Surface vegetation and acrotelmic peat would be left *in-situ* to provide additional strength and support;
- Floating road construction would be conducted at a rate which allows sufficient time for the peat to 'rebound' and regain strength. This may involve applying aggregates in a number of layers and monitoring of settlement;
- Construction of the floating roads would be conducted outward from the starting point so as to limit loadings directly onto peat by construction traffic;
- Measures to limit the weight of delivery vehicles may be required to reduce loading onto the peat during construction.

The above mitigation measures will also be required at locations where displacement or floated/piled crane pads are required.

7.4 Borrow Pitting

The Proposed Development contains two borrow pit search areas with Borrow Pit search area A situated in an area of predominantly Moderate risk with small localised areas of High risk. Borrow Pit search area B is situated within an area of very shallow peat and Negligible peat landslide risk.

A detailed ground investigation would be undertaken to determine the susceptibility of the upslope area that will be undercut by the excavation. In addition, the ground investigation will also provide information to determine the volumes of stone that are available and to establish suitable methods of extraction in order to reduce the amount of borrow pitting. The excavation techniques employed would seek to limit methods that are likely to induce larger ground accelerations where possible (e.g. blasting).

Where required, mitigation measures would include monitoring of the upslope areas of the borrow pit (either visually or quantitatively) and formation of a catch mound or a catch fence upslope of the excavation.

Where blasting is unavoidable a borrow pit scheme of works will be prepared that includes a borrow pit blasting method statement. This would detail measures to reduce blasting, vibrations and monitor sensitive slopes for movement. In addition to the mitigation presented in the borrow pit scheme of works the following would also be required:

- Blasting would not be undertaken during and shortly following periods of heavy or sustained rainfall to reduce the risk of a slide event occurring during periods where peat moisture contents at the peat/substrate interface are at their highest;
- All blasts will be designed and supervised by a suitably qualified blast engineer to minimise the number of blasts required;
- The smallest amount of explosive will be used to minimise vibrations;
- Any other excavation and/or blasting of the peat substrate (i.e. rock or deposits) will be ceased during the borrow pit blasts to minimise the magnitude of vibrations within the substrate at any one time; and,
- Areas of peat (>0.5m in thickness) within a distance of the blast as identified in the method statement will be visually inspected prior to and following the blasts to identify any areas of instability. Where instability is identified prior to the blast it will not proceed until further assessment of the peat landslide likelihood and risk has been established and mitigation measures have been implemented.

7.5 Side Casting & Stockpiling

A peat management plan detailing the measures for handling and storage of peat and the design and selection of peat and subsoil storage areas has been prepared separately to this peat landslide risk assessment (EIA Report Appendix 6B). The recommendations of the peat management plan should be followed throughout the construction of the Proposed Development and storage areas should be confirmed through detailed ground investigation and confirmation of the peat landslide risks at the stockpiling areas.

Storage of excavated materials on slopes with peat depths >1.0m and areas with a Low or greater risk of peat landslides should be avoided. Where storing of materials in these areas is unavoidable, a detailed assessment of their stability should be undertaken during the post consent ground investigation and mitigation measures similar to those for floating and cut tracks should be employed accordingly.

8. Conclusions & Recommendations

8.1 Conclusions

A peat landslide risk assessment has been conducted in general accordance with the Scottish Government best practice guidance document Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments (2nd edition, 2017). The methodology has used a probabilistic and deterministic approach to assess the hazards supported by field observations and published literature to determine the potential risk of peat slide and bog flow failure across the Development Site.

A series of Phase 1 and 2 peat depth surveys comprising a total 4,158 peat depth measurements have been taken across the Development Site. This has revealed peat depths ranging between 0.00m and 3.80m. A total of 2,415 (~58%) recorded peat depths ≥0.5m and the calculated mean of all peat depths ≥0.5m is 1.08m.

An assessment of peat landslide likelihood has been undertaken to assess the likelihood of a peat slide failure within the Development Site. This has been undertaken by combining the results of a hazard assessment and the results of the infinite slope analysis to identify areas of peat landslide susceptibility.

The results of the infinite slope analysis reveal that under unloaded conditions the majority of the Development Site has an F value >1.4. This was noted to be consistent with the conditions observed on the Development Site where no relic peat slide failures were identified. In the loaded scenario large areas of the Development Site contain **F** values <1.4 but in most cases these are areas situated on steep slopes with shallow thicknesses of peat such as the steep valley sides of the Water of Ken valley. In general the lower, shallower slopes with deeper peat depths contain **F** values >1.4 except in areas over steepened by gullies and water course and along the steep slopes of Alhang, Alwhat and Brown Hill.

The results of the likelihood assessment indicate that the Proposed Development is predominantly within areas where the peat slide likelihood is Negligible or Unlikely. However, areas of Likely or greater peat slide susceptibility have been identified along some access tracks in the northwest and southeast, at borrow pit search area A and at the turbine and/or the crane pads for T1, T2, T3, T6, T7, T9, T10, T11 and T14. In general areas of greatest susceptibility have been identified in areas with factor of safety values <1.4. In addition, susceptible areas have been identified on slopes with extremely susceptible peat depths and slope angles, as well as the presence of, or conditions likely to be conducive to the presence of hazardous natural drainage features including peat pipes.

The result of the peat landslide risk assessment indicate that the Proposed Development is in areas of predominantly Negligible to Low Risk of peat slide failure. However, areas of Moderate risk have been identified throughout mid and upper slopes of the Afton Water and the Alwhat Burn catchments in the northwest of the Development Site. This includes at temporary compound A, borrow pit search area A, the blade laydowns for T11 and T13 and along the access tracks to T11, T13 and T15. In the southeast of the Development Site areas of Moderate risk have been identified along some of the access tracks and at the blade laydown for T3. In addition a number of small areas of High risk have been identified at the head of the Alhang Burn to the east of T13 and upslope of temporary compound A. In general, the Moderate and High risks in the northwest of the Development Site are principally driven by the potential high consequence of a slide on Afton Reservoir which is a source of public drinking water. In the southeast the Moderate risks are generally driven by the presence of susceptible slopes including those with natural drainage and pre-failure indicators.

8.2 Recommendations

The following recommendations are provided based on the assessments conducted herein.

A post-consent detailed ground investigation is recommended to assist in detailed assessment of peat slope stability in the most sensitive areas of the Proposed Development. The ground investigation should also aim to establish the nature and geotechnical parameters of the peat and peat substrate interface. It is recommended that ground investigation information is used to check/verify the peat slope stability assessments.

It is also recommended that primary mitigation measures are considered to relocate infrastructure from areas susceptible to peat landslides followed by mitigation to reduce peat landslide risks particularly where crossing peat pipes, flushes, peat grips and drainage ditches. The mitigation measures employed should aim to minimise additional loading or undercutting of susceptible peat covered slopes (especially convex slopes), maintain the current drainage of the peat, avoid ponding of surface water and where necessary redirect drainage to a purpose-built drainage network. In addition, monitoring of slopes may be required where a detailed ground investigation of the proposed infrastructure confirms that sensitive slopes may be moderately susceptible to peat landslides.

In conjunction with the above, a geotechnical risk register should be developed and maintained by a geotechnical engineer throughout the life cycle of the Proposed Development. During construction, a Geotechnical Clerk of Works should also be present on site to monitor sensitive slopes for movement and to manage any changes to the peat landslide risks.

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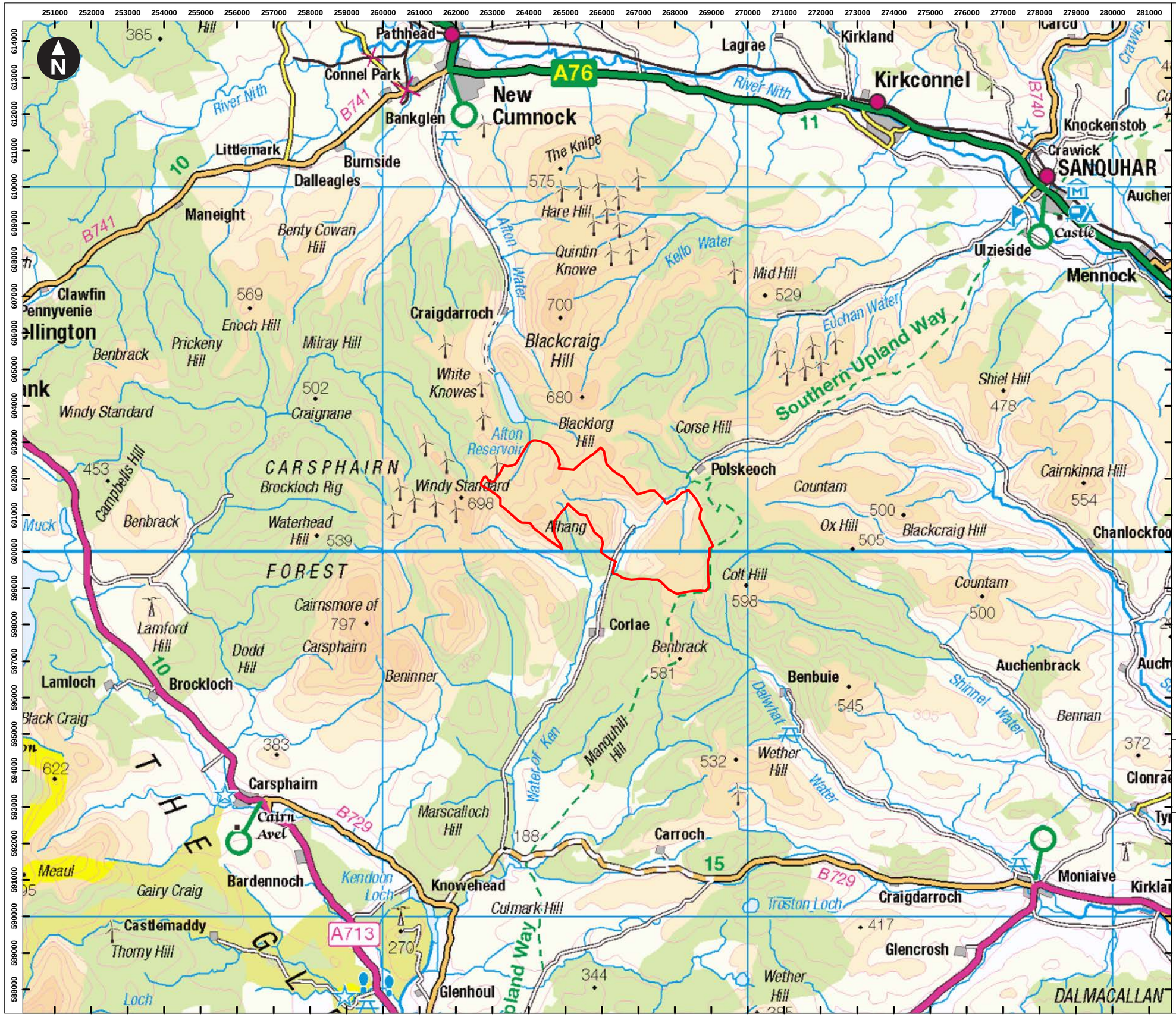
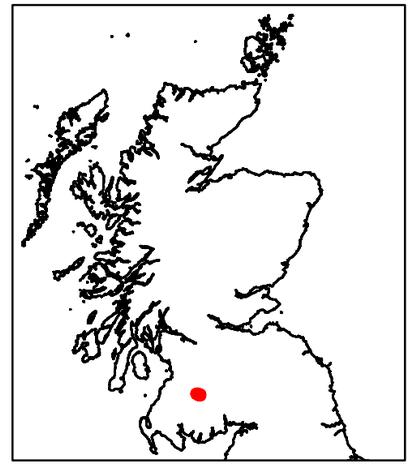
Appendix A
Figures



Key

Development Site boundary



0 1 2 3 4 5 Kilometers

Scale at A3: 1:100,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 1.0
Site location

October 2022

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262000 263000 264000 265000 266000 267000 268000 269000

604000 603000 602000 601000 600000 599000 598000

T1 T2 T3 T4 T5 T6 T7 T8 T9 T10 T11 T12 T13 T14 T15

TC-A TC-B BP-A BP-B MM-A MM-B

Galloway

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

Client

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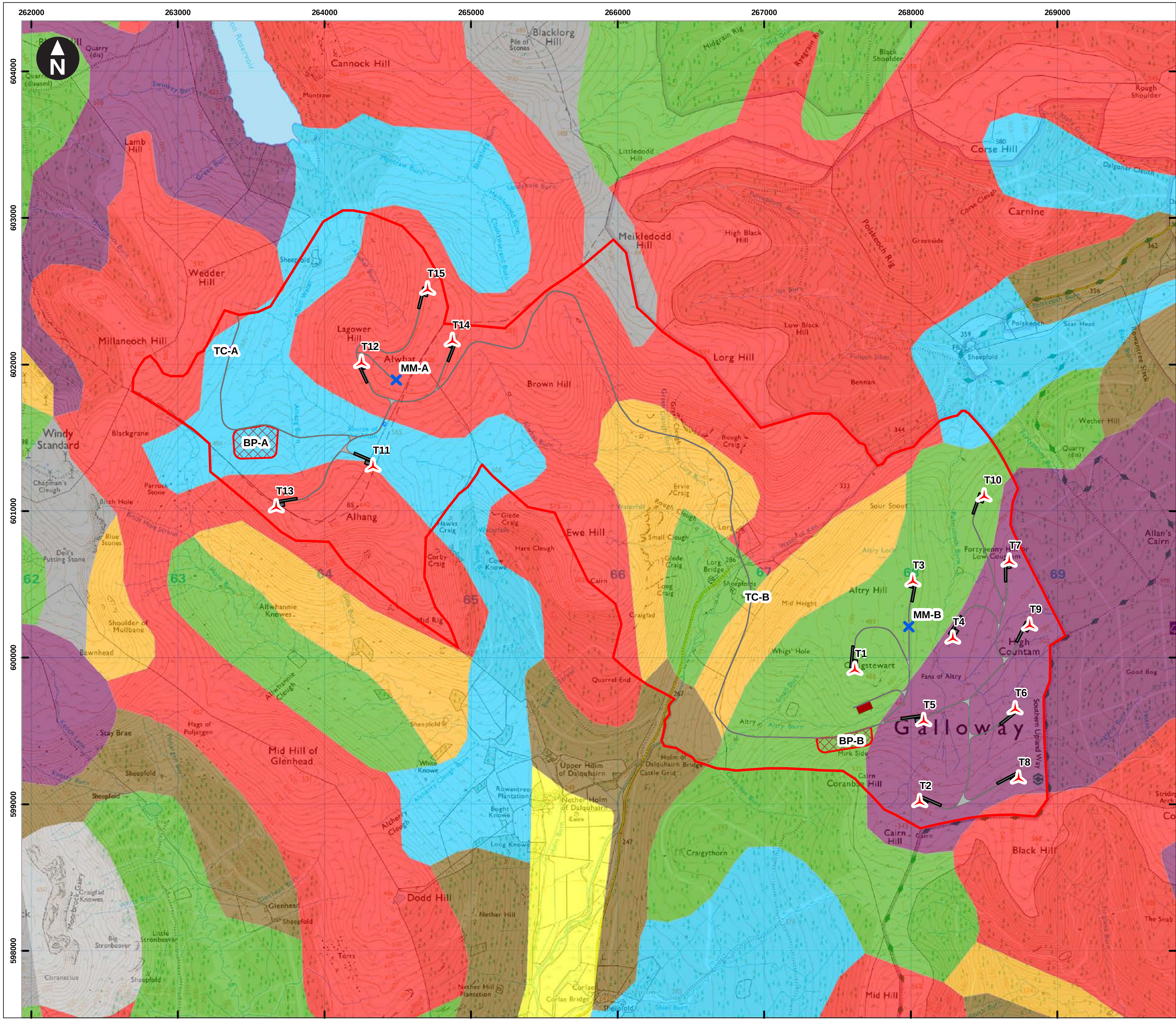
Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 2.0
Site layout

October 2022



Client

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Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 3.0
Soil Map of Scotland (1:250,000)

October 2022

wsp

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604000 603000 602000 601000 600000 599000 598000

N

T15 T14 T12 T11 T13 T10 T7 T3 T9 T4 T1 T6 T5 T8 T2

TC-A MM-A BP-A TC-B MM-B BP-B

Blacklorg Hill Cannock Hill Lamb Hill Wedder Hill Millaneoch Hill Lagower Hill Alwhat Brown Hill Windy Standard Blackgrane Alhang Ewe Hill Meikledodd Hill Littledodd Hill Black Shoulder Rough Shoulder Corse Hill Carnine High Black Hill Lorg Hill Bennan Wether Hill Altry Hill Whigs' Hole Clugstewart Fans of Altry High Countam Galloway Mid Hill of Glenhead Dodd Hill Allan's Cairn Black Hill Cairn Hill Coranbae Hill Craigythorn Mid Hill

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

NatureScot Soil Carbon Classification

- Class -2: Non-soil
- Class 0: Mineral soils
- Class 1: Carbon-rich and deep peat with all cover priority peatland habitats
- Class 2: Carbon-rich and deep peat with cover dominated by peatland habitats
- Class 3: Mostly carbon-rich soils with some deep peat and occasional peatland habitats
- Class 4: Area unlikely to include carbon-rich soils
- Class 5: No peatland habitat recorded

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3:1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 4.0
NatureScot Carbon and Peatland Map 2016

wsp

October 2022

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262000 263000 264000 265000 266000 267000 268000 269000

604000 603000 602000 601000 600000 599000 598000

T15 T14 T12 T11 T13 T10 T7 T3 T9 T4 T1 T6 T5 T8 T2

TC-A TC-B MM-A MM-B

Blacklorg Hill · Cannock Hill · Lamb Hill · Wedder Hill · Millaneoch Hill · Lagower Hill · Alwhat · Brown Hill · Meikledodd Hill · Littledodd Hill · High Black Hill · Low Black Hill · Lorg Hill · Bennan · Corse Hill · Carnine · Windy Standard · Blackgrane · Alhang · Ewe Hill · Altry Hill · Countam · Galloway · Mid Hill of Glenhead · Dodd Hill · Black Hill · Coranbae Hill · Cairn Hill · Mid Hill

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Access tracks
- Substation
- Borrow pit

BGS Superficial Geology

- Alluvium - silt, sand and gravel
- Glacial Till - diamicton
- Hummocky (Moundy) Glacial Deposits - diamicton, sand and gravel
- Peat
- Superficial Deposits - sediment

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 5.0
Superficial Geology

October 2022

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262000 263000 264000 265000 266000 267000 268000 269000

603000 602000 601000 600000 599000 598000 597000

N

T15 T14 T12 MM-A TC-A BP-A T11 T13 TC-B MM-B T10 T7 T3 T9 T4 T1 T6 T5 BP-B T8 T2

Lamb Hill Littledodd Hill Corse Hill Carnine Meikledodd Hill High Black Hill Polskeoch Rig Greenside Corse Cleugh Dalgonar Cleuch Wedder Hill Millaneoch Hill Lagower Hill Alwhat Brown Hill Low Black Hill Lorg Hill Polskeoch Scar Head Sheepfold Bennan Wether Hill Quarry (dis) Windy Standard Blackgrane Chapman's Cleugh Parrock Stone Bitch Hole Blue Stones Dell's Putting Stone Alhang Rough Craig Erryie Hawks Craig Glede Craig Hare Cleugh Cow Knowe Ewe Hill Small Cleugh Lorg Bridge Sheepfolds Altry Hill Mid Height Sour Snout Altry Loch Forty Penny Hill Low Cowlam Allan's Cairn Whigs' Hole Quarrel End Fans of Altry Good Bog Allwhannie Knowes Shoulder of Mullbane Bawnhead Allwhannie Cleugh Stay Brae Hags of Pollargon Mid Hill of Glenhead Sheepfold White Knowe Upper Holm of Dalquhairn Nether Holm of Dalquhairn Rowantree Plantation Holm of Dalquhairn Cattle Grid Coranbae Hill Cairn Hill Black Hill Striding Arch Benbrack Mid Hill Craigbane Melkle Dibbin Hill Little Dibbin Craigs Galloway

BGS Solid Geology

- Fault - inferred, displacement unknown
- Fault - inferred, thrust
- Axial plane trace of major syncline
- Margin of contact metamorphic aureole, symbol towards intrusion

- Kirkcolm Formation - wacke
- Portpatrick Formation - wacke
- Moffat Shale Group - mudstone
- Crawford Group - chert
- North Britain Siluro-Devonian Calc-Alkaline Dyke Suite - granitic, granodiorite, microdioritic and dioritic rocks
- Galdenoch Formation - wacke
- Unnamed Igneous Intrusion - microgabbro
- Crawford Group - basaltic-rock
- Moffat Shale Group - mudstone, chert and smectite-claystone
- Glenwhargen Formation - wacke
- Southern Midland Valley Felsite Sills - felsite
- South of Scotland Granitic Suite - granitic-rock
- Cairnsmore of Carsphairn Pluton - dioritic-rock
- Armathwaite-Cleveland Dyke - basaltic-andesite

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3:1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 6.0
Solid Geology

October 2022

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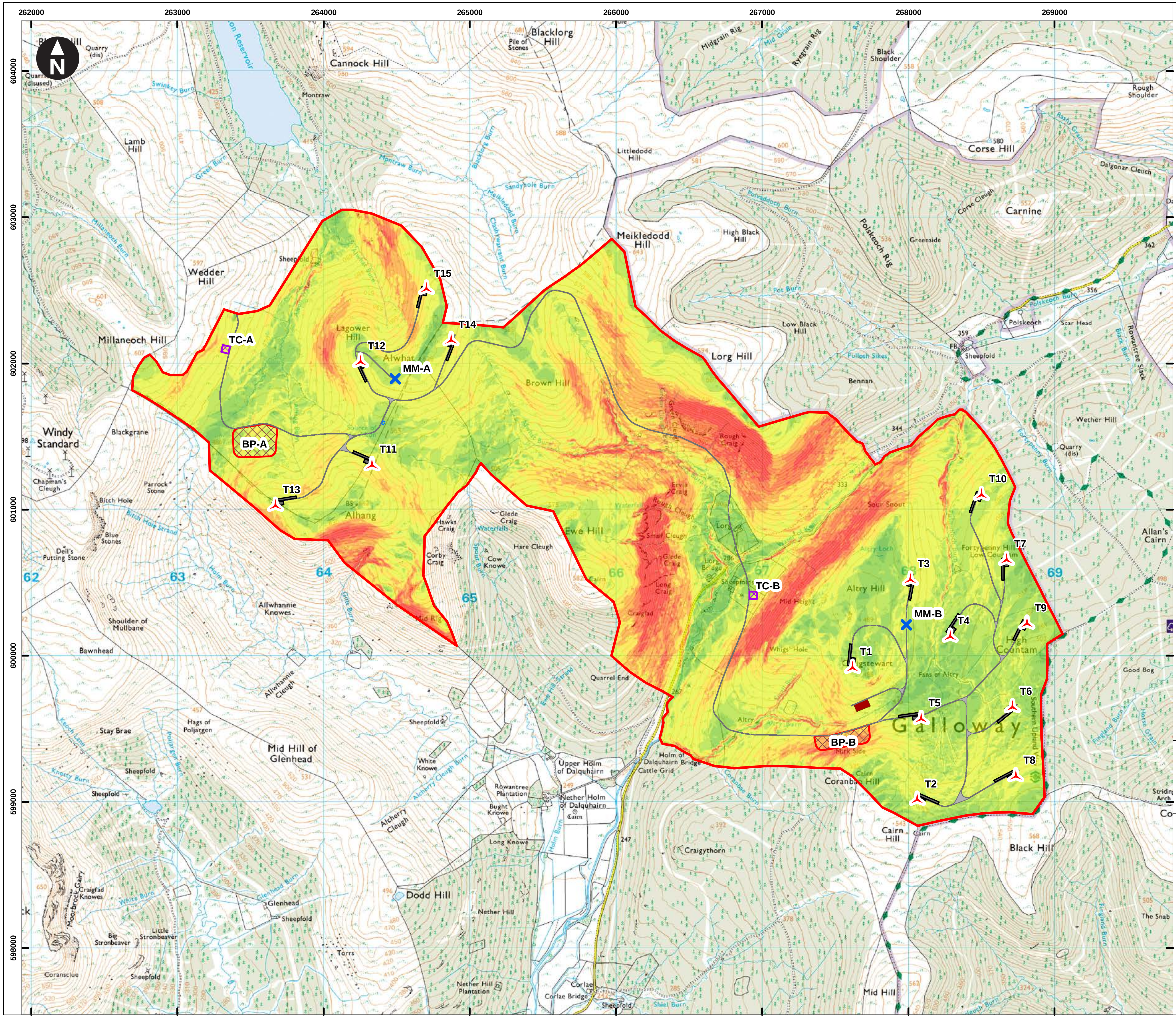

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Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

Slope Angle (degrees)

- 0 - 2
- 2 - 5
- 5 - 8
- 8 - 15
- 15 - 20
- 20 - 25
- 25 - 30
- >30

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 7.0
OS Terrain 5 DTM

October 2022

wsp

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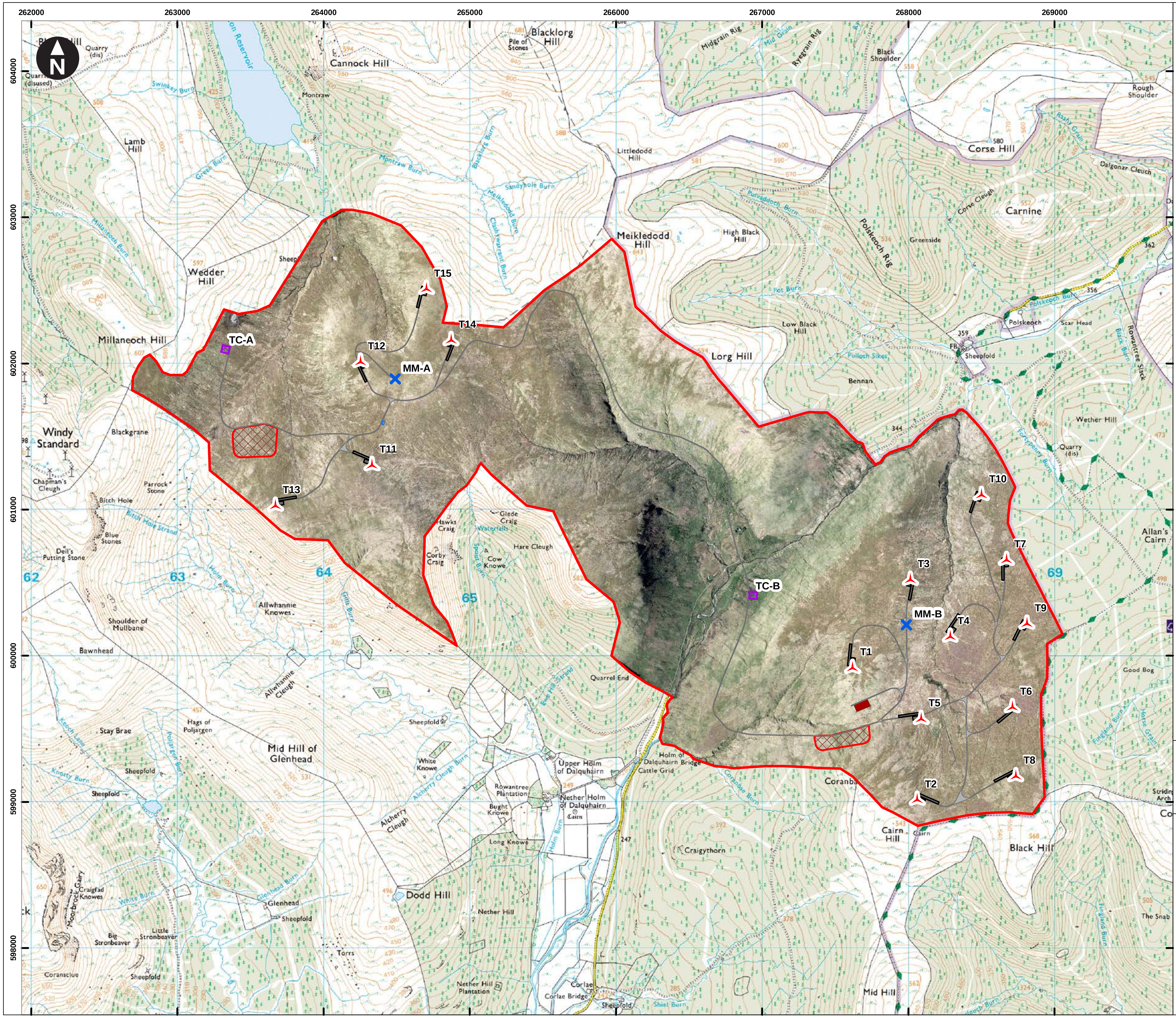

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 8.0
Aerial Imagery

October 2022

wsp

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604000 603000 602000 601000 600000 599000 598000

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 300 400 500 600 700 800 900 1,000 1,100 1,200 1,300 1,400 m

Scale at A3: 1:25,000

Client

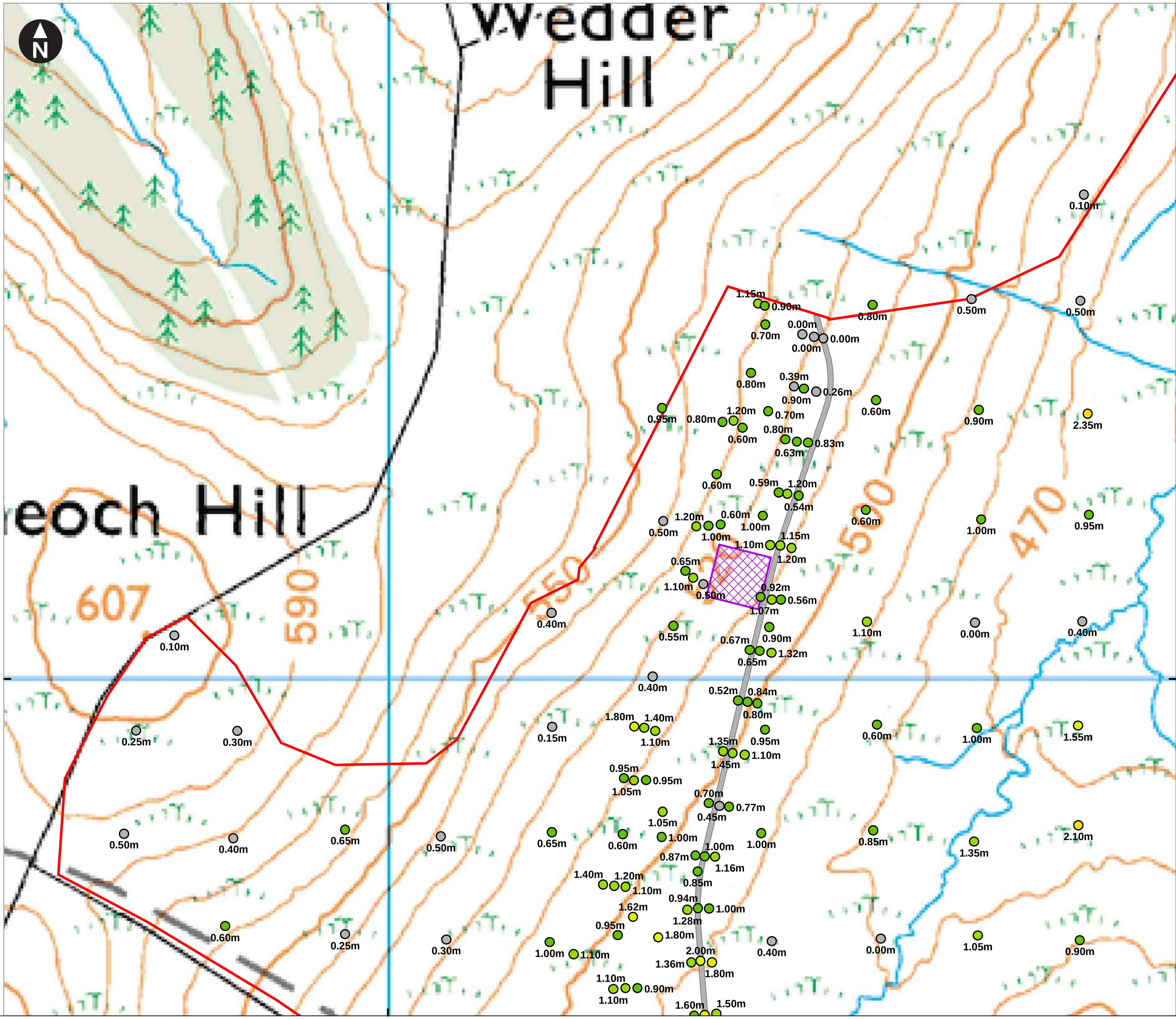
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.0
Peat Depth Survey Results

wsp

October 2022

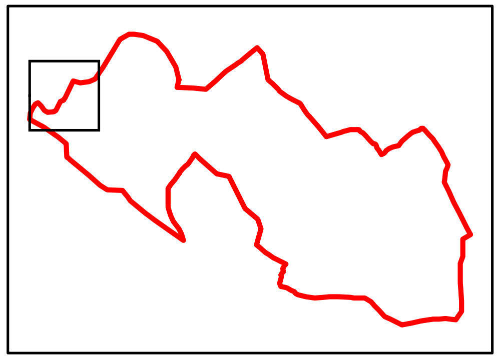


Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0



0 100 200 m
Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.1
Peat Depth Survey Results

October 2022

wsp

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

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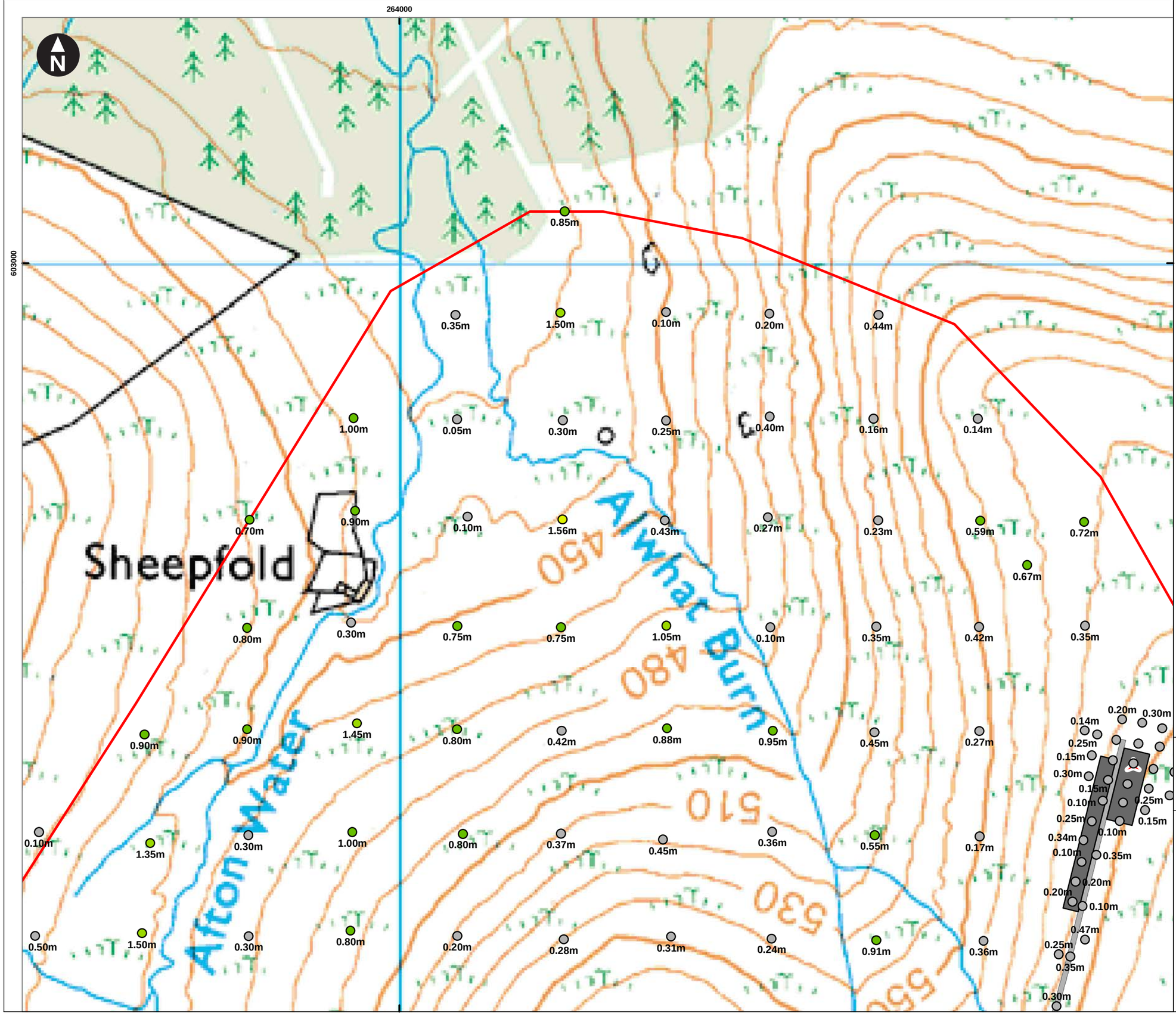
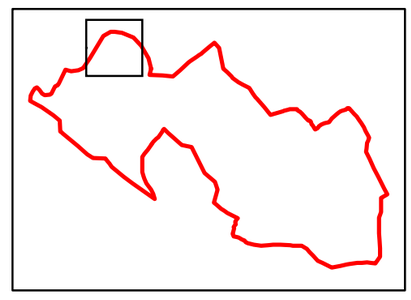


Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0



0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.2
Peat Depth Survey Results

October 2022

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265000

602000

Brown Hill

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

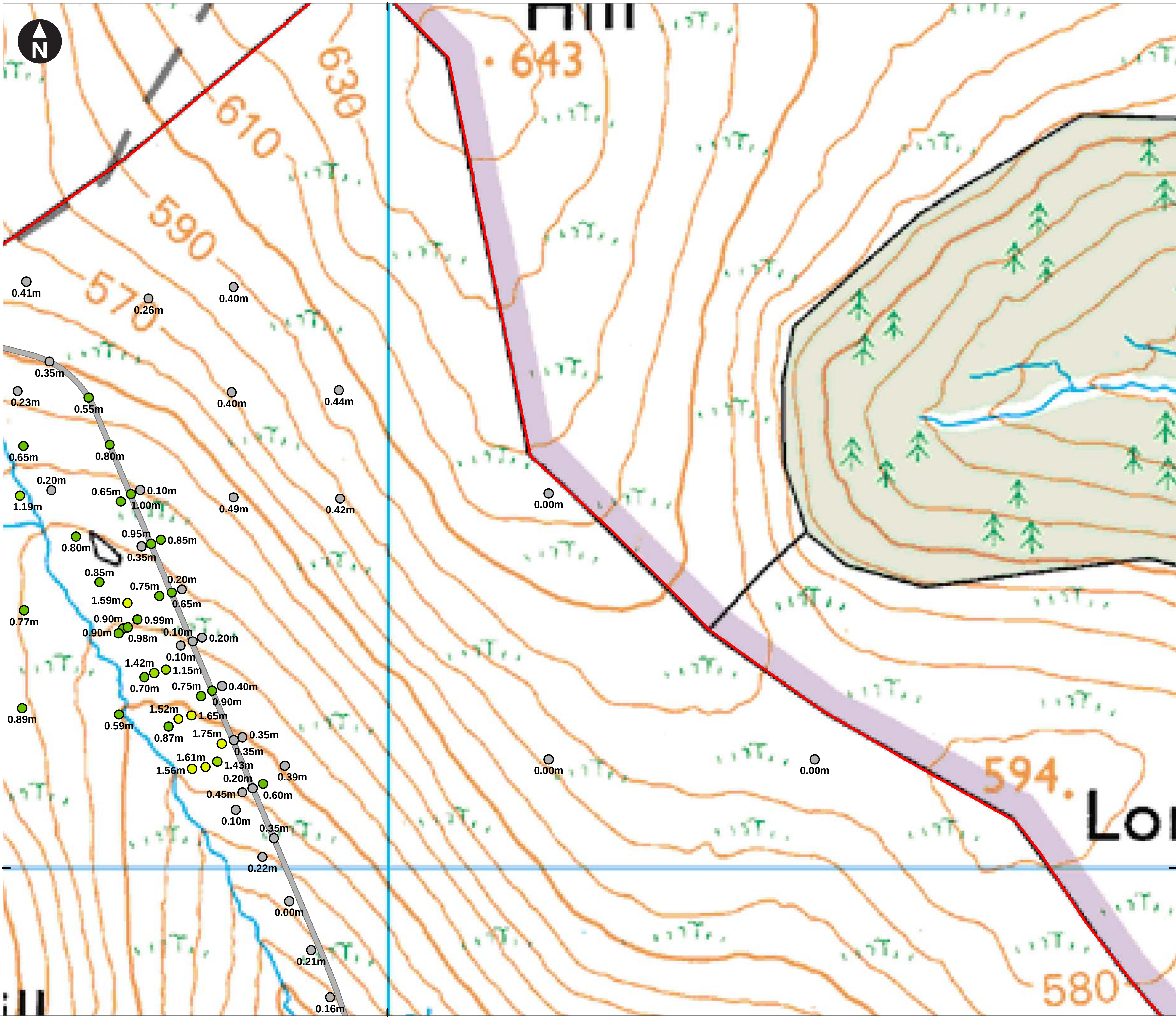
Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.3
Peat Depth Survey Results

October 2022

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira



Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.4
Peat Depth Survey Results

October 2022

wsp

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira

263000

601000

kgrane

Parrock Stone

ole

Bitch Hole Strand

N

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

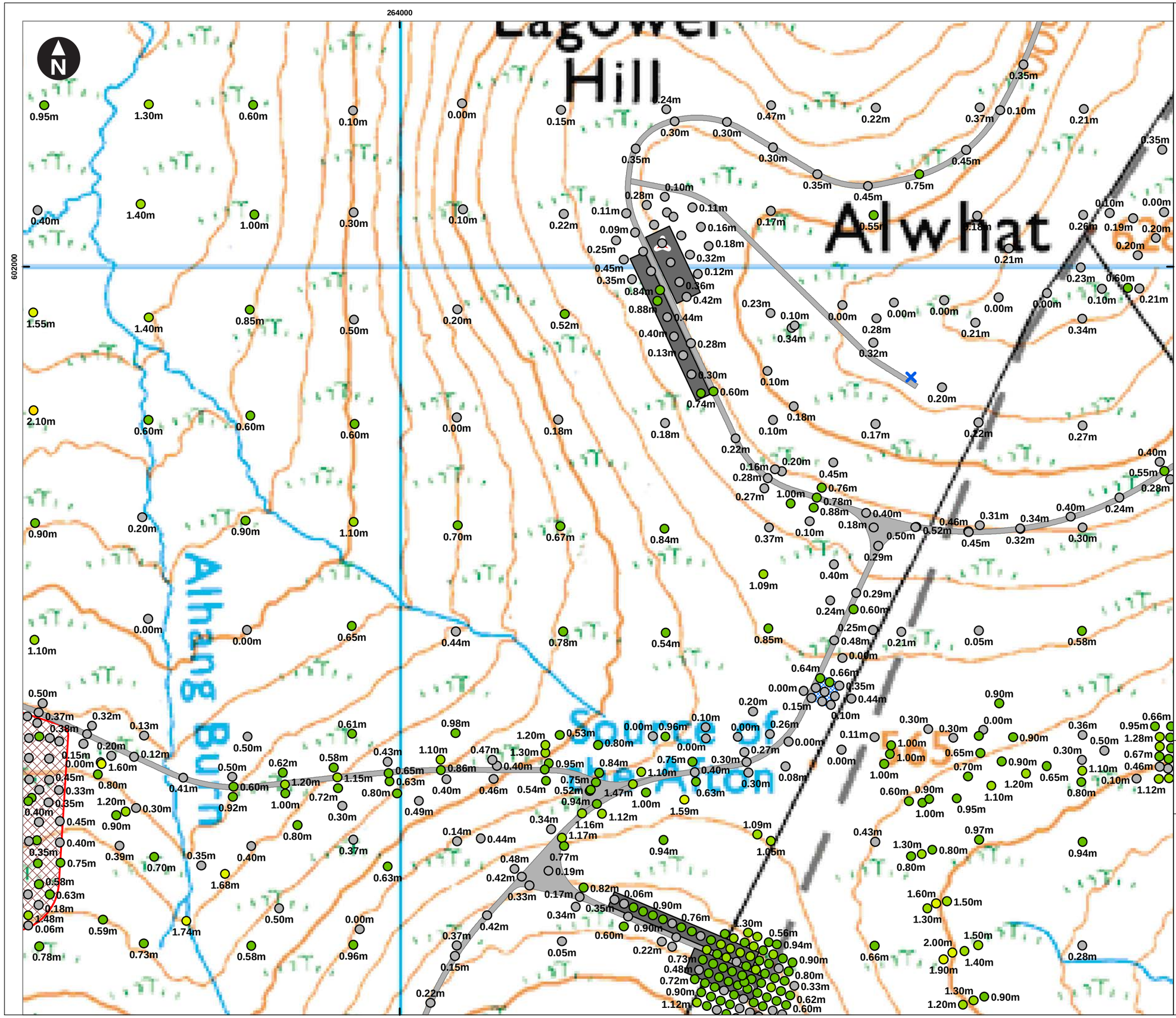
Lorg Wind Farm
Peat Landslide Risk Assessment

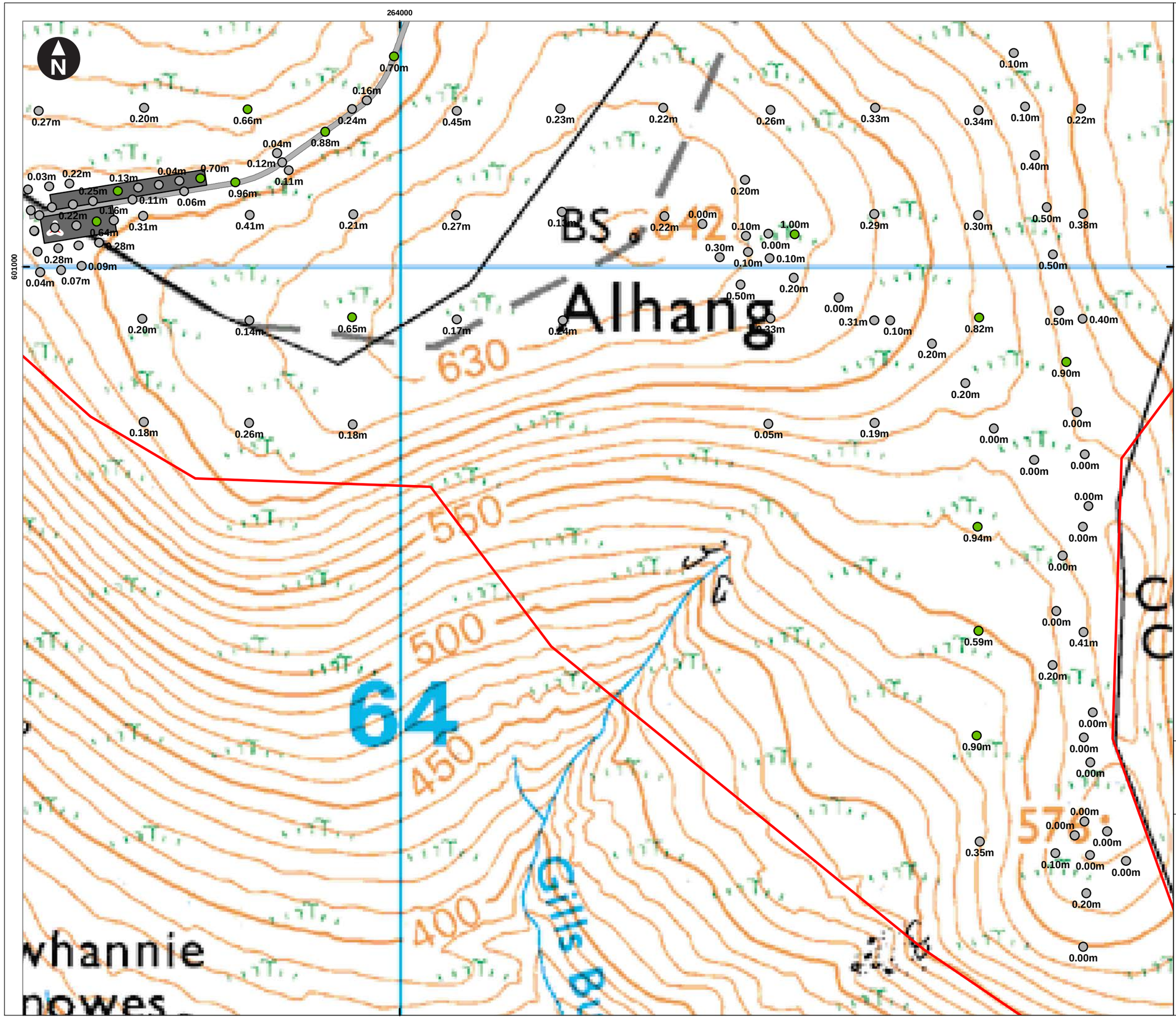
Figure 9.5
Peat Depth Survey Results

October 2022

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira


264000
602000
Lagower Hill
Alwhat
Alhang Burn
Source of the Afton
Key
Development Site boundary
Turbine location
Met mast location
Western control building
Crane pads
Access tracks
Substation
Borrow pit
Peat Depth (m)
0.0 - 0.5
0.5 - 1.0
1.0 - 1.5
1.5 - 2.0
2.0 - 2.5
2.5 - 3.0
3.0 - 3.5
3.5 - 4.0
0
100
200 m
Scale at A3: 1:3,500
Client
RWE
Lorg Wind Farm
Peat Landslide Risk Assessment
Figure 9.6
Peat Depth Survey Results
October 2022
W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira
32964-WOOD-XX-XX-FG-R-0009_S3_P01.2



W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.7
Peat Depth Survey Results

October 2022

265000

601000

Alwhat Burn

Glede Craig

Hawks Craig

Waterfalls

505

575

550

Ew

0.40m 0.90m 1.10m 0.58m 0.27m 1.00m 0.95m 1.19m 0.64m 2.11m 0.35m 1.70m 1.80m 1.10m 0.10m 0.41m 1.17m 0.65m 1.10m 0.90m 0.60m 0.80m 0.60m 0.85m 1.40m 0.30m 0.24m 1.20m 0.90m 1.55m 0.70m 0.80m 0.95m 1.60m 1.80m 0.36m 0.66m 0.75m 0.97m 0.94m 1.42m 1.02m 0.95m 1.28m 1.50m 0.30m 1.48m 1.20m 0.90m 0.85m 1.41m 0.26m 1.11m 1.39m 0.67m 1.40m 0.50m 0.64m 1.59m 0.57m 0.46m 1.52m 1.80m 1.10m 1.60m 0.80m 0.10m 1.12m 1.90m 0.80m 1.02m 0.95m 0.90m 0.94m 1.18m 1.13m 0.94m 1.17m 0.87m 0.57m 0.71m 0.41m 1.59m 0.28m 0.65m 1.37m 0.57m 0.19m 0.37m 0.51m 0.64m 0.97m 0.00m 1.21m 0.15m 0.45m 1.08m 0.80m 0.03m 0.98m 0.22m 0.18m 0.89m 1.50m 0.14m 0.22m 0.38m 0.32m 0.67m 0.80m 0.40m 0.41m 0.00m 0.00m 0.00m

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

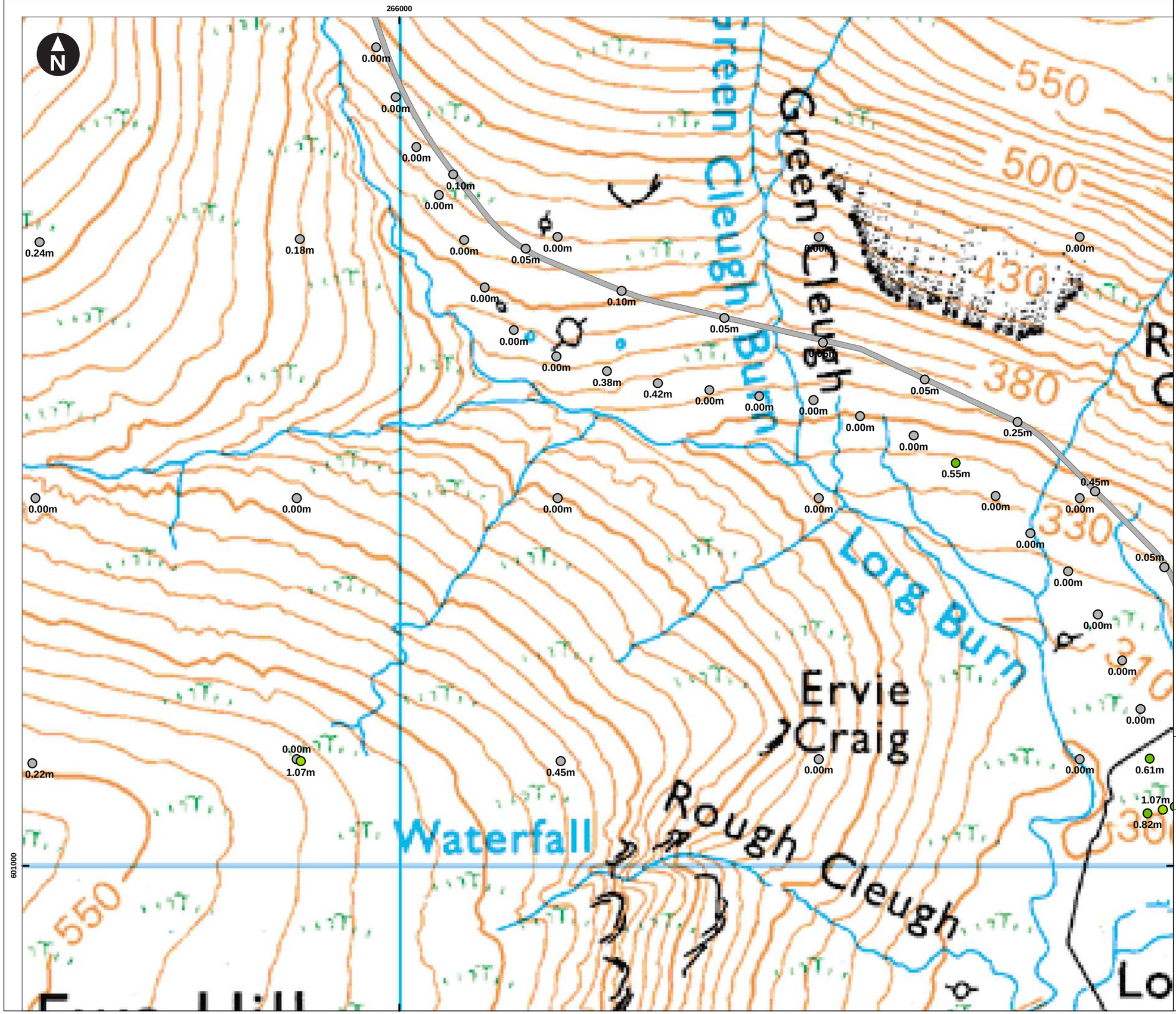
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.8
Peat Depth Survey Results

October 2022

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira



Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.9
Peat Depth Survey Results

October 2022

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

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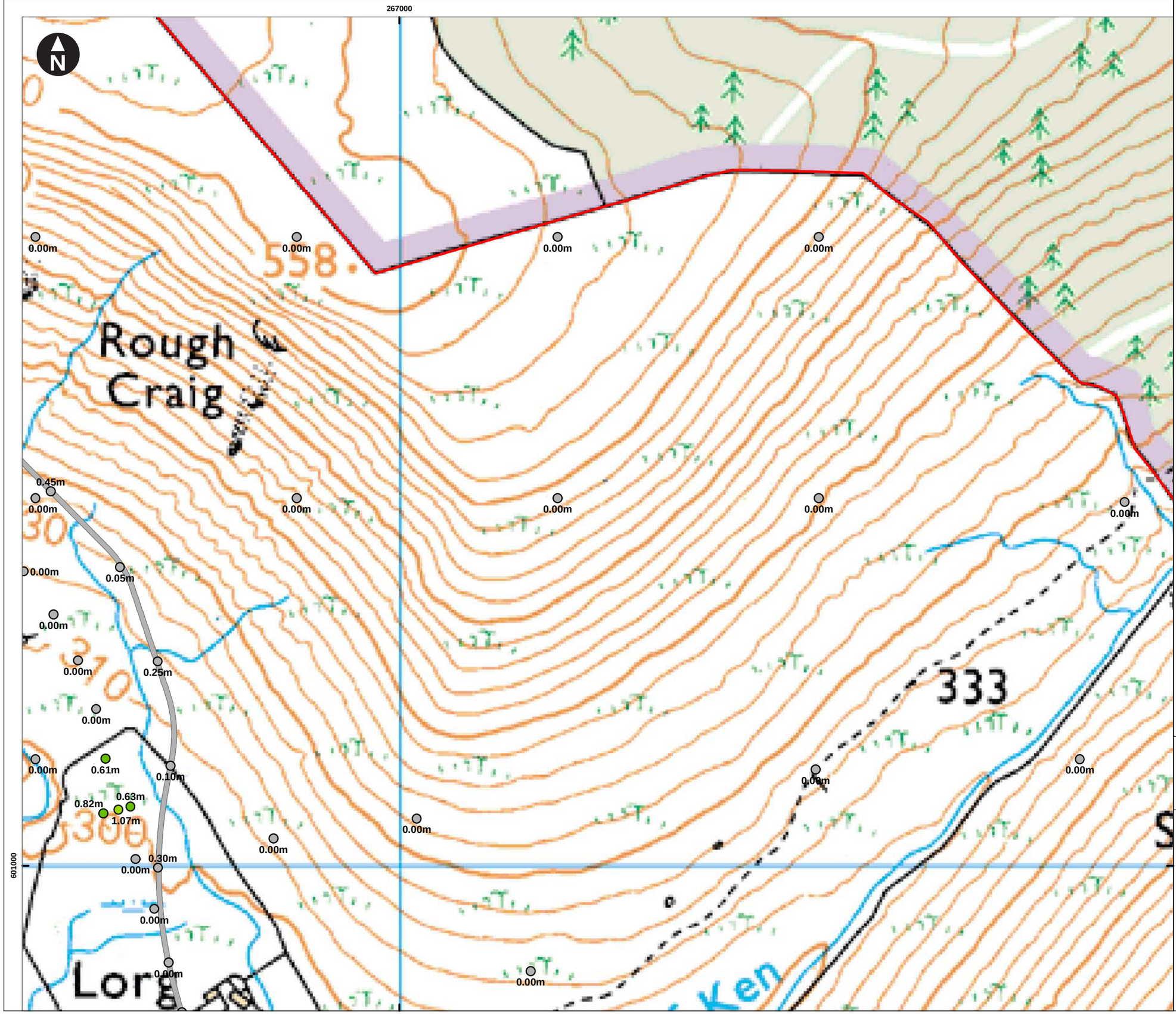
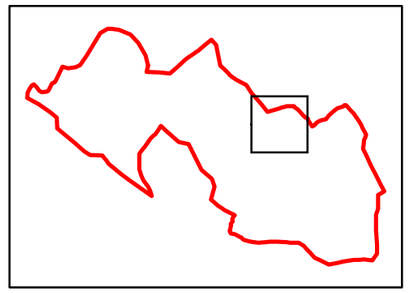


Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0



0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.10
Peat Depth Survey Results

October 2022

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira

268000

601000

Sour Snout

344

370

350

400

420

440

460

Pulmu

0.00m 0.60m 0.15m 0.40m 0.45m 0.85m 0.40m 0.25m 0.90m

0.45m 0.05m 0.35m 0.90m 0.81m 2.71m

0.70m 0.95m 0.25m 0.30m 0.53m

0.00m 0.00m 0.00m 0.36m

0.75m 0.50m 0.85m 0.20m 1.40m 1.03m 0.84m

0.60m 0.55m 0.95m 0.35m 1.01m 0.19m 0.59m

0.58m 1.18m 0.70m 0.46m 0.69m 0.50m 0.96m 0.25m 0.94m 0.27m 0.96m 0.40m 0.50m 0.41m 0.50m 0.83m 0.46m 0.77m 1.52m 1.50m 1.00m 1.00m 1.05m 1.01m 0.43m 0.82m 1.88m 0.53m 1.27m 1.46m 1.26m 1.60m 1.70m 2.00m 1.46m 1.48m 1.64m 2.20m 2.10m 1.50m 1.48m 0.60m

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.11
Peat Depth Survey Results

October 2022

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

266000

267000

600000

N

Glede Craig

Lorg Bridge

286

Long Craig

Craigfad

Sheepfolds

66

67

290

280

210

0.00m

0.11m

0.29m

0.70m

0.40m

0.15m

0.10m

0.42m

0.50m

0.30m

0.41m

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.12
Peat Depth Survey Results

October 2022

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira

267000

268000

600000

Water

Altry Loch

Altry Hill

Mid Height

Whigs' Hole

Cogstewart

350

400

440

460

480

489

N

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.13
Peat Depth Survey Results

wsp

October 2022

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

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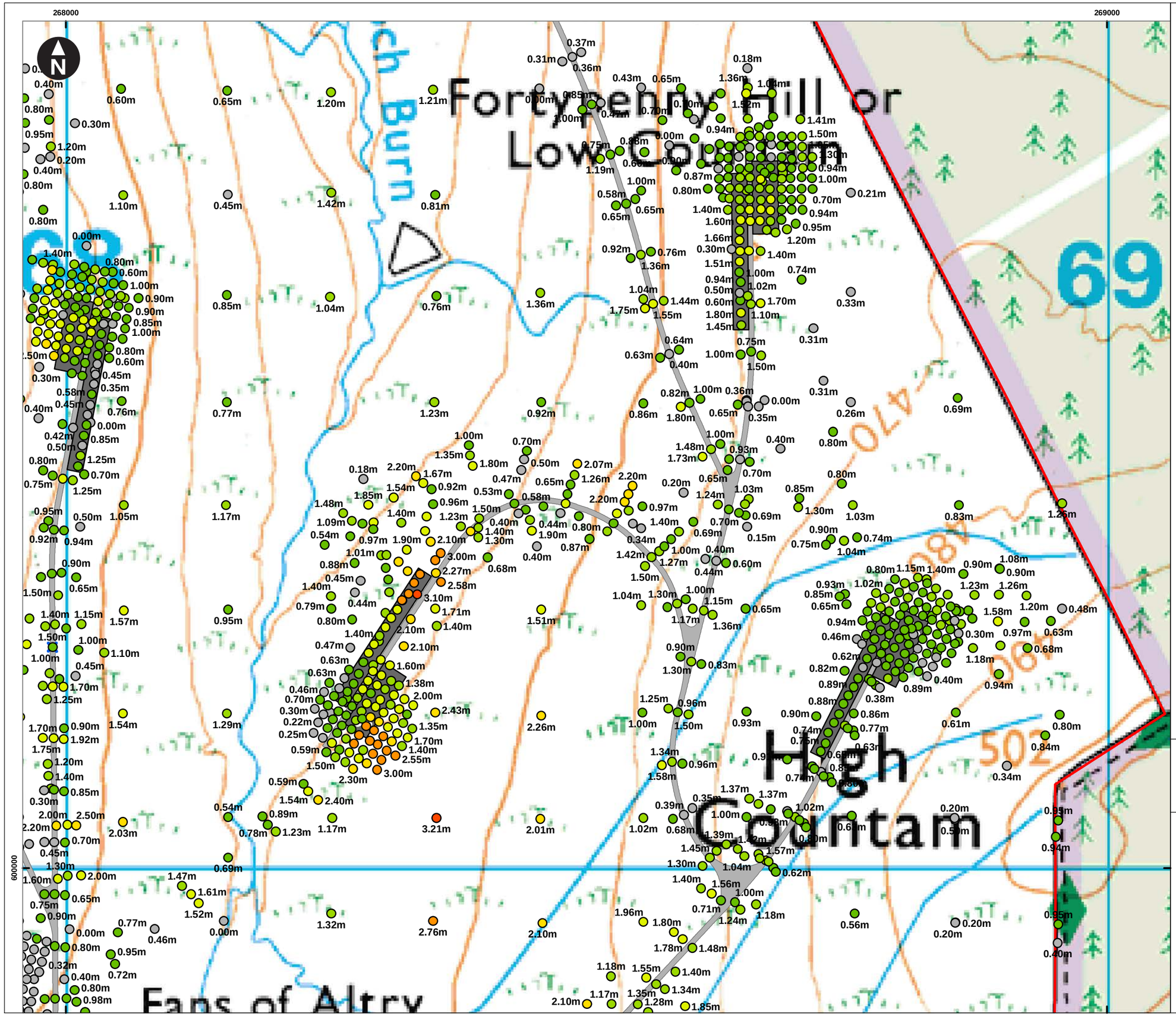


Client

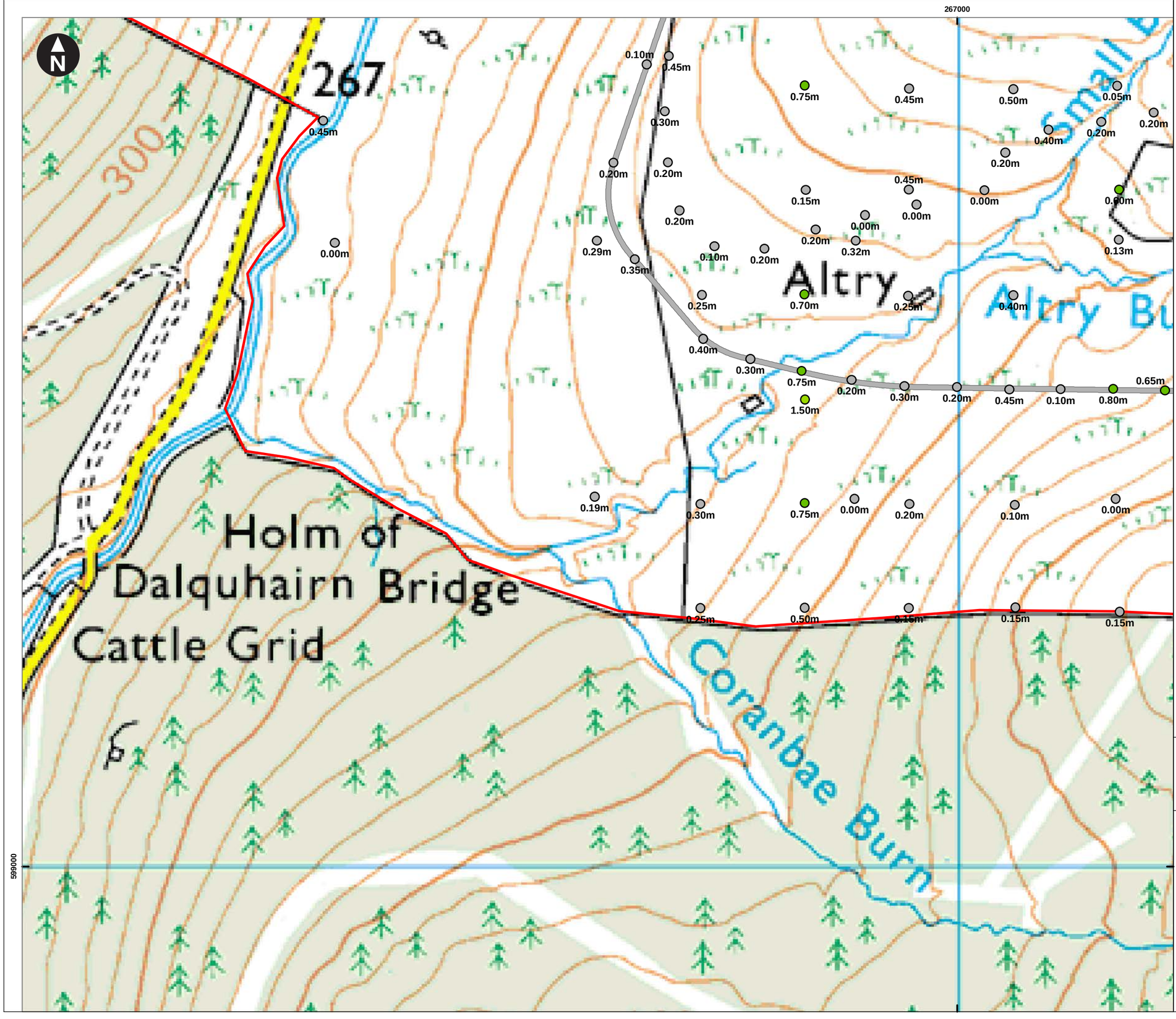
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.14
Peat Depth Survey Results

October 2022

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira



Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Access tracks
- Substation
- Borrow pit

Peat Depth (m)

- 0.0 - 0.5
- 0.5 - 1.0
- 1.0 - 1.5
- 1.5 - 2.0
- 2.0 - 2.5
- 2.5 - 3.0
- 3.0 - 3.5
- 3.5 - 4.0

0 100 200 m

Scale at A3: 1:3,500

Client

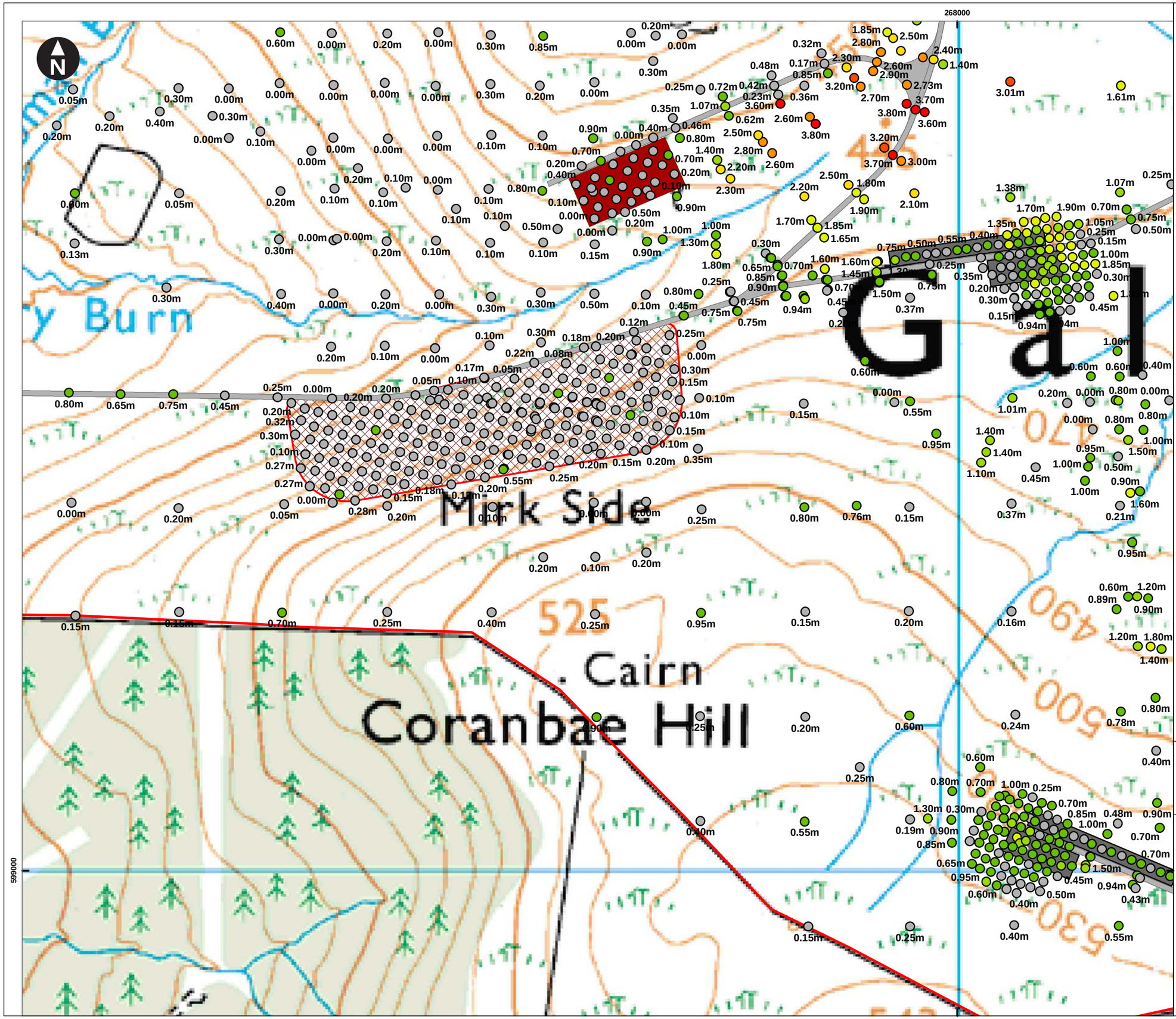
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.15
Peat Depth Survey Results

October 2022

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira



Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.16
Peat Depth Survey Results

October 2022

wsp

32964-WOOD-XX-XX-FG-R-0009_S3_P01.2

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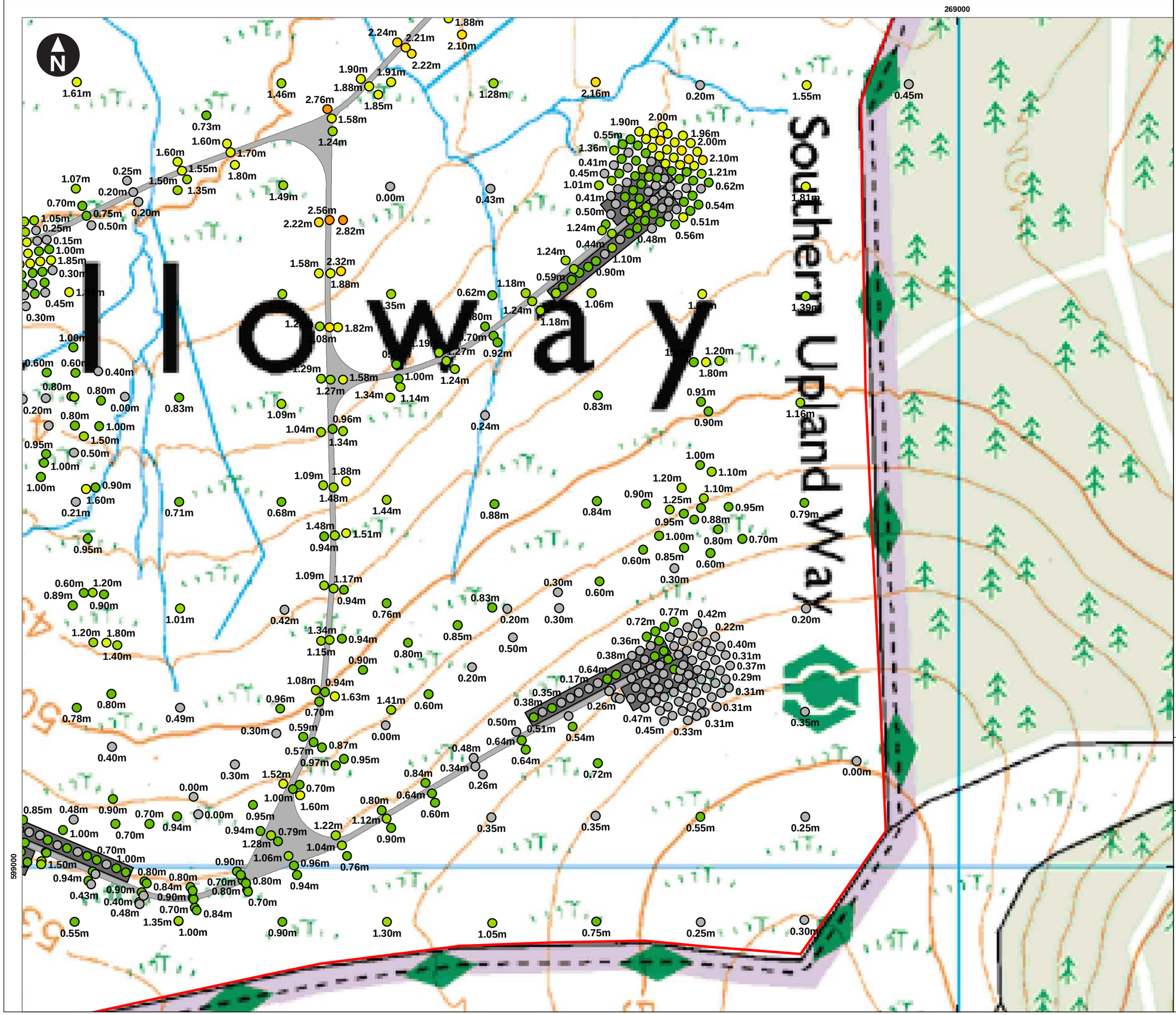


Client

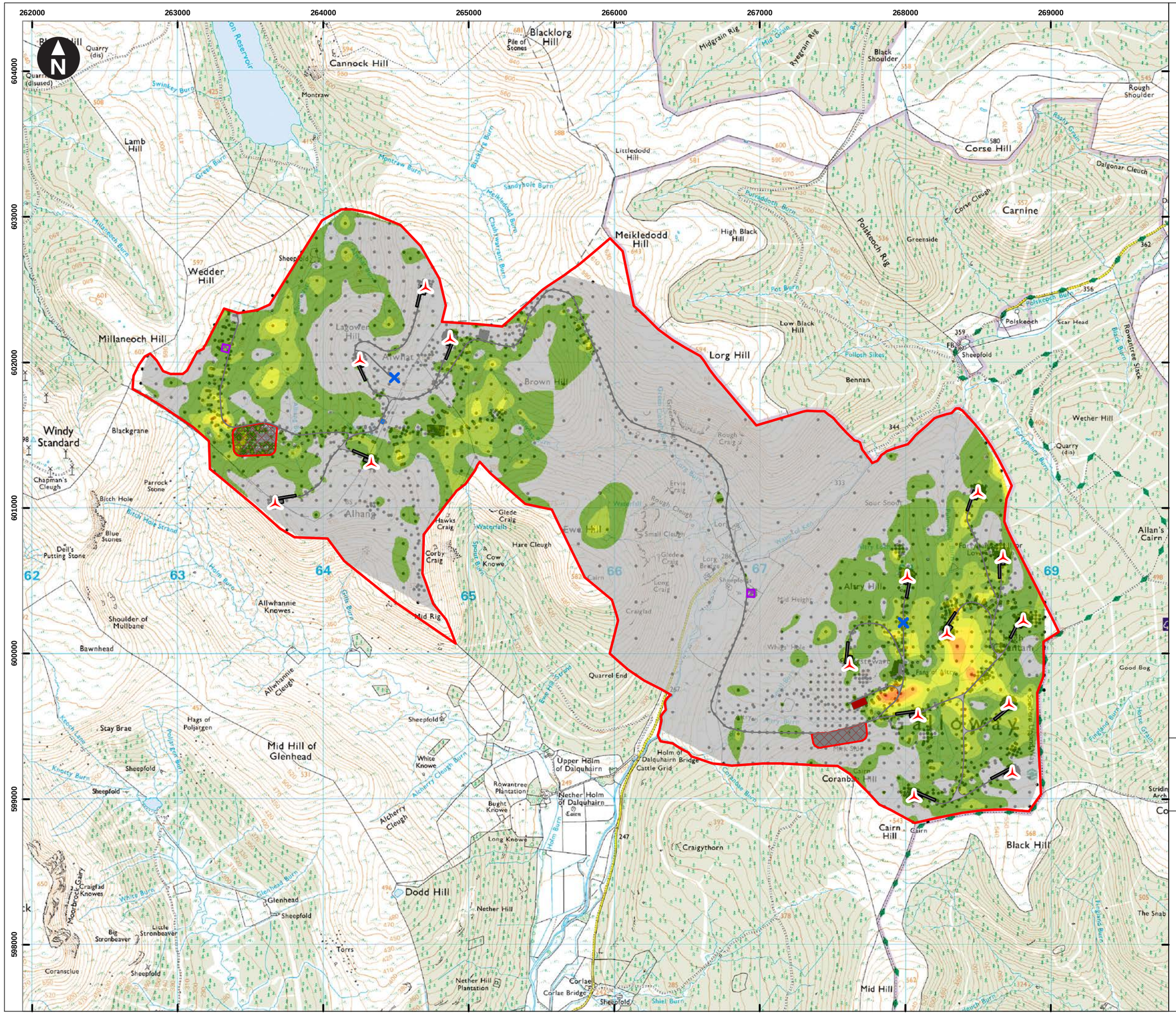
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 9.17
Peat Depth Survey Results

October 2022

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\PSRA\32964-WOOD-XX-XX-FG-R-0009_S3_P01.2 Originator: benjamin.amaira



Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 10
Interpolated Peat Depth Map

October 2022

263000
264000
265000
603000
602000
601000

Wedder Hill
Sheepfold
Afton Water
Alwhat Burn
Meikledodd Burn
Clashywarrant Burn
Lagower Hill
Alwhat
Brown Hill
Alhang
Alhang Burn
Source of the Afton
Hawks Craig
Glede Craig
Waterfalls
Corby Craig
Spout Burn
Cow Knowe
Hare Cleugh
Ewe Hill
Cairn
Allwhannie
grane
eoch Hill

TN-25
TN-26
TN-12
TN-11
TN-67
TN-16
TN-19
TN-66
P8
P9
P10
TN-28
TN-27
TN-68
TN-65
TN-64
TN-29
TN-62
TN-30
P6
P7
TN-63
TN-61
TN-32
TN-33
TN-34
TN-31
TN-39
TN-40
TN-43
TN-42
TN-41
TN-44
TN-45
TN-46
TN-36
TN-35

Geomorphic features

- Peat Pipe
- Peat Pipe (collapse)
- Peat Pipe (outfall)
- Peat Pipe (possible)
- Peat Pipe (sinks)
- Spring
- Gully
- Peat pipe
- Possible pipe
- Scarp
- Concave slope break
- Convex slope break
- Bedrock Outcrops
- Debris Fans
- Peaty-debris Slide
- Pools
- Flush
- Peat hagging
- Peat gripping
- Landslide
- Landslide (oversteepening)
- Peatslide
- Possible Relic Peatslide
- Relic Peatslide
- Scree
- Public imagery locations
- Target Notes

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

0 100 200 300 400 500 600 m

Scale at A3: 1:10,560

Client

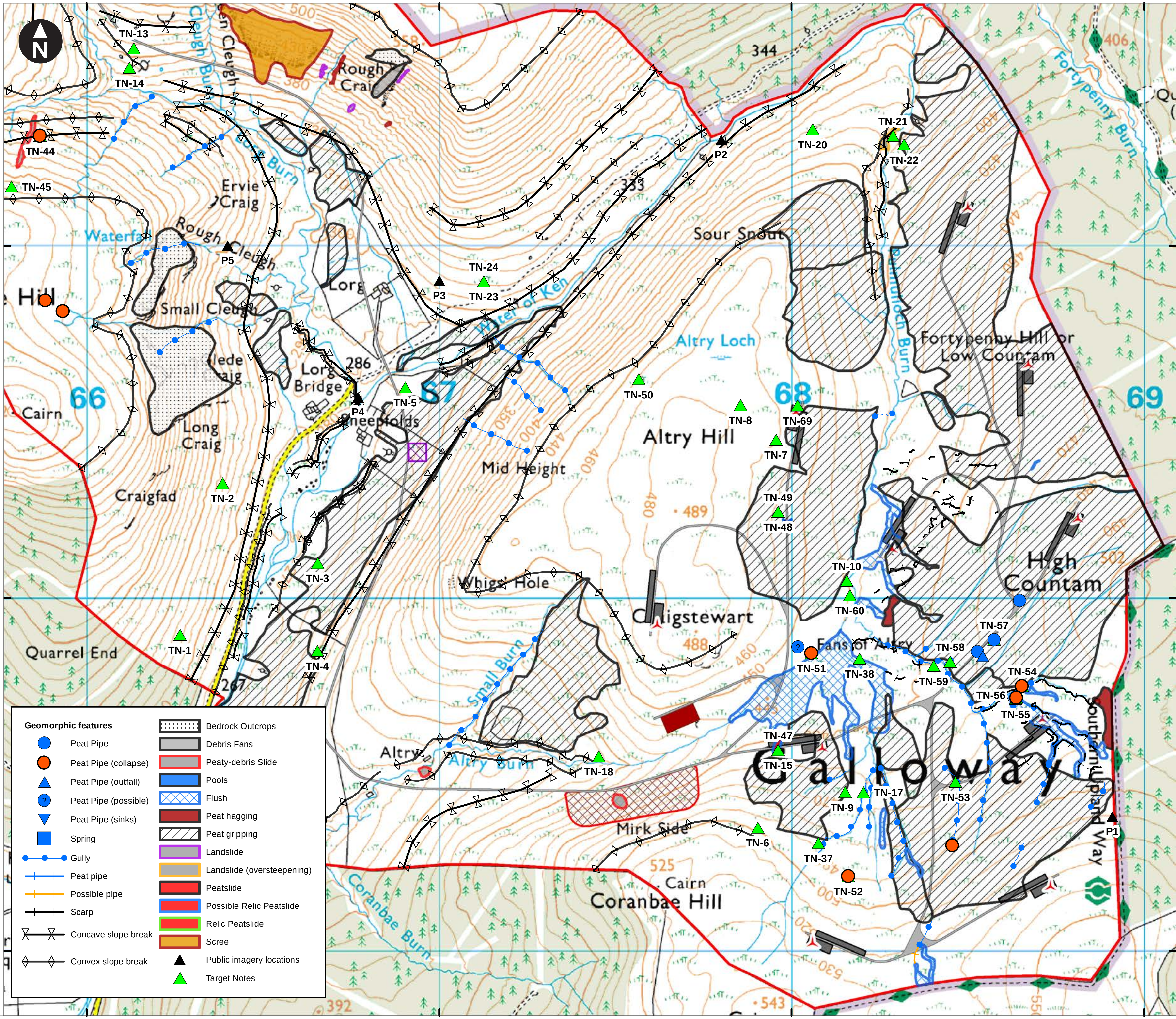
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 11.0
Geomorphology

November 2022

wsp



Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

0 100 200 300 400 500 600 m

Scale at A3: 1:10,560

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

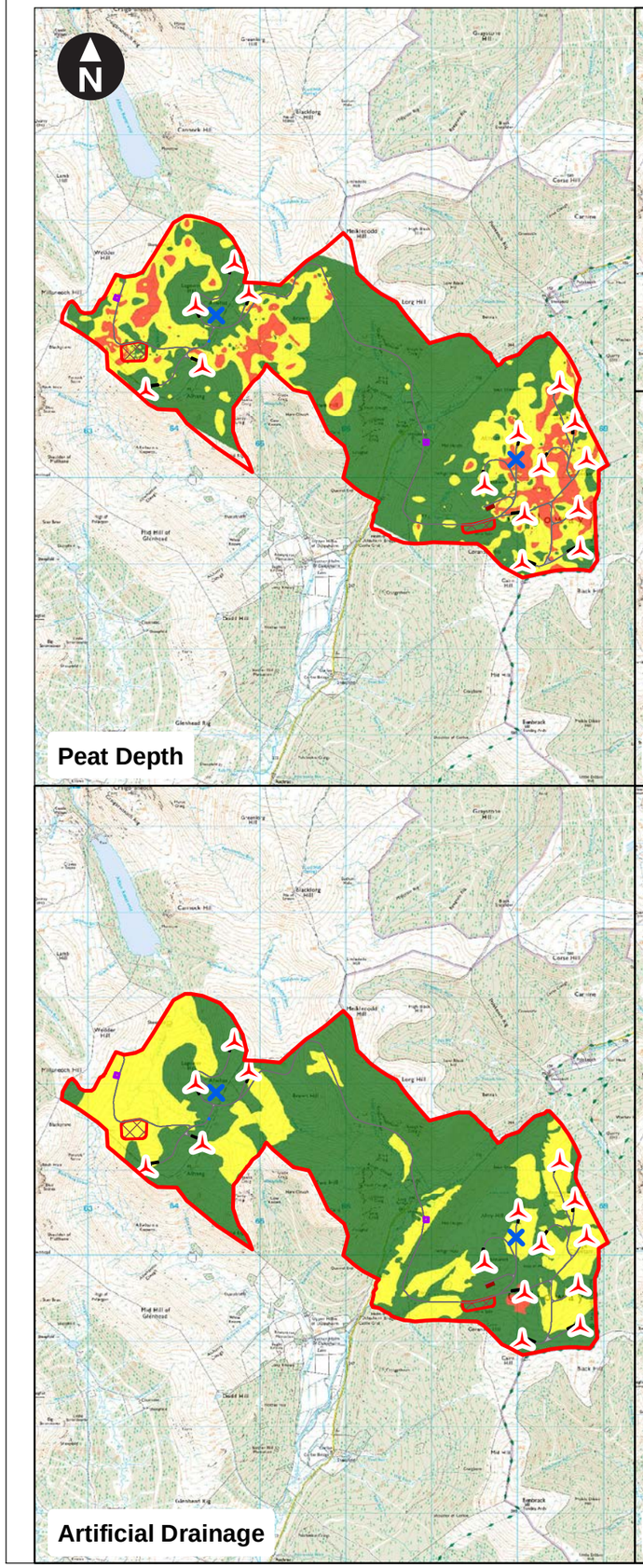
Figure 11.1
Geomorphology

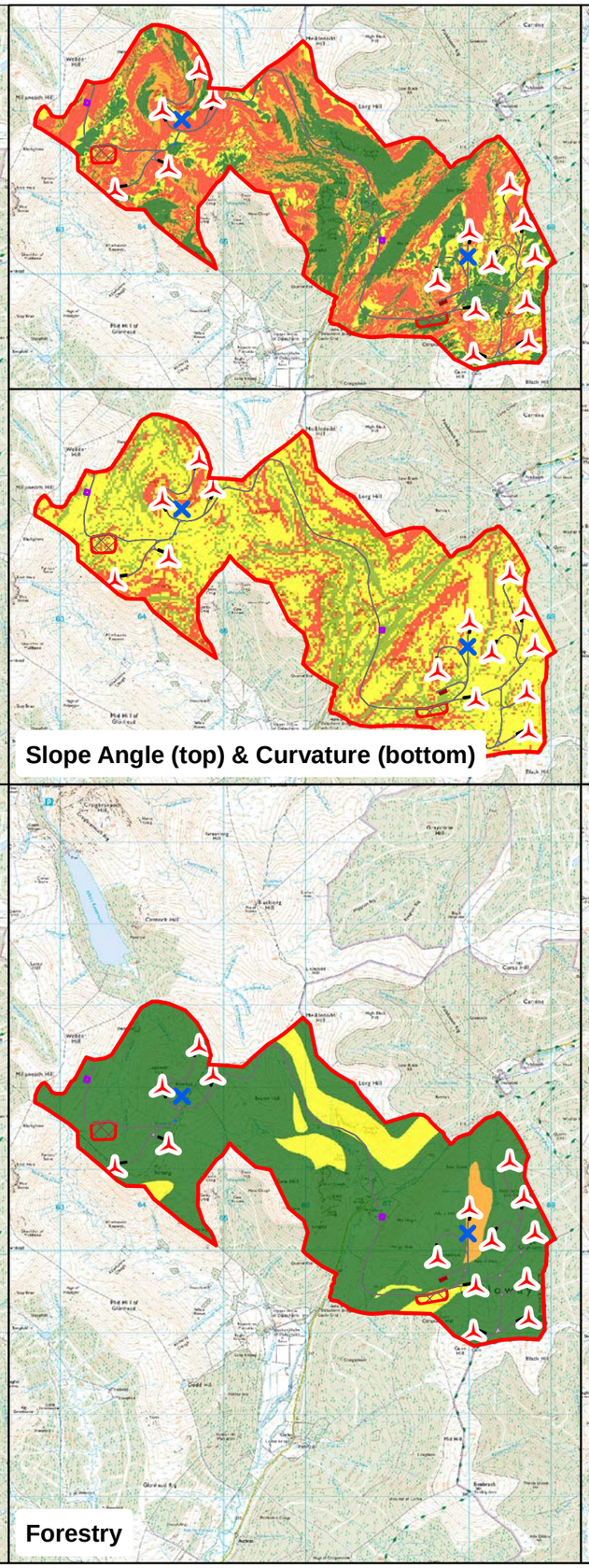
November 2022

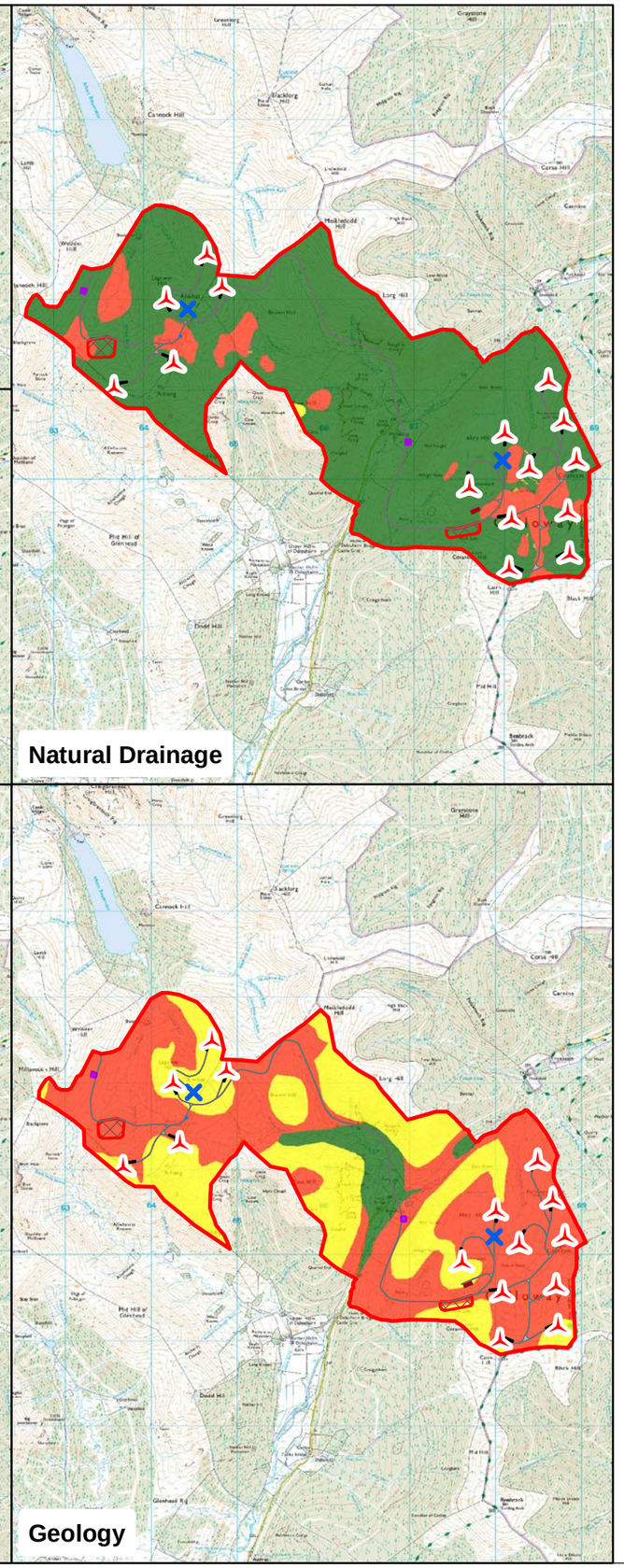
wsp

W:\32964 Afton II Sub Folder\D040 Design\Drawings\ArcGIS\MXD\P01\32964-WOOD-XX-XX-FG-R-0011_S3_P01.2 Originator: benjamin.amaira

32964-WOOD-XX-XX-FG-R-0011_S3_P01.2







Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

Significance of the Hazard

- 1 (Insignificant)
- 2 (Significant)
- 3 (Substantial)
- 4 (Serious)
- 5 (Extremely Serious)

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 12.0
Peat Slide Hazard Scores

wsp

October 2022

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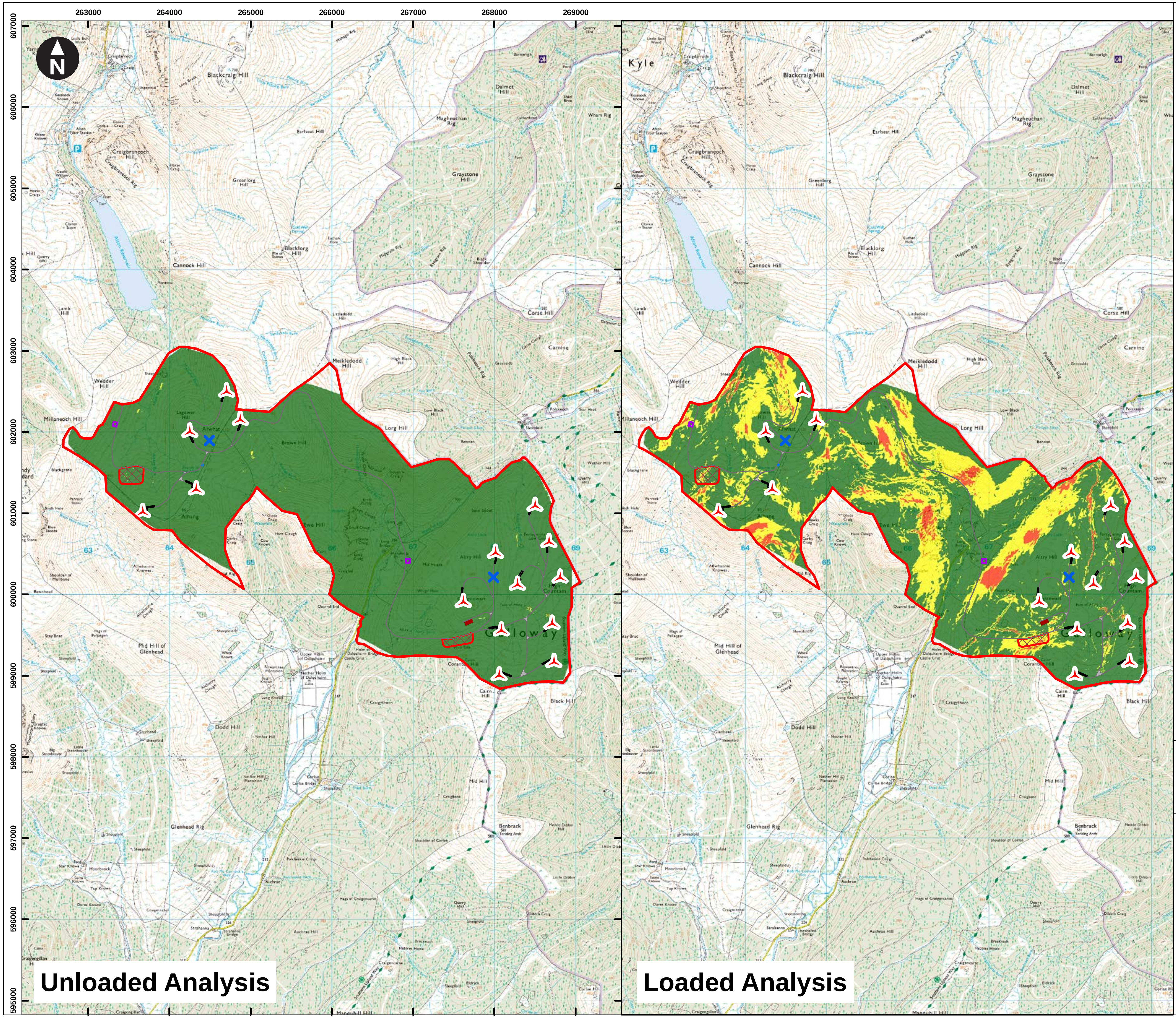


Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

Factor of Safety

- < 1
- 1 - 1.4
- >1.4

0 0.25 0.5 0.75 1 1.25 1.5 1.75 2 2.25 Kilometers

Scale at A3: 1:45,000

Client

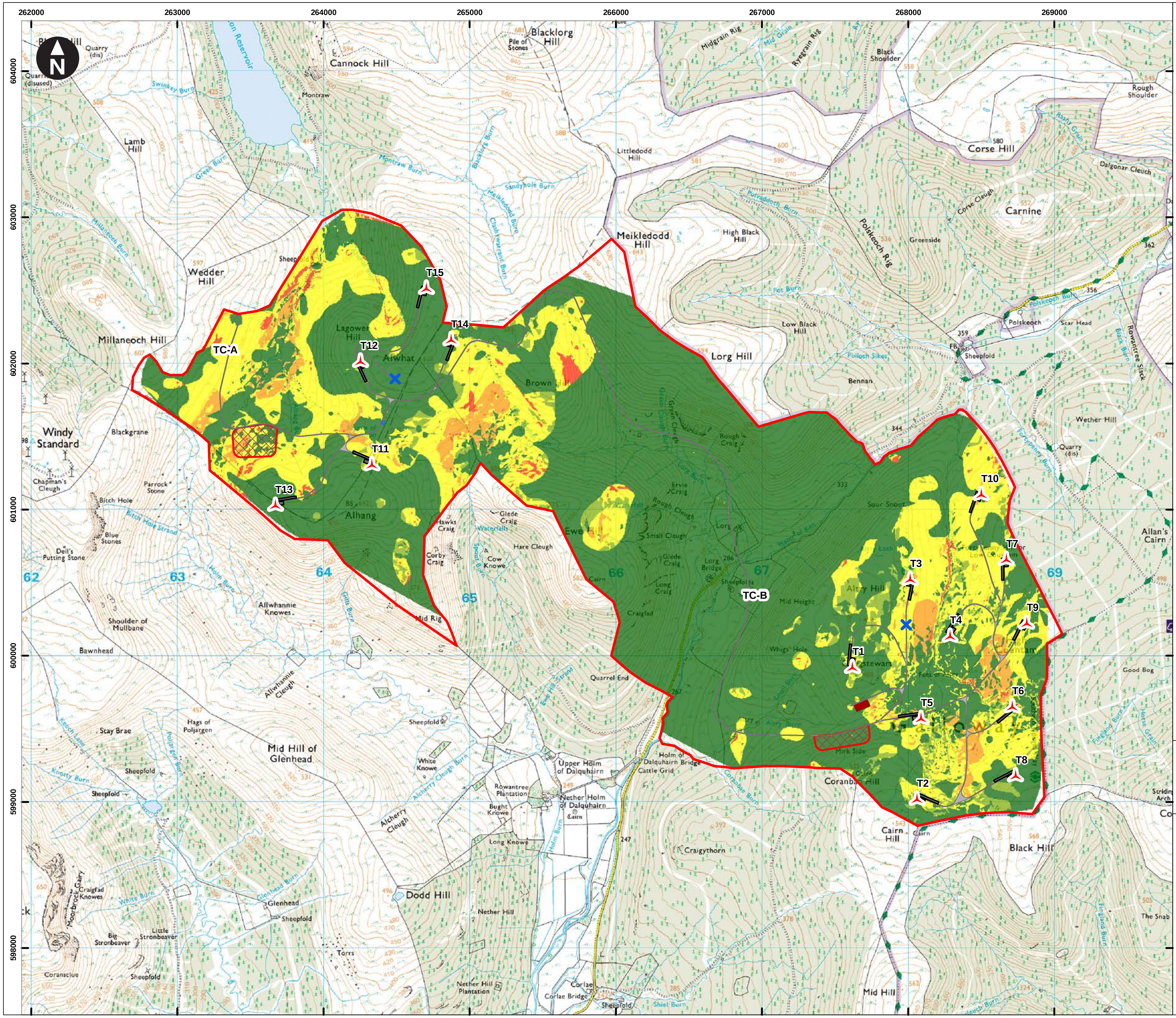
RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 13.0
Infinite Slope Analysis

October 2022

wsp



Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

Peat Slide Likelihood

- 1 (Negligible)
- 2 (Unlikely)
- 3 (Likely)
- 4 (Probable)
- 5 (Almost Certain)

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 14.0
Peat Slide Likelihood

October 2022

wsp

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262000 263000 264000 265000 266000 267000 268000 269000

604000 603000 602000 601000 600000 599000 598000

T1 T2 T3 T4 T5 T6 T7 T8 T9 T10 T11 T12 T13 T14 T15 TC-A TC-B

Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit
- Private water supplies
- Surface water courses
- GWDTEs

Peat Slide Likelihood

- 1 (Very Low)
- 2 (Low)
- 3 (Moderate)
- 4 (High)
- 5 (Very High)

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

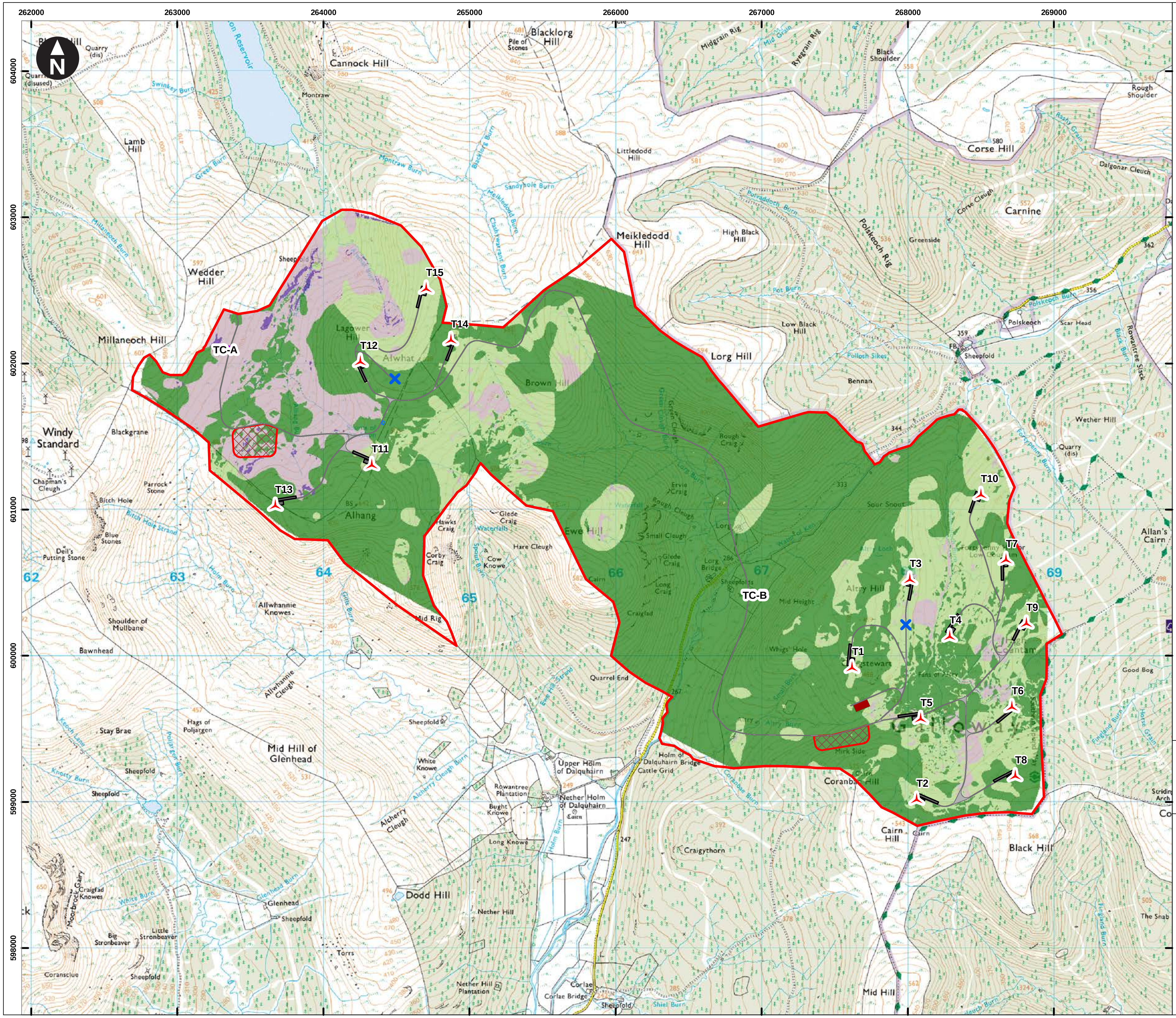
Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 15.0
Peat Landslide Consequences

October 2022



Key

- Development Site boundary
- Turbine location
- Met mast location
- Western control building
- Crane pads
- Temporary compound
- Access tracks
- Substation
- Borrow pit

Peat Landslide Risk

- Negligible
- Low
- Moderate
- High

0 0.25 0.5 0.75 1 1.25 Kilometers

Scale at A3: 1:25,000

Client

RWE

Lorg Wind Farm
Peat Landslide Risk Assessment

Figure 16.0
Peat Landslide Risk Assessment

October 2022

wsp

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32964-WOOD-XX-XX-FG-R-0016_S3_P01.2

Appendix B
Target Notes

Target Note	Description	Photographs
001	Looking northeast towards Lorg Farmhouse along the line of the 'U' shaped valley with Lorg Hill in the distance. Note the predominance of grasses in this area.	
002	Looking north from adjacent to the current access road along the lower eastern slope of Ewe Hill.	
003	Looking generally north along the lower western side of Altry Hill where the Spine road will pass through. Note the predominance of mineral soils in this area.	

Target Note	Description	Photographs
004	Looking northeast up towards Altry Hill from the Water of Ken.	
005	Looking generally west from the eastern side of the Water of Ken towards Ewe Hill. Note the Hummocky Glacial Deposits exposed by the Water of Ken in the mid-ground.	

Target Note	Description	Photographs
006	Looking generally north from the mid slope of Coranbae Hill towards Fortypenny Hill in the distance and the proposed location of the Eastern Turbine Array.	
007	Looking generally east from Altry Hill towards High Countam and the proposed location of the Eastern Array. Note the peat faces on the right side of the image.	
008	Looking generally north across the summit of Altry Hill towards Sour Snout. Note the dominance of grasses with some mosses which indicate the presence of shallow peat.	

Target Note	Description	Photographs
009	Looking generally north from the foot of Coranbae Hill over Fans of Altry.	
010	Looking north along the bottom of the basin in the southeast of the site and along the Pulmulloch Burn. Note the steep sided banks of the burn which continue to steepen downstream towards the Water of Ken confluence.	
011	Looking generally southeast from Alhang towards a large relic rotational landslide on the western slope of Mid Rig. Note the presence of well-defined flanks, flat lying heads and hummocky ground at the toe.	

Target Note	Description	Photographs
012	Looking generally northwest from the northern slope of Alhang towards Windy Standard Wind Farm and the proposed route of the access road from Afton Wind Farm.	
013	Looking generally west from the steep valley sides of the Lorg Burn towards the confluence with the Alwhat Burn. Note the steepness of valley sides which would confine any peatslides. In addition, also note the translational possible peaty-debris slide towards the central top of the image.	
014	A possible peaty-debris slide on the lower steep slope of Ewe Hill near the confluence of Alwhat Burn and Lorg Burn. Access to confirm the failure as a peaty-debris slide was not possible due to the steepness of the slope.	

Target Note	Description	Photographs
015	Looking generally southeast from the lower ground at Fans of Altry towards Black Hill.	
016	Looking generally northwest from Mid Rig towards the very steep southern slope of Alhang.	
017	'V' shaped gully erosion of the peat and substrate located to the east of T11.	

Target Note	Description	Photographs
018	Looking in a downstream direction along the Altry Burn. Note the very steep sided valley sides of the burn.	
019	Looking generally north along the very steep eastern slope of Mid Rig showing Corby Craig.	
020	A substrate exposure on the northern slope of Sour Snout.	

Target Note	Description	Photographs
021	A slope failure of the superficial deposits located on the outside of a meander of the Pulmulloch Burn. Note the dominance of granular deposits.	
022	Slope failures caused by oversteepening of the slope on the outside of meanders on the Pulmulloch Burn.	
023	Looking generally southeast from the low slopes of Lorg Hill towards Altry Hill. Note the presence of some shallow slope failures near the top of the slope.	

Target Note	Description	Photographs
024	Looking generally west from the low slope of Lorg Hill towards Ewe Hill, showing Rough Cleugh, Small Cleugh, Glede Craig, Ervie Craig and Long Craig.	
025	Looking generally southeast from the toe of the slope on the eastern slope of Millaneoch Hill towards the route of the Spine road as it passes between Alhang and Alwhat.	
026	A flush feature located in the low ground between Alhang and Millaneoch Hill adjacent to the route of the Spine road.	

Target Note	Description	Photographs
027	Looking generally northeast from Alhang towards Alwhat showing the bog pools in the col between the hills.	
028	Looking generally south from the col between Alhang and Alwhat towards Alhang.	
029	Looking generally southeast from the summit of Alwhat towards Ewe Hill over a section of the Western Turbine Array area.	

Target Note	Description	Photographs
030	An exposure of the peat and substrate on Alwhat. Note the dominance of granular deposits or weathered bedrock.	
031	A 'V' shaped gully on the upper reaches of the Alwhat Burn.	
032	A large flush feature (extending behind and to the right of the image) located adjacent to the south of the T5 spur road.	

Target Note	Description	Photographs
033	A large peat hagg located adjacent to the south of T5 spur road.	
034	A large flush feature at the source of the Alwhat Burn. Note the peat exposures on the left.	
035	The back scar of a possible peaty-debris slide on the steep mid-slope of Meikledodd Hill upslope of the Spine road.	

Target Note	Description	Photographs
036	Looking across the possible peaty-debris slide on Meikledodd Hill.	
037	A series of peat pipe collapses extended downslope located between T8 and T11.	
038	Part of a large flush feature forming the Fans of Altry and the source of the Pulmulloch Burn.	

Target Note	Description	Photographs
039	Looking generally west from the low slope of Brown Hill towards the bottom of the basin between Brown Hill, Alwhat and Alhang.	
040	An exposure of the substrate on the Alwhat Burn. Note the dominance of course granular deposits and an irregular interface.	
041	A large peat pipe collapse on a tributary of the Alwhat Burn.	

Target Note	Description	Photographs
042	Peat piping along a tributary of the Alwhat Burn.	
043	An exposure of the bedrock substrate on the low northern slope of Ewe Hill.	
044	A peat pipe collapse on the northern slope of Ewe Hill.	

Target Note	Description	Photographs
045	Looking northward down towards a translational failure on the northern slope of Ewe Hill, situated within a potentially larger relic failure.	
046	A translational debris slide situated on the steep valley side of the Lorg Burn on Brown Hill.	
047	Potential slope creep on the lower slope of Coranbae Hill.	

Target Note	Description	Photographs
048	Possible tension cracking on the mid-slope of Altry Hill slightly upslope of the T9 spur road.	
049	Possible tension cracking slightly upslope of the T9 spur road denoted by the line of rushes.	
050	A peat-debris slide located on the upper western slope of Altry Hill.	

Target Note	Description	Photographs
051	A peat pipe collapse in the Fans of Altry area.	
052	A peat pipe collapse adjacent to the west of the proposed T14 spur road on the slope of Coranbae Hill.	
053	A 'V' shaped gully on the lower slope of Black Hill.	

Target Note	Description	Photographs
054	Gullying of the peat on the col between High Countam and Black Hill to the southeast of T12.	
055	Gullying and slumping of deep peat on the col between High Countam and Black Hill to the southeast of T12.	
056	Gullying and slumping of deep peat on the col between High Countam and Black Hill to the southeast of T12. Note the substrate which comprises bedrock and granular deposits.	

Target Note	Description	Photographs
057	An example of a moss filled grip adjacent to the proposed location of T12.	
058	Headward gullying of a peat grip outfall to the southwest of T12.	
059	An exposure of the peat substrate on the outside of a meander. Note the presence of clayey deposits with a significant granular content.	

Target Note	Description	Photographs
060	A flush feature at Fans of Altry.	
061	A peat pipe outfall to the north of the T5 spur road.	
062	A flush feature located to the east of T4.	

Target Note	Description	Photographs
063	Peat piping to the east of the Control Building and SPEN substation compound.	
064	Peat pipe sink on the outside of a meander in the Spout Burn taking all flows from the stream through the pipe to an outfall on the downstream side of the meander.	
065	A peat flush at the source of the Spout Burn.	

Target Note	Description	Photographs
066	An exposure on the western slope of Mid Rig showing weathered bedrock.	
067	A bog pool located between Mid Rig and Alhang.	
068	A peat flush at the source of the Spout Burn adjacent to the T3 spur road.	

Target Note	Description	Photographs
069	Peat pipe (exposed by collapse under the weight of the surveyor) and a possible tension crack. Note, the sink was identified slightly up slope.	

Appendix C
Project Team

Ben Amaira, BSc (Hons), FGS – author

Ben has over 13 years' experience in the environmental consultancy sector specialising in contaminated land and peat land slide risk assessment. Ben has significant experience of supporting and advising clients in the renewable sector on the peat slide risks and peat management. This includes significant experience in the planning and undertaking of Phase 1 and 2 peat surveys for a range of small and large scale wind farms as well as advising clients on their wind farm layouts. Ben's skills also include the identification and mapping of upland geomorphology including a wide range of incipient and relic peat slide features.

Richard Bagnall, BEng (Hons) – technical reviewer

Richard is a qualified Civil Engineer with over 14 years postgraduate experience as a geotechnical engineer. He has been involved in a number of high-profile jobs from conception through to construction. His routine work includes the design and management of strategic geotechnical infrastructure including at numerous wind farm sites throughout the United Kingdom. Richard regularly manages Phase 1 and 2 peatland surveys and undertakes peat slide risk assessments for planning applications in accordance with Scottish Government Best Practice including the geomorphological mapping of sites to identify evidence of any relic peat slide features. Additionally, Richard provides design advice on wind farm layouts and micro-siting of turbines to alleviate site constraints prior to design freeze.

Graeme Smart, BEng (Hons), MICE, CEng – technical approver

Graeme is a chartered civil engineer with over 30 years of consultancy experience specialising in geotechnical engineering. Graeme has significant experience across a number of sectors including renewables and has successfully led the Geotechnical Team enabling timely delivery and ensuring technical quality of many peat landslide risk assessments for numerous windfarms across the UK. Due to Graeme's experience in this sector he is often asked to review contractors wind turbine foundation proposals, on behalf of clients, to identify any potential issues with design and/or construction. This frequently necessitates a good understanding of the interaction of construction processes/materials and peat.

Appendix D
Peat Depth Data

Easting	Northing	Peat Depth (m)
262858.83	601950.83	0.3
262799.66	602040.57	0.1
262763.67	601951.06	0.25
262752.22	601854.17	0.5
262855.05	601850.13	0.4
262847.38	601767.32	0.6
262951.18	601657.12	0
262960.16	601759.56	0.25
262960.29	601858.09	0.65
263050.35	601851.70	0.5
263055.29	601754.70	0.3
263052.65	601652.73	0.9
263153.11	601558.91	1.5
263154.30	601658.03	0.9
263152.63	601752.33	1
263154.56	601855.71	0.65
263154.92	601954.63	0.15
263154.32	602061.89	0.4
263259.32	602147.99	0.5
263258.17	602254.55	0.95
263348.56	602352.61	1.15
263358.03	602251.46	0.7
263353.06	602153.13	1
263359.07	602048.52	0.9
263355.10	601951.79	0.95
263351.51	601854.78	1
263257.84	601851.23	1
263254.60	601756.66	1.8
263257.19	601658.20	1.95
263350.35	601649.90	1
263361.41	601753.15	0.4
263459.80	601654.69	0.6
263463.96	601755.55	0
263456.75	601857.34	0.85
263460.35	601956.78	0.6
263450.84	602053.65	1.1
263449.92	602158.58	0.6
263459.47	602261.73	0.6
263456.32	602351.27	0.8
263549.36	602356.69	0.5
263556.10	602252.78	0.9
263558.30	602149.65	1
263552.59	602052.60	0
263554.34	601953.51	1
263551.75	601846.68	1.35
263555.11	601758.49	1.05
263556.30	601655.29	0
264057.61	602254.59	0.2
264055.87	602355.39	0.2

Easting	Northing	Peat Depth (m)
263651.24	601754.02	0.9
263649.81	601862.23	2.1
263649.45	601955.70	1.55
263653.53	602053.91	0.4
263659.76	602154.15	0.95
263658.55	602248.99	2.35
263651.83	602355.33	0.5
263655.16	602455.10	0.1
263756.43	602548.36	0.9
263762.06	602444.32	1.35
263753.95	602357.97	1.5
263753.35	602256.18	1.5
263759.77	602155.05	1.3
263752.13	602059.79	1.4
263759.93	601951.03	1.4
263759.71	601852.94	0.6
263753.73	601759.58	0.2
263759.32	601662.50	0
263854.00	601651.64	0
263852.51	601756.35	0.9
263857.51	601857.08	0.6
263856.76	601958.33	0.85
263861.32	602049.80	1
263860.19	602154.63	0.6
263853.35	602255.94	0.9
263856.21	602355.26	0.3
263855.90	602451.94	0.3
263854.80	602553.39	0.9
263854.85	602650.55	0.8
263857.20	602753.82	0.7
263956.73	602851.58	1
263957.99	602762.52	0.9
263954.32	602655.47	0.3
263959.80	602559.06	1.45
263955.52	602454.90	1
263953.78	602360.35	0.8
263959.41	602249.22	0.3
263955.89	602149.20	0.1
263956.21	602051.86	0.3
263956.67	601949.00	0.5
263957.14	601849.22	0.6
263956.26	601755.09	1.1
263954.56	601655.51	0.65
264055.82	601751.84	0.7
264055.13	601855.37	0
264055.62	601958.85	0.2
264060.92	602054.78	0.1
264060.12	602155.90	0
264061.16	602453.32	0.8

Easting	Northing	Peat Depth (m)
264065.54	602757.02	0.1
264156.73	602754.22	1.56
264254.65	602753.25	0.43
264353.44	602756.34	0.27
264458.82	602753.48	0.23
264454.39	602850.87	0.16
264459.13	602950.03	0.44
264554.14	602850.97	0.14
264656.15	602751.89	0.72
264755.18	602652.34	0.16
264755.98	602550.42	0.27
264757.35	602453.31	0.18
264757.45	602352.71	0.26
264659.00	602250.30	0.23
264657.03	602351.88	0.47
264655.61	602447.33	0.34
264656.91	602552.15	0.14
264657.24	602652.56	0.35
264601.62	602710.68	0.67
264556.75	602753.08	0.59
264555.34	602651.59	0.42
264555.77	602551.73	0.27
264555.96	602450.75	0.17
264559.78	602350.78	0.36
264558.67	602252.44	0.52
264556.02	602152.11	0.37
264456.57	602151.82	0.22
264356.46	602154.33	0.47
264256.61	602051.60	0.27
264158.51	601954.20	0.52
264157.54	602050.19	0.22
264154.78	602149.76	0.15
264255.93	602150.37	0.24
264157.31	602249.54	0.46
264252.90	602251.43	0.19
264356.65	602250.29	0.78
264454.45	602255.45	1.33
264457.18	602351.33	0.91
264356.83	602352.92	0.24
264260.73	602354.76	0.31
264157.82	602352.16	0.28
264155.22	602453.58	0.37
264253.00	602447.80	0.45
264357.43	602455.35	0.36
264455.61	602452.16	0.55
264455.34	602550.54	0.45
264456.96	602651.64	0.35
264355.82	602651.22	0.1
264358.18	602552.03	0.95

Easting	Northing	Peat Depth (m)
264256.80	602554.22	0.88
264155.81	602551.94	0.42
264256.22	602652.61	1.05
264155.04	602651.07	0.75
264156.90	602849.24	0.3
264256.01	602849.17	0.25
264355.24	602852.99	0.4
264354.76	602951.19	0.2
264255.81	602952.93	0.1
264158.82	603049.45	0.85
264154.66	602952.14	1.5
264054.22	602950.22	0.35
264055.70	602850.13	0.05
264055.76	602652.46	0.75
264055.46	602553.35	0.8
266152.00	602352.00	0
264905.00	602098.00	0.39
265904.00	602096.00	0.39
266152.00	602102.00	0
266402.00	602102.00	0
264903.00	601850.00	0.63
265655.00	601849.00	0.54
265904.00	601847.00	0.21
266152.00	601852.00	0
266402.00	601852.00	0
266652.00	601852.00	0
265656.00	601597.00	0.24
265905.00	601600.00	0.18
266152.00	601602.00	0
266402.00	601602.00	0
266652.00	601602.00	0
266902.00	601602.00	0
267152.00	601602.00	0
267402.00	601602.00	0
268431.00	601622.00	0.25
265652.00	601352.00	0
265902.00	601352.00	0
266152.00	601352.00	0
266402.00	601352.00	0
266652.00	601352.00	0
266902.00	601352.00	0
267152.00	601352.00	0
267402.00	601352.00	0
267695.00	601348.00	0
267902.00	601352.00	0.6
268060.00	601330.00	0.15
268361.00	601338.00	0.45
265409.00	601098.00	0.14
265649.00	601098.00	0.22

Easting	Northing	Peat Depth (m)
265902.00	601102.00	0
265906.00	601100.00	1.07
266155.00	601100.00	0.45
266402.00	601102.00	0
266652.00	601102.00	0
266880.00	601026.00	0
267017.00	601045.00	0
267399.00	601092.00	0
267652.00	601102.00	0
267902.00	601102.00	0
268152.00	601102.00	0
268405.00	601099.00	0.36
265656.00	600847.00	0.41
266152.00	600852.00	0
266438.00	600830.00	0.19
266651.00	600846.00	0.29
266900.00	600815.00	0
267126.00	600899.00	0
267402.00	600852.00	0
267652.00	600852.00	0
267904.00	600847.00	0.79
268157.00	600854.00	0.41
268655.00	600850.00	0.36
265902.00	600602.00	0
266152.00	600602.00	0
266402.00	600602.00	0
266467.00	600670.00	0
266652.00	600598.00	0.11
266904.00	600598.00	0
267159.00	600605.00	0
267402.00	600602.00	0
266152.00	600352.00	0
266423.00	600384.00	0
266655.00	600349.00	0
266905.00	600349.00	0.42
267152.00	600352.00	0
266152.00	600102.00	0
266401.00	600096.00	0
266655.00	600100.00	0.41
266902.00	600102.00	0
267152.00	600102.00	0
267405.00	600098.00	1.17
268904.00	600098.00	0.34
266152.00	599852.00	0
266401.00	599856.00	0
266654.00	599851.00	0
266902.00	599852.00	0
267152.00	599852.00	0
267409.00	599844.00	0.44

Easting	Northing	Peat Depth (m)
267655.00	599849.00	0.56
268905.00	599847.00	0.47
266404.00	599597.00	0
266655.00	599599.00	0.29
266903.00	599599.00	0.32
267155.00	599600.00	0.13
267403.00	599603.00	0
267653.00	599599.00	0.15
266653.00	599354.00	0.19
266902.00	599352.00	0
267152.00	599352.00	0
267402.00	599352.00	0
267652.00	599352.00	0
267904.00	599349.00	0.76
267907.00	599099.00	0.25
268405.00	599097.00	0.97
268656.00	599099.00	0.72
268904.00	599101.00	0
265661.00	602551.00	0.41
265856.00	602546.00	0.4
265556.00	602449.00	0.24
265653.00	602448.00	0.23
265854.00	602447.00	0.4
265955.00	602449.00	0.44
265357.00	602345.00	0.57
265457.00	602354.00	0.42
265553.00	602349.00	0.84
265655.00	602350.00	1.19
265856.00	602348.00	0.49
265956.00	602347.00	0.42
264849.00	602254.00	0.17
264958.00	602248.00	0.19
265056.00	602249.00	0.67
265159.00	602253.00	0.47
265255.00	602251.00	0.6
265354.00	602250.00	0.22
265452.00	602252.00	1.08
265555.00	602248.00	0.22
265659.00	602242.00	0.77
265756.00	602249.00	1.59
264953.00	602149.00	0.69
265060.00	602147.00	1.09
265154.00	602145.00	0.24
265255.00	602149.00	0.41
265357.00	602156.00	0.58
265456.00	602149.00	0.46
265555.00	602149.00	0.4
265657.00	602150.00	0.89
265748.00	602144.00	0.59

Easting	Northing	Peat Depth (m)
264952.00	602048.00	0.57
265056.00	602050.00	0.21
265155.00	602045.00	0.63
265256.00	602045.00	0.64
265353.00	602047.00	0.61
265050.00	601950.00	0.78
265156.00	601947.00	0.9
265255.00	601950.00	0.38
265348.00	601949.00	0.27
265051.00	601850.00	0.41
265157.00	601849.00	1.49
265256.00	601852.00	0.67
265355.00	601748.00	0.59
265360.00	601843.00	0.36
264953.00	601749.00	0.82
265059.00	601747.00	1.58
265155.00	601745.00	1.09
265257.00	601750.00	1.62
264951.00	601655.00	0.64
265054.00	601647.00	2.11
265153.00	601647.00	1.1
265253.00	601648.00	0.41
265356.00	601650.00	1.17
265054.00	601549.00	1.41
265157.00	601545.00	1.59
265254.00	601530.00	0.57
265356.00	601546.00	0.26
265453.00	601549.00	1.11
265055.00	601448.00	1.17
265155.00	601448.00	0.87
265255.00	601453.00	0.57
265356.00	601449.00	0.71
265454.00	601449.00	0.41
265053.00	601345.00	0.19
265155.00	601348.00	0.37
265251.00	601345.00	0.51
265357.00	601356.00	0.64
265452.00	601350.00	0.97
265154.00	601247.00	0.03
265252.00	601255.00	0.98
268555.00	601246.00	0.81
268659.00	601251.00	2.71
268457.00	601150.00	0.69
268555.00	601149.00	0.46
268656.00	601149.00	0.53
268455.00	601049.00	1.01
268556.00	601050.00	1.03
268655.00	601049.00	0.84
268355.00	600947.00	1.01

Easting	Northing	Peat Depth (m)
268456.00	600947.00	1.48
268557.00	600945.00	0.19
268655.00	600949.00	0.59
265857.00	600855.00	1.81
265955.00	600851.00	1.08
268354.00	600851.00	1.27
268556.00	600847.00	0.4
265756.00	600750.00	0.21
267753.00	600751.00	0.82
267856.00	600747.00	0.45
267949.00	600745.00	0.37
268353.00	600747.00	1.21
268553.00	600749.00	0.43
268655.00	600749.00	1.36
267564.00	600632.00	0.57
267653.00	600648.00	0.49
267755.00	600650.00	0.46
267855.00	600648.00	0.44
267955.00	600649.00	1.66
268355.00	600646.00	0.81
268553.00	600650.00	1
268654.00	600650.00	1.31
268754.00	600648.00	0.21
267456.00	600547.00	0.44
267556.00	600552.00	0.83
267655.00	600545.00	0.92
267757.00	600549.00	0.69
267855.00	600548.00	0.49
267956.00	600551.00	0.43
268057.00	600547.00	1.17
268155.00	600550.00	0.85
268356.00	600549.00	0.76
268456.00	600552.00	1.36
268555.00	600546.00	1.04
268655.00	600549.00	1.02
268754.00	600553.00	0.33
267459.00	600446.00	0.23
267555.00	600447.00	0.78
267656.00	600447.00	0.74
267755.00	600456.00	0.25
267856.00	600447.00	0.78
267956.00	600450.00	0.6
268054.00	600448.00	0.76
268155.00	600447.00	0.77
268354.00	600447.00	1.23
268457.00	600447.00	0.92
268555.00	600446.00	0.86
268654.00	600449.00	0.36
268754.00	600447.00	0.26

Easting	Northing	Peat Depth (m)
268857.00	600451.00	0.69
267356.00	600348.00	0.35
267454.00	600349.00	0.31
267556.00	600348.00	1.05
267654.00	600349.00	0.63
267757.00	600351.00	1.01
267855.00	600349.00	0.27
267935.00	600355.00	1.28
268056.00	600348.00	1.05
268154.00	600348.00	1.17
268353.00	600349.00	0.96
268459.00	600347.00	0.58
268554.00	600347.00	0.97
268656.00	600354.00	1.03
268756.00	600348.00	1.03
268858.00	600348.00	0.83
268957.00	600350.00	1.26
267353.00	600251.00	0.12
267454.00	600250.00	0.2
267555.00	600248.00	0.29
267654.00	600246.00	0.34
267755.00	600249.00	0.93
267852.00	600249.00	0.47
267945.00	600247.00	1.28
268056.00	600247.00	1.57
268156.00	600248.00	0.95
268355.00	600249.00	1.71
268457.00	600248.00	1.51
268553.00	600252.00	1.04
268653.00	600249.00	0.65
268750.00	600253.00	0.65
268855.00	600249.00	1.02
268957.00	600249.00	0.48
267655.00	600147.00	0.34
267857.00	600146.00	1.84
267956.00	600145.00	1.93
268055.00	600148.00	1.54
268155.00	600148.00	1.29
268355.00	600149.00	2.43
268457.00	600146.00	2.26
268554.00	600149.00	1
268654.00	600150.00	0.93
268757.00	600148.00	0.86
268855.00	600149.00	0.61
267653.00	600046.00	0.41
267755.00	600047.00	1.06
267856.00	600049.00	0.86
267955.00	600049.00	0.98
268055.00	600044.00	2.03

Easting	Northing	Peat Depth (m)
268156.00	600049.00	0.54
268356.00	600048.00	3.21
268456.00	600047.00	2.01
268555.00	600048.00	1.02
268654.00	600049.00	1
268755.00	600050.00	0.63
267556.00	599948.00	0.5
267654.00	599946.00	0.41
267754.00	599949.00	0.39
267955.00	599949.00	0.76
268050.00	599938.00	0.77
268152.00	599949.00	0
268353.00	599949.00	2.76
268458.00	599947.00	2.1
268555.00	599948.00	1.96
268663.00	599965.00	1.18
268758.00	599956.00	0.56
267958.00	599849.00	0.34
268056.00	599844.00	0.89
268152.00	599844.00	1.07
268351.00	599855.00	1.13
268456.00	599852.00	3.48
268554.00	599849.00	1.04
268656.00	599847.00	1.18
268755.00	599848.00	0.99
268851.00	599851.00	0.21
267854.00	599751.00	0.36
267952.00	599752.00	2.73
268051.00	599755.00	3.01
268157.00	599751.00	1.61
268353.00	599750.00	1.46
268458.00	599751.00	1.91
268556.00	599750.00	1.28
268654.00	599751.00	2.16
268754.00	599748.00	0.2
268856.00	599748.00	1.55
267854.00	599645.00	2.2
267959.00	599648.00	2.1
268051.00	599644.00	1.38
268156.00	599649.00	1.07
268355.00	599652.00	1.49
268457.00	599651.00	0
268553.00	599649.00	0.43
268657.00	599652.00	1.01
268755.00	599649.00	0.49
268855.00	599651.00	1.81
267853.00	599550.00	0.97
267955.00	599548.00	0.37
268055.00	599548.00	0.21

Easting	Northing	Peat Depth (m)
268150.00	599550.00	1.89
268354.00	599548.00	1.23
268458.00	599548.00	1.35
268555.00	599547.00	0.62
268650.00	599549.00	1.06
268756.00	599548.00	1.67
268855.00	599546.00	1.39
267955.00	599449.00	0.55
268053.00	599452.00	1.01
268152.00	599450.00	0.8
268353.00	599443.00	1.09
268457.00	599449.00	1.34
268548.00	599432.00	0.24
268656.00	599451.00	0.83
268755.00	599445.00	0.91
268850.00	599444.00	1.16
268052.00	599351.00	0.37
268156.00	599349.00	0.21
268353.00	599349.00	0.68
268454.00	599351.00	1.44
268557.00	599347.00	0.88
268655.00	599350.00	0.84
268755.00	599343.00	0.88
268854.00	599348.00	0.79
268052.00	599248.00	0.16
268153.00	599250.00	0.89
264433.00	601586.00	0.44
268356.00	599246.00	0.42
268454.00	599252.00	0.76
268555.00	599248.00	0.83
268056.00	599149.00	0.24
268157.00	599152.00	0.78
268352.00	599151.00	0.96
268458.00	599150.00	1.41
267955.00	599049.00	0.19
268055.00	599051.00	0.72
268154.00	599045.00	0.48
263259.00	601875.00	1.05
263231.00	601776.00	1.62
263221.00	601677.00	0.5
263239.00	601585.00	1.2
263290.00	601493.00	1.85
263364.00	601425.00	0.8
263460.00	601415.00	0.32
263552.00	601457.00	0.28
263648.00	601491.00	0.75
263732.00	601445.00	0.39
263796.00	601373.00	1.74
263885.00	601385.00	0.5

Easting	Northing	Peat Depth (m)
263989.00	601425.00	0.63
264078.00	601452.00	0.44
264175.00	601476.00	1.16
264273.00	601489.00	1.59
264370.00	601521.00	0.08
264413.00	601680.00	0.24
264375.00	601773.00	1
264378.00	601866.00	0.18
264454.00	601927.00	0.32
264552.00	601946.00	0.21
264653.00	601999.00	0.23
264703.00	602046.00	0.19
264782.00	602067.00	0.23
264709.00	601979.00	0.21
264520.00	601884.00	0.2
264416.00	601812.00	0.45
264481.00	601650.00	0.21
264343.00	601456.00	1.09
264143.00	601421.00	0.19
263962.00	601365.00	0
263716.00	601374.00	0.59
263621.00	601438.00	0.84
263412.00	601364.00	1.45
263218.00	601515.00	0.25
263175.00	601741.00	1.1
263291.71	601818.75	0.85
263278.00	601637.00	1.75
263353.00	601491.00	0.5
263495.00	601490.00	0.39
263714.00	601525.00	0
263833.00	601418.00	1.68
264019.00	601488.00	0.49
264224.00	601504.00	1.47
264349.00	601705.00	1.09
264376.00	601941.00	0.34
264584.00	602017.00	0.21
264731.00	602112.00	0.35
265164.00	601983.00	2.19
265138.00	601386.00	1.59
265776.00	602535.00	0.26
265366.00	601313.00	1.21
265420.00	601059.00	0.8
265759.00	600845.00	0.19
266393.00	599714.00	0.45
266683.00	600579.00	0.29
268455.00	600748.00	0
268253.00	599048.00	0.94
268256.00	599152.00	0.49
268256.00	599247.00	1.01

Easting	Northing	Peat Depth (m)
268255.00	599349.00	0.71
268255.00	599449.00	0.83
268281.00	599719.00	0.73
268253.00	599853.00	2.27
268255.00	599956.00	1.32
268256.00	600048.00	1.17
268254.00	600149.00	0.44
268255.00	600249.00	0.79
268254.00	600548.00	1.04
268255.00	600648.00	1.42
266734.23	599628.26	0.2
266723.10	599674.07	0.2
266720.23	599722.96	0.3
266724.16	599775.92	0.45
266738.75	599873.47	0
266756.15	599920.08	0.15
266796.25	600013.33	0.1
266727.22	599825.66	0.2
266771.88	599968.35	0
266815.41	600055.07	0
266837.31	600100.06	0.1
266857.68	600146.59	0.3
266880.45	600192.11	0.4
266889.81	600235.63	0.3
266903.13	600291.27	0.5
266912.29	600338.51	0
266914.74	600388.35	0.1
266943.18	600407.73	0
266937.43	600392.68	0
266954.59	600389.01	0.1
266971.58	600397.59	0.1
266973.13	600413.88	0
266973.74	600434.09	0
266957.18	600418.81	0.1
266955.05	600436.14	0
266937.58	600429.24	0
266920.86	600422.87	0
266922.04	600441.03	0.15
266916.20	600489.64	0.4
266901.75	600537.77	0.7
266878.12	600579.68	0.1
266847.37	600620.69	0
267961.21	600767.32	0.2
267983.68	600742.90	0.4
267960.36	600738.77	0.8
267934.18	600741.78	0.5
267911.01	600714.45	1
267934.44	600715.23	0.5
267961.02	600714.81	0.95

Easting	Northing	Peat Depth (m)
267984.10	600718.02	0.7
268008.89	600714.68	0.3
267985.78	600692.54	1.2
267985.27	600682.54	0.2
267975.66	600680.23	0.4
267960.95	600691.24	0.2
267935.44	600691.82	2.5
267959.56	600665.86	0.8
267978.24	600631.53	0.8
267978.41	600580.67	1.4
267968.12	600583.76	0.7
267987.79	600578.91	1.1
267978.82	600530.55	0.6
267974.37	600480.77	0.3
267973.86	600431.79	0.4
267978.40	600381.55	0.8
267983.32	600333.15	0.95
267986.56	600282.20	1
267976.30	600278.98	1
267996.02	600283.22	0.9
267989.78	600233.86	1.4
267980.30	600232.10	1.5
268000.47	600229.83	0.9
267994.04	600181.21	0.6
267998.45	600133.76	0.9
267983.32	600088.19	1.4
267982.71	600099.71	1.2
267985.82	600076.05	1.5
268001.63	600041.43	2
267991.22	600040.44	2.2
268010.09	600040.99	2.5
268002.07	599992.42	1.3
268014.80	599992.79	2
267992.46	599989.74	1.6
268003.93	599941.15	0
267998.90	599893.05	0.4
267971.92	599830.38	0.8
267938.80	599796.30	2.5
267933.25	599802.03	1.85
267946.39	599784.19	2.5
267901.66	599758.62	3.2
267907.86	599750.08	2.7
267894.22	599768.68	2.3
267858.90	599721.11	2.6
267864.42	599714.26	3.8
267830.77	599733.64	3.6
267814.32	599697.20	2.8
267823.22	599686.36	2.6
267809.85	599703.65	2.5

Easting	Northing	Peat Depth (m)
267773.59	599670.77	2.2
267782.96	599661.77	2.3
267770.26	599679.96	1.4
267731.71	599644.92	0.9
267768.89	599598.53	1.3
267769.28	599607.99	1
267769.47	599589.61	1.8
267816.76	599590.61	0.3
267861.58	599569.60	0.9
267891.03	599534.02	0.2
267912.00	599487.55	0.6
267940.07	599448.11	0
267979.97	599418.16	0.95
268028.17	599400.21	1.4
268031.58	599411.42	1.4
268023.11	599390.33	1.1
268075.31	599385.62	0.45
268125.66	599386.35	1
268127.61	599394.83	0.95
268122.72	599373.08	1
268154.24	599396.26	0.5
268163.71	599411.75	1.5
268155.12	599422.22	0.8
268129.91	599422.23	0
268105.54	599447.26	0.2
268127.40	599448.28	0
268154.55	599449.33	1.1
268155.67	599472.68	0.6
268128.24	599472.94	0.6
268153.64	599497.05	1
268177.75	599474.06	0.4
268203.20	599449.74	0
268180.42	599446.15	0.8
268178.73	599421.70	1
268165.92	599361.40	1.6
268175.19	599362.98	0.9
268167.69	599314.02	0.95
268172.50	599262.29	1.2
268163.91	599261.80	0.6
268182.94	599260.31	0.9
268185.48	599214.21	1.8
268195.80	599211.86	1.4
268172.99	599214.58	1.2
268190.18	599165.45	0.8
268190.89	599114.58	0.4
268191.73	599064.63	0.9
268194.10	599040.81	0.7
268143.90	599034.88	1
268095.14	599034.29	0.6

Easting	Northing	Peat Depth (m)
268069.87	599050.07	0.2
268045.42	599037.07	0.6
268044.75	599050.08	0.8
268045.93	599071.76	0.9
268022.60	599074.87	0.7
268022.05	599099.01	0.6
267995.50	599075.67	0.8
267972.16	599049.83	1.3
267994.59	599048.61	0.9
267995.31	599026.50	0.85
268020.43	599048.21	0.95
268021.17	599026.66	0.9
268022.01	599001.77	0.95
268044.63	599024.66	0.95
268226.52	599040.77	0.7
268273.31	599049.95	0
268325.81	599058.79	0.95
268370.47	599078.24	0.7
268413.06	599103.14	0.95
268452.90	599135.18	0
268493.84	599164.95	0.6
268535.61	599190.81	0.2
268574.82	599219.33	0.5
268618.77	599247.35	0.3
268657.68	599272.92	0.6
268699.59	599303.41	0.6
268729.46	599285.45	0.3
268763.91	599300.20	0.6
268738.74	599305.22	0.85
268714.50	599316.70	1
268702.05	599347.32	0.9
268725.09	599341.63	1.25
268738.33	599337.89	0.95
268748.33	599332.03	0.95
268771.36	599322.62	0.8
268794.40	599313.78	0.7
268781.22	599344.23	0.95
268757.62	599352.54	1.1
268736.31	599362.63	1.2
268753.90	599384.38	1
268765.06	599378.11	1.1
268762.00	599435.92	0.9
268759.58	599482.94	1.8
268747.82	599482.92	1
268772.33	599484.23	1.2
266767.52	599593.86	0.1
266815.76	599591.29	0.2
266864.41	599609.68	0.2
266912.09	599623.65	0

Easting	Northing	Peat Depth (m)
266961.12	599633.69	0
267026.27	599647.50	0
267046.11	599683.65	0.2
267087.77	599705.60	0.4
267137.90	599713.00	0.2
267188.27	599721.70	0.2
267236.83	599726.18	0.4
267286.92	599722.08	0.3
267302.86	599748.51	0
267351.32	599753.37	0
267351.83	599802.16	0.6
267351.92	599850.96	0.1
267403.29	599900.09	0
267451.54	599901.61	0.5
267452.80	599851.65	0
267501.06	599853.73	0.3
267551.89	599852.95	0.1
267658.79	599828.23	0
267685.05	599852.50	0.5
267711.75	599877.31	0
267763.26	599924.39	0.1
267786.42	599968.80	0.2
267810.98	600010.75	0
267844.45	600049.83	0.5
267885.17	600075.90	0.9
267931.62	600084.53	1.1
267931.31	600095.49	1.1
267932.43	600076.34	1.1
267744.12	599879.31	0.5
267734.77	599849.90	0
267711.45	599849.67	0
267685.62	599825.57	0
267687.87	599801.57	0
267709.90	599826.15	0.3
267725.10	599831.26	0
267737.91	599824.01	0.3
267760.75	599825.93	0
267736.56	599799.92	0
267711.31	599798.82	0.2
267709.09	599774.39	0.3
267603.76	599798.51	0.85
267652.66	599754.37	0
267600.55	599751.10	0.2
267553.47	599799.46	0.3
267503.44	599802.07	0
267553.13	599752.70	0.3
267500.73	599750.75	0
267454.45	599800.75	0.2
267401.27	599801.05	0

Easting	Northing	Peat Depth (m)
267402.87	599751.64	0
267451.98	599753.69	0
267502.06	599703.01	0
267554.00	599704.06	0.1
267603.25	599703.33	0.1
267651.48	599700.58	0.9
267702.97	599650.98	0
267651.54	599649.55	0
267603.04	599650.26	0.8
267551.49	599651.98	0.1
267502.73	599651.22	0
267454.94	599700.53	0
267402.73	599701.16	0
267426.33	599671.88	0.2
267450.64	599648.88	0.1
267472.07	599653.43	0.1
267520.21	599633.25	0.1
267567.18	599616.81	0.1
267617.31	599613.83	0.5
267682.00	599630.08	0.2
267718.30	599603.94	1
267703.19	599601.79	0.9
267669.93	599612.44	0
267603.79	599600.87	0.1
267552.81	599600.54	0.1
267500.96	599602.65	0.1
267454.01	599602.01	0.2
267403.81	599652.32	0.1
267382.02	599688.79	0
267333.10	599707.33	0.1
267302.71	599701.00	0
267352.25	599650.16	0.2
267406.30	599604.55	0
267452.81	599551.38	0.2
267504.31	599551.51	0
267553.60	599548.92	0.3
267601.40	599553.06	0.3
267652.65	599551.90	0.5
267702.00	599551.17	0.1
267752.66	599551.69	0.8
267755.33	599502.81	0
267753.29	599452.21	0.1
267752.05	599403.62	0.35
267702.42	599402.32	0.2
267702.22	599352.96	0
267702.57	599304.33	0.2
267653.71	599300.22	0.1
267603.79	599299.86	0.2
267651.46	599405.70	0

Easting	Northing	Peat Depth (m)
267703.35	599450.91	0.2
267702.38	599499.94	0.2
267654.22	599501.56	0.2
267549.97	599452.35	0
267601.67	599505.36	0.3
267552.21	599502.57	0.1
267500.22	599499.86	0
267503.83	599450.57	0
267453.42	599451.52	0.2
267401.29	599451.60	0
267452.18	599502.22	0.1
267400.55	599501.17	0.2
267402.72	599552.33	0
267352.90	599551.59	0.4
267350.87	599603.80	0.3
263354.80	602350.50	0.9
263355.43	602333.04	0.7
263341.84	602287.43	0.8
263325.53	602242.65	1.2
263315.11	602241.49	0.8
263333.89	602235.71	0.6
263309.57	602192.30	0.6
263301.82	602143.73	1
263313.29	602144.86	0.6
263290.68	602142.96	1.2
263287.49	602094.62	1.1
263280.06	602101.16	0.65
263296.95	602088.94	0.5
263269.05	602049.72	0.55
263249.47	602002.07	0.4
263241.41	601953.69	1.4
263232.34	601954.90	1.8
263251.80	601950.77	1.1
263231.93	601904.25	1.05
263222.36	601906.40	0.95
263243.17	601904.64	0.95
263221.16	601853.73	0.6
263213.10	601805.36	1.2
263202.96	601806.41	1.4
263223.87	601804.28	1.1
263216.42	601758.67	0.95
263223.99	601708.88	1.1
263212.21	601708.14	1.1
263235.11	601708.91	0.9
263234.86	601659.74	0.95
263247.51	601609.98	3.2
263258.53	601617.06	2.2
263238.28	601606.00	2.85
263271.67	601565.81	2

Easting	Northing	Peat Depth (m)
263281.35	601567.18	1.4
263264.63	601559.92	2.85
263302.19	601532.20	0.7
263345.29	601501.17	0.6
263387.10	601476.31	1
263385.44	601487.68	2
263384.46	601466.00	0.9
263437.57	601481.44	0.6
263481.16	601496.98	0.3
263528.85	601515.36	0.5
263573.09	601538.31	0.2
263620.83	601547.79	0
263674.34	601545.03	0.4
263714.87	601523.55	1.6
263724.11	601531.06	0.2
263711.28	601513.45	0.8
263737.83	601477.93	1.2
263747.77	601480.96	0.3
263728.93	601474.31	0.9
263765.08	601434.41	0.7
263810.16	601425.97	0.35
263858.28	601444.53	0.4
263902.33	601464.70	0.8
263945.36	601483.05	0.3
263997.84	601494.98	0.8
264045.28	601508.74	0.4
264093.55	601521.55	0.4
264140.11	601534.04	1.3
264140.13	601541.65	1.2
264143.41	601524.10	0.95
264190.43	601541.40	0.8
264242.80	601549.82	0
264293.48	601558.47	0.1
264293.79	601547.88	0
264324.33	601549.17	0
264372.81	601544.90	0
264423.51	601537.04	0
264470.19	601532.82	1
264471.19	601541.14	1
264464.61	601523.53	1
264501.28	601486.21	1
264507.74	601489.54	0.9
264488.09	601487.73	0.6
264500.62	601436.87	1.3
264490.39	601434.96	0.8
264510.81	601441.20	0.8
264514.21	601389.69	1.6
264505.91	601384.93	1.3
264524.76	601391.77	1.5

Easting	Northing	Peat Depth (m)
264529.93	601342.81	2
264521.26	601336.21	1.9
264541.41	601344.13	1.4
264550.13	601296.91	1.3
264540.15	601292.57	1.2
264560.62	601300.48	0.9
264570.53	601250.44	0
264588.61	601204.42	0.1
264599.75	601153.04	0.1
264608.81	601106.55	0.4
264620.21	601056.65	0.5
264626.35	601011.55	0.5
264632.21	600957.56	0.5
264638.87	600908.54	0.9
264648.95	600860.54	0
264656.92	600820.02	0
264660.28	600770.55	0
264635.53	600723.06	0
264629.56	600670.16	0
264625.86	600618.31	0.2
264664.51	600572.96	0
264662.21	600525.15	0
264661.72	600436.46	0
264658.37	600399.81	0.2
264628.50	600438.03	0.1
264696.27	600430.63	0
264656.45	600468.72	0
264678.06	600459.11	0
264608.14	600814.65	0
264569.77	600844.96	0
264542.49	600888.11	0.2
264510.40	600926.21	0.2
264470.51	600948.40	0.1
264420.87	600970.34	0
264378.12	600989.28	0.2
264354.97	601007.99	0.1
264334.07	601013.83	0.1
264332.00	601029.11	0.1
264290.62	601040.77	0
264306.90	601008.72	0.3
264327.08	600982.68	0.5
264331.10	601082.77	0.2
264353.56	601031.23	0
264378.86	601030.64	1
265751.86	602224.72	0.9
265130.46	601603.39	0.7
265179.57	601616.37	0.3
265198.70	601635.83	0.55
265234.40	601601.34	0.95

Easting	Northing	Peat Depth (m)
265228.13	601670.20	1.8
265232.58	601638.88	1.1
265215.96	601618.23	0.9
265214.04	601652.81	0.5
265194.78	601670.47	1.7
265161.64	601667.40	0.35
265180.35	601652.35	0.1
265166.30	601629.21	0.65
265165.65	601597.31	0.8
265081.13	601597.29	1.4
265082.20	601608.02	0.6
265082.59	601589.45	1.55
265037.85	601584.32	1.2
265030.34	601591.78	0.85
265042.03	601575.65	1.6
264993.83	601554.30	1.5
264988.24	601562.26	1.8
265003.21	601546.03	0.85
264956.17	601528.17	1.4
264958.13	601515.86	1.6
264950.15	601538.93	0.9
264904.55	601516.38	1.8
264901.74	601528.34	1.2
264907.12	601506.84	1.9
264855.78	601504.32	0.95
264805.33	601499.55	0.8
264755.55	601502.93	1
264757.77	601492.47	0.9
264706.28	601509.08	0.1
264654.30	601516.79	1.1
264653.98	601527.19	0.3
264653.44	601506.05	0.8
264620.34	601521.36	0.65
264600.43	601514.36	1.2
264567.23	601502.38	1.1
264577.16	601525.83	0.9
264587.93	601548.89	0.9
264574.73	601581.40	0.9
264556.54	601533.89	0.65
264559.53	601555.94	0
264544.83	601511.23	0.7
264534.03	601490.41	0.95
264530.93	601548.22	0.3
264506.93	601556.56	0.3
264338.95	601573.59	0.2
264387.43	601593.45	0
264424.50	601624.79	0
264435.05	601671.60	0.6
264416.46	601714.67	0.4

Easting	Northing	Peat Depth (m)
264393.04	601755.66	0.1
264366.56	601803.80	0.2
264358.21	601852.86	0.1
264352.66	601899.80	0.1
264378.88	601943.35	0.1
264424.48	601962.74	0
264474.02	601965.31	0
264521.96	601967.73	0
264574.25	601970.40	0
264620.76	601974.55	0
264672.98	601978.51	0.1
264697.90	601979.42	0.6
264707.32	602010.50	0.2
264680.40	602051.22	0.1
264725.09	602027.03	0.2
264763.44	601996.53	0.5
264732.63	602052.04	0
264750.62	602069.12	0.1
264762.12	602095.31	0.2
264790.32	602134.53	0.2
264831.41	602165.75	0.3
264878.34	602187.14	0.9
264921.53	602200.49	0.6
264962.95	602204.42	0
265014.13	602191.72	0.3
265059.34	602174.19	0
265077.14	602164.19	0.2
265078.24	602176.03	0
265080.49	602183.57	0
265083.20	602196.11	0.55
265084.89	602206.45	0.2
265087.07	602215.29	0.2
265096.78	602210.91	0.55
265094.19	602202.27	0.5
265107.18	602211.52	0.2
265116.27	602207.53	0.1
265126.73	602207.03	0.2
265136.95	602205.23	0.1
265133.66	602194.57	0.2
265123.15	602197.12	0.1
265114.00	602199.07	0.2
265104.61	602200.28	0.25
265093.52	602190.97	0.1
265101.70	602191.83	0
265111.86	602188.00	0.1
265123.01	602185.61	0
265132.85	602185.31	0.1
265128.71	602174.49	0.1
265115.87	602166.90	0.2

Easting	Northing	Peat Depth (m)
265119.34	602176.45	0.1
265109.05	602179.36	0
265106.84	602169.40	0.2
265095.69	602171.60	0.4
265098.54	602181.72	0
265089.95	602184.95	0
265088.12	602169.98	0.3
265084.46	602164.71	0.4
265094.93	602160.67	0.2
265104.55	602160.20	0.2
265114.74	602157.47	0.1
265125.72	602156.40	0.1
265126.56	602166.58	0
265156.11	602170.32	0.1
265205.90	602181.23	0.1
265253.45	602192.03	0
265281.22	602185.80	0.1
265305.10	602198.07	0.3
265324.10	602150.72	0.3
265351.10	602216.89	0
265331.59	602243.66	0
265283.81	602239.54	0.1
265341.91	602294.19	0.95
265365.29	602338.58	0.9
265398.54	602373.57	0.2
265434.86	602408.28	0.4
265475.56	602433.95	0.2
265522.73	602446.07	0.2
265573.66	602446.00	0.1
265618.93	602430.34	0
265658.24	602396.48	0.65
265684.72	602354.85	0.2
265707.76	602311.46	0.8
265729.53	602268.30	0.85
264989.80	602165.00	0.65
264993.90	602118.66	0.8
264996.71	602065.31	1.2
265008.04	602068.68	1.3
264986.58	602062.84	0.8
264992.56	602015.89	0.8
264990.28	601965.48	1.2
264980.99	601966.50	1.3
265001.32	601962.91	1.8
264982.68	601917.64	0.95
264963.94	601869.41	0.6
264946.46	601823.91	0.7
264921.69	601779.20	0.5
264897.51	601736.51	0.55
264868.17	601698.25	0.4

Easting	Northing	Peat Depth (m)
264832.53	601658.33	1.1
264841.69	601653.04	0.95
264822.98	601664.56	0.9
264795.10	601625.51	1.1
264791.92	601632.66	1
264802.53	601615.82	0.6
264762.09	601592.00	1.2
264755.71	601601.66	0.8
264769.52	601585.83	0.9
264724.12	601559.20	0.95
264675.55	601536.18	0.5
266792.09	600859.38	0.22
266779.52	600907.09	0
266765.89	600958.35	0
266747.76	601006.19	0
266731.55	601053.67	1.07
266716.94	601049.92	0.82
266742.96	601056.50	0.63
266718.97	601102.42	0.61
266710.05	601149.85	0
266692.70	601196.49	0
266669.13	601240.47	0
266640.66	601281.82	0
266604.53	601318.33	0
266571.43	601354.05	0
266533.14	601385.53	0.55
266492.84	601411.96	0
266441.80	601430.44	0
266396.92	601445.98	0
266345.21	601449.47	0
266297.33	601455.37	0
266248.01	601461.91	0.42
266199.37	601473.32	0.38
266150.70	601487.58	0
266110.11	601512.71	0
266082.21	601553.87	0
266062.40	601598.96	0
266038.38	601642.48	0
266016.76	601688.41	0
265997.07	601735.83	0
265978.21	601783.68	0
265962.44	601830.37	0.4
265946.57	601878.05	0.16
265928.72	601922.54	0.21
265908.12	601968.66	0
265882.75	602010.07	0.22
265858.12	602054.49	0.1
265829.49	602094.64	1.61
265816.76	602092.87	1.56

Easting	Northing	Peat Depth (m)
265840.46	602099.95	1.43
265804.12	602139.73	1.52
265816.25	602143.18	1.65
265794.84	602132.57	0.87
265772.13	602179.10	0.7
265781.37	602183.03	1.42
265792.12	602186.33	1.15
265765.62	602233.44	0.99
265756.44	602226.09	0.98
265747.74	602220.30	0.9
268654.76	600767.71	0.18
268678.20	600743.29	1.04
268653.75	600743.46	1.52
268628.92	600743.50	0.62
268603.47	600718.49	0.36
268629.00	600719.44	0.94
268655.09	600719.02	1.3
268656.21	600706.99	1.2
268665.71	600710.83	0.75
268674.95	600713.14	0.56
268679.26	600720.86	0.6
268705.88	600718.51	1.41
268677.92	600694.53	0.42
268652.18	600694.22	0.68
268628.42	600694.66	0.85
268653.22	600667.87	1.11
268669.29	600658.30	1.23
268679.82	600662.60	0.97
268688.86	600666.81	1.08
268692.82	600613.13	1.2
268681.64	600609.86	1.44
268701.37	600618.42	0.95
268706.99	600564.75	0.74
268718.35	600517.79	0.31
268728.02	600467.67	0.31
268737.08	600418.59	0.8
268745.58	600368.73	0.8
268747.53	600314.18	1.04
268735.05	600315.61	0.9
268760.17	600317.27	0.74
268748.52	600262.87	0.93
268759.92	600219.49	0.46
268808.50	600222.97	0.52
268849.13	600237.28	1.15
268860.00	600234.02	1.13
268857.76	600225.05	0.3
268857.47	600216.80	0.85
268870.92	600239.34	0.9
268872.81	600261.93	1.23

Easting	Northing	Peat Depth (m)
268896.85	600287.44	1.08
268896.37	600262.05	1.26
268922.98	600261.44	1.2
268946.31	600236.90	0.63
268921.19	600236.24	0.97
268895.25	600236.65	1.58
268871.25	600210.99	1.18
268897.87	600213.17	1.03
268923.86	600210.81	0.68
268896.37	600185.99	0.94
268748.02	600188.98	0.82
268720.80	600145.54	0.9
268693.08	600104.20	0.91
268665.58	600061.38	1.37
268656.45	600066.27	1.37
268677.42	600056.18	0.7
268645.67	600018.13	1.42
268651.86	600011.36	1.04
268634.67	600022.41	1.39
268620.32	599975.36	1.56
268610.25	599980.30	1.4
268629.19	599968.73	0.71
268592.45	599931.57	1.78
268584.40	599938.27	1.8
268601.92	599923.24	1.48
268567.18	599888.19	1.35
268557.51	599894.68	1.55
268575.76	599883.52	1.34
268523.76	599895.99	1.18
268500.61	599869.16	2.1
268524.31	599869.23	1.17
268532.45	599851.19	0.95
268549.62	599869.02	1.28
268575.09	599844.25	1.33
268548.93	599838.40	1.57
268549.02	599846.19	1.28
268540.61	599847.67	0.9
268525.37	599844.05	1.34
268501.00	599844.35	2.36
268474.24	599845.54	2.76
268499.14	599817.74	2.3
268525.27	599818.69	1.51
268550.22	599818.98	1.83
268525.77	599796.31	2.1
268703.83	600346.17	1.3
268653.01	600338.20	0.69
268652.30	600349.11	1.09
268654.62	600327.52	0.15
268602.97	600332.08	0.69

Easting	Northing	Peat Depth (m)
268552.98	600325.84	0.34
268503.01	600315.93	0.87
268452.76	600308.76	0.4
268405.29	600297.92	0.68
268355.67	600282.95	2.27
268355.06	600295.31	2.73
268360.66	600274.43	2.58
268310.81	600264.67	1.41
268309.89	600276.84	0.94
268307.67	600287.87	0.6
268327.61	600305.41	1.9
268303.13	600300.05	1.01
268277.73	600292.66	0.88
268248.99	600310.11	0.54
268273.59	600318.15	0.84
268274.81	600333.08	1.09
268284.88	600330.38	0.99
268295.61	600331.57	1.59
268295.45	600325.15	0.97
268322.41	600331.20	1.4
268346.61	600337.21	1.8
268314.80	600355.55	1.54
268290.62	600348.42	1.85
268266.70	600340.56	1.48
268285.83	600373.41	0.18
268277.84	600264.39	0.44
268273.37	600211.35	0.47
268270.36	600162.98	0.69
268262.90	600113.54	0.9
268232.87	600073.56	1.54
268228.55	600080.45	0.59
268242.68	600065.23	2.4
268201.87	600034.88	1.23
268194.13	600041.38	0.78
268188.97	600049.39	0.89
268156.20	600009.89	0.69
268120.62	599974.72	1.61
268127.83	599966.08	1.52
268111.60	599982.80	1.47
268085.64	599941.39	0.46
268047.35	599907.81	0.72
268010.40	599871.27	0.98
268008.72	599882.57	0.8
268018.78	599861.61	0.64
264955.59	601152.14	1.5
264954.44	601251.29	0.8
264954.62	601350.67	0.57
264954.23	601452.80	0.94
264955.07	601552.78	1.42

Easting	Northing	Peat Depth (m)
264955.52	601850.25	0.35
264953.80	601951.11	0.44
264854.31	602150.37	0.28
264856.42	602048.70	0.32
264854.97	601949.91	1.25
264857.06	601850.16	0.23
264855.41	601749.91	0.26
264855.61	601649.38	1.19
264854.64	601547.76	1.02
264855.42	601449.57	1.13
264853.98	601349.50	1.37
264855.12	601251.07	1.08
264854.56	601148.92	0.89
264854.82	601050.05	0.67
264756.99	600951.86	0.41
264755.95	601049.40	0.32
264754.94	601152.46	0.18
264754.13	601253.86	0.45
264755.76	601350.64	0.65
264756.12	601449.10	1.18
264754.04	601651.62	0.27
264754.96	601750.53	0.74
264756.37	601850.29	0.36
264754.33	601951.38	0.41
264755.50	602051.20	0.1
264754.20	602151.33	0.1
264755.42	602248.38	0.54
264655.94	602150.83	0.21
264655.30	602049.29	0.26
264654.32	601949.69	0.34
264654.82	601847.53	0.27
264654.74	601749.96	0.3
264654.02	601650.97	0.58
264654.81	601550.99	0.36
264654.65	601448.75	0.94
264654.30	601349.59	0.28
264656.17	601248.60	0.15
264653.37	601150.95	0.22
264655.26	601050.54	0.38
264654.80	600949.71	0.4
264655.00	600750.64	0
264655.68	600649.97	0.41
264655.83	600549.00	0
264647.01	600455.39	0
264655.43	600348.56	0
264556.05	600449.36	0.35
264552.98	600550.62	0.9
264554.81	600651.11	0.59
264553.91	600750.70	0.94

Easting	Northing	Peat Depth (m)
264555.55	600950.88	0.82
264554.51	601048.98	0.3
264554.81	601149.46	0.34
264554.54	601349.94	1.5
264555.39	601450.92	0.97
264555.07	601549.98	0.65
264555.07	601651.27	0.05
264556.15	601751.98	0.31
264554.93	601850.54	0.22
264553.73	602048.50	0.18
264454.47	602049.21	0.55
264457.14	601950.07	0.28
264456.24	601848.96	0.17
264454.44	601749.88	0.18
264453.97	601651.60	0.25
264455.16	601548.94	0.11
264455.88	601448.88	0.43
264455.43	601349.09	0.66
264457.01	601248.89	0.46
264455.98	601151.98	0.33
264454.90	601050.25	0.29
264454.87	600948.34	0.31
264455.34	600850.32	0.19
264353.73	600849.49	0.05
264355.86	600950.17	0.33
264355.86	601149.90	0.26
264354.38	601248.81	0.33
264354.01	601352.34	0.56
264356.12	601449.71	1.05
264355.17	601551.84	0.26
264353.79	601653.19	0.85
264354.40	601749.76	0.37
264355.66	601955.06	0.23
264356.00	602053.21	0.17
264256.74	601951.43	0.44
264254.63	601849.91	0.18
264254.11	601748.70	0.84
264255.26	601649.10	0.54
264255.07	601549.66	0.96
264253.13	601450.46	0.94
264251.47	601353.11	0.22
264253.69	601251.09	0.24
264252.96	601151.83	0.22
264253.98	601048.25	0.22
264156.72	600948.48	0.24
264155.61	601052.23	0.13
264154.40	601151.01	0.23
264155.70	601250.18	0.17
264155.63	601353.32	0.05

Easting	Northing	Peat Depth (m)
264155.77	601452.60	1.17
264153.70	601550.94	0.53
264156.86	601650.23	0.78
264154.25	601751.12	0.67
264152.25	601853.19	0.18
264054.24	601650.40	0.44
264053.81	601552.69	0.98
264055.24	601449.23	0.14
264727.54	601508.97	1.12
264737.48	601509.62	1.02
264748.22	601506.91	1.08
264756.93	601503.84	1.08
264756.41	601495.71	0.37
264768.29	601508.86	0.46
264777.97	601506.45	0.69
264787.65	601506.63	0.49
264798.21	601505.90	0.79
264806.46	601501.86	1.15
264818.32	601505.32	1.31
264827.66	601503.54	1.02
264826.60	601515.48	1.52
264816.24	601514.45	1.41
264807.17	601515.08	0.78
264798.22	601515.94	0.61
264786.95	601516.85	0.85
264776.66	601516.90	0.52
264768.33	601517.19	0.5
264757.49	601518.10	0.44
264747.06	601518.40	0.41
264736.41	601518.95	0.42
264728.42	601520.71	0.46
264728.12	601530.47	0.67
264728.56	601540.09	1.48
264739.61	601538.47	0.99
264749.56	601538.46	0.56
264759.80	601536.90	0.69
264768.94	601537.50	0.69
264778.86	601536.84	0.67
264790.60	601536.56	1.04
264799.07	601535.89	0.94
264808.55	601534.63	0.85
264819.41	601535.84	1.22
264828.68	601533.24	1.39
264828.00	601545.94	1.19
264818.58	601545.70	0.96
264808.20	601545.32	0.14
264797.83	601546.28	0.99
264787.80	601547.11	1.11
264779.28	601546.94	1.17

Easting	Northing	Peat Depth (m)
264767.40	601547.72	0.77
264758.45	601548.06	0.82
264748.83	601547.17	0.47
264738.63	601548.61	0.68
264728.49	601549.35	1.28
264739.33	601559.43	0.66
264751.27	601557.84	0.75
264760.59	601556.96	0.7
264770.06	601557.77	1.16
264780.06	601557.50	1.14
264790.24	601556.07	1.17
264800.32	601556.79	0.97
264809.72	601556.35	0.94
264819.55	601554.92	1.04
264829.70	601553.25	0.94
264827.85	601525.25	0.64
264818.80	601525.84	1.19
264806.95	601524.88	1.23
264795.99	601526.39	0.92
264787.60	601527.31	1.03
264776.67	601527.29	0.82
264767.18	601527.55	0.94
264756.82	601528.33	0.47
264747.31	601527.39	0.76
264737.12	601528.30	0.62
264055.08	601349.55	0.37
264053.53	601250.52	0.21
264054.96	601148.98	0.45
264054.41	601049.00	0.27
264055.01	600949.10	0.17
263955.59	600848.91	0.18
263954.78	600951.18	0.65
263956.02	601050.02	0.21
263954.82	601150.65	0.24
263955.19	601252.08	0.29
263956.05	601350.09	0.96
263955.91	601450.89	0.37
263954.90	601552.10	0.61
263854.61	601549.45	0.5
263858.27	601349.33	0.58
263855.28	601250.05	0.67
263854.57	601150.27	0.66
263856.90	601049.43	0.41
263856.57	600948.25	0.14
263856.07	600850.21	0.26
263755.11	600851.18	0.18
263753.77	600949.91	0.2
263754.44	601048.62	0.31
263755.34	601151.93	0.2

Easting	Northing	Peat Depth (m)
263755.76	601250.79	0.94
263755.03	601351.17	0.73
263755.38	601550.37	0.13
263650.69	601642.12	1.1
263654.98	601549.66	0.55
263652.97	601450.26	0.52
263654.97	601348.63	0.78
263654.87	601249.60	0.3
263654.37	601148.90	0.27
263655.06	601049.21	0.28
263554.03	601050.55	0.45
263555.17	601151.00	0.24
263556.01	601249.83	0.52
263555.27	601350.72	0.98
263555.69	601551.48	2
263455.04	601548.97	1.13
263453.88	601448.35	2.63
263451.25	601349.96	0.38
263454.28	601249.31	0.84
263452.26	601152.11	0.19
263354.94	601250.56	0.44
263356.20	601351.21	1.28
263356.78	601449.42	0.54
263355.23	601551.53	2.17
263255.68	601449.03	0.6
263254.84	601349.37	0.74
263255.92	601248.57	0.78
266800.24	600812.63	0
266812.41	600763.95	0
266821.41	600714.21	0
266838.87	600668.17	0
266815.59	600636.95	0
266767.44	600618.96	0
267652.61	599624.00	0
267669.94	599629.12	0.1
267688.19	599639.95	0.5
267706.45	599645.99	0.3
267729.46	599666.21	0.2
267710.75	599658.58	0.1
267693.46	599649.56	0.35
267673.66	599642.61	0.2
267656.33	599634.95	0
267642.32	599641.16	0.1
267662.05	599649.10	0.2
267679.54	599654.45	0
267699.07	599665.11	0.1
267717.90	599674.85	0.15
267723.48	599684.61	0.7
267703.63	599677.67	0.1

Easting	Northing	Peat Depth (m)
267684.43	599669.22	0
267667.55	599660.32	0.6
267649.82	599652.96	0.3
267635.14	599656.67	0.4
267640.46	599674.16	0.2
267653.17	599663.12	0.4
267659.01	599679.10	0.7
267670.91	599675.68	0.4
267677.64	599687.89	0.3
267690.29	599681.85	0.3
267692.81	599694.31	0
267709.12	599688.62	0.2
267708.86	599701.38	0.4
267916.22	599834.27	0.2
267938.53	599824.51	0.4
267961.45	599813.54	1.2
267993.84	599829.34	1.6
267982.12	599859.53	0.1
267958.80	599872.10	0.3
267948.42	599846.58	0.1
267926.40	599856.70	0.7
267902.23	599867.02	0.95
267936.19	599882.02	0.8
267969.73	599892.94	0.2
268043.18	599916.99	0.95
268295.26	600194.59	1.5
268301.13	600217.41	1.15
268324.86	600212.79	2.1
268331.45	600238.80	2.1
268356.29	600232.14	1.4
268337.68	600262.63	3.1
268307.30	600244.73	1.1
268275.10	600238.43	0.8
268254.75	600260.70	1.4
268283.19	600275.59	0.45
268319.76	600293.84	2.2
268308.24	600300.42	1.4
268328.55	600284.84	2.1
268350.54	600313.02	2.1
268360.28	600302.21	3
268345.09	600323.23	2
268397.23	600335.30	1.5
268396.33	600326.45	1.4
268396.55	600317.31	1.3
268447.81	600323.38	1.9
268445.89	600334.00	1.5
268441.79	600343.75	0.6
268493.08	600337.49	0.8
268540.67	600342.85	1.4

Easting	Northing	Peat Depth (m)
268536.83	600351.32	2.2
268544.81	600330.31	0.2
268593.35	600360.31	0.2
268635.98	600381.99	0.65
268603.58	599833.94	1.9
268568.77	599826.10	2
268581.68	599846.22	1.75
268594.84	599867.16	1.85
268585.66	599900.54	1.4
268559.39	599861.45	1.3
268010.04	600278.89	0.65
268013.85	600327.32	0.5
268017.82	600377.73	0.7
268024.05	600427.53	0
268028.04	600476.99	0
268030.09	600527.41	0.8
268020.00	600522.00	0.45
267995.00	600547.00	0.2
268020.00	600597.00	0
268045.00	600572.00	0.6
268070.00	600547.00	0.9
268045.00	600522.00	0.35
268020.00	600547.00	0.7
267995.00	600572.00	0.6
267970.00	600547.00	0.9
267995.00	600522.00	1.7
268020.00	600497.00	0.6
268045.00	600547.00	0.4
268020.00	600572.00	0.7
268686.38	600402.22	0.4
268671.45	600448.77	0
268658.39	600495.82	0.75
268647.91	600544.69	0.6
268639.80	600593.61	0.3
268631.35	600643.09	0.9
268618.18	600690.01	0.85
268573.39	600717.69	0.7
268555.70	600687.08	0.6
268597.54	600724.15	0.7
268616.93	600651.70	0.8
268604.00	600700.00	0.85
268610.46	600675.85	0.9
268621.69	600730.61	1.4
268591.08	600748.30	0.65
268586.31	600669.39	0.9
268579.85	600693.54	0
268704.87	600355.02	0.85
268730.48	600310.12	0.75
268743.34	600260.28	0.85

Easting	Northing	Peat Depth (m)
268827.07	600277.09	1.4
268862.08	600282.01	0.9
268836.91	600207.07	0.9
268897.09	600286.93	0.9
268831.99	600242.08	0.95
268847.04	600262.05	1.05
268867.00	600247.00	0.55
268269.01	599066.71	0
268308.52	599097.63	0.3
268348.19	599127.36	0.3
268389.41	599157.91	0.7
268431.01	599188.21	0.9
268474.28	599214.09	0.8
268521.70	599231.07	0.85
268569.34	599246.81	0.2
268617.88	599262.61	0.3
267962.55	600214.62	1.55
267937.71	600217.37	1.3
267987.40	600211.87	1
267959.81	600189.77	0.9
267981.90	600162.17	1.25
267992.90	600261.57	1.5
268015.00	600233.97	1.15
268009.50	600184.27	0.45
267965.30	600239.47	1.25
268037.10	600206.37	1.1
267984.65	600187.02	1.35
268012.25	600209.12	1
268320.29	598977.87	0.8
268315.68	598986.91	0.7
268310.53	598995.23	0.9
268266.00	598980.41	0.8
268268.14	598970.33	0.9
268270.07	598960.43	0.7
268254.53	598947.53	1
268216.71	598965.92	0.4
268219.12	598975.50	0.9
268221.96	598985.62	0.8
268203.99	598994.32	0.6
268194.89	598998.12	1
268185.47	599002.11	0.3
268176.27	599006.28	0.7
268166.95	599010.09	0.9
268157.84	599013.89	0.5
268147.67	599017.53	0.6
268138.54	599020.40	0.5
268129.26	599025.50	0.85
268121.76	599029.81	0.5
268111.56	599032.71	0.4

Easting	Northing	Peat Depth (m)
268101.79	599035.60	0.9
268092.58	599039.22	0.25
268083.47	599043.01	0.5
268074.59	599047.18	0.9
268064.33	599051.38	0.9
268045.45	599058.07	0.75
268037.28	599061.28	0.8
268040.64	599070.83	0.7
268050.40	599067.76	0.65
268058.98	599063.98	0.7
268068.49	599059.61	0.7
268062.86	599073.14	1
268072.19	599069.89	0.25
268081.04	599064.62	0.7
268090.82	599061.91	0.7
268105.67	599044.77	0.85
268095.93	599048.58	0.2
268087.15	599052.74	0.4
268077.30	599056.56	0.55
268023.46	599056.13	0.3
268015.93	599038.16	0.4
268012.03	599028.26	0.3
268014.13	599006.29	0.65
268028.25	598989.35	1.2
268038.10	598985.72	0.6
268047.32	598982.10	0.5
268057.07	598978.47	0.4
268079.37	598980.22	0.5
268070.05	598984.02	0.4
268061.14	598987.26	0.3
268052.02	598990.50	0.4
268042.39	598994.69	0.5
268032.44	598998.51	0.6
268017.80	599015.83	0.6
268027.42	599011.28	0.6
268036.54	599008.04	0.8
268045.95	599003.86	0.5
268054.73	598999.51	0.75
268064.61	598996.99	0.7
268073.31	598993.58	0.8
268082.50	598989.22	0.25
268096.32	598994.19	0.45
268086.07	598998.77	0.85
268076.56	599003.13	0.75
268068.69	599005.96	0.5
268059.27	599009.77	0.6
268049.20	599013.23	0.55
268039.87	599016.66	0.3
268031.01	599021.75	0.6

Easting	Northing	Peat Depth (m)
268034.86	599029.99	0.8
268025.87	599033.97	0.94
268029.21	599042.96	0.8
268038.95	599038.96	0.85
268052.27	599045.24	1.2
268123.14	599005.08	1.5
268127.42	599013.49	1.05
268107.56	599022.81	0.85
268098.14	599026.62	0.9
268088.49	599030.06	0.75
268079.17	599033.86	0.3
268069.95	599037.29	1.1
268061.17	599041.45	0.7
268057.49	599031.73	1.6
268060.18	599025.89	1.3
268066.18	599028.31	1.4
268075.82	599024.68	0.6
268085.15	599021.25	0.94
268093.82	599016.91	0.85
268103.48	599013.84	1
268109.75	599004.00	1
268099.70	599004.30	1.25
268090.27	599008.11	0.75
268081.04	599011.16	0.6
268072.16	599015.51	0.8
268062.84	599019.32	0.9
268032.88	599052.32	0.75
268053.29	599022.39	0.85
268172.34	598995.27	0.94
268168.26	598986.48	0.94
268308.52	599671.79	1.8
268304.21	599683.80	1.7
268300.96	599692.06	1.6
268262.86	599657.75	1.35
268253.54	599647.45	1.5
268257.81	599666.07	1.55
268253.61	599674.54	1.6
268205.18	599656.50	0.25
268211.32	599645.74	0.2
268215.92	599636.50	0.2
268171.17	599613.90	0.5
268166.56	599622.94	0.75
268162.19	599632.54	0.7
268116.52	599618.49	1.05
268106.96	599617.48	1.45
268096.71	599615.00	1.35
268086.30	599614.01	1.8
268076.10	599613.02	1.5
268066.79	599610.14	1.85

Easting	Northing	Peat Depth (m)
268056.72	599609.88	1.35
268047.97	599607.92	1.7
268049.60	599598.77	1.65
268039.54	599598.89	0.4
268029.35	599598.08	0.6
268019.22	599596.15	0.45
268009.22	599594.78	0.55
268000.17	599593.38	0.8
267989.75	599592.02	0.4
267979.96	599590.64	0.5
267970.92	599589.62	0.5
267960.27	599587.89	0.8
267951.14	599587.24	0.75
267940.76	599583.83	1.3
267973.81	599580.06	0.25
267975.84	599569.98	0.75
268022.85	599586.40	0.35
268039.93	599587.18	0.8
268050.13	599587.99	0.35
268060.15	599589.92	0.45
268070.36	599591.10	0.9
268079.63	599593.05	1.2
268088.68	599594.45	1.6
268099.32	599595.99	1.6
268109.22	599597.55	1.7
268119.22	599598.74	0.35
268128.26	599599.96	0.15
268118.04	599608.98	0.25
268107.71	599607.25	1.45
268098.13	599605.86	1.6
268088.57	599605.04	1.55
268078.96	599602.54	1.5
268068.99	599602.28	0.75
268058.76	599600.36	1
268062.17	599579.47	0.8
268071.76	599581.41	0.35
268080.84	599583.92	1.2
268091.02	599584.18	1.5
268100.21	599586.69	1.6
268110.50	599586.94	1.55
268120.73	599588.86	0.6
267737.96	599531.06	0.45
267789.39	599535.65	0.75
267785.95	599544.66	0.1
267782.62	599553.85	0.5
267821.20	599586.29	0.75
267828.21	599579.59	0.7
267831.92	599569.08	0.85
267833.56	599559.94	0.94

Easting	Northing	Peat Depth (m)
267835.58	599549.67	1.8
267854.06	599547.45	0.94
267876.45	599555.69	0.7
267925.72	599562.57	1.5
268024.79	599576.69	0.35
268042.07	599577.10	0.45
268051.43	599578.12	0.45
268053.49	599569.15	0.3
268063.06	599570.35	0.82
268072.40	599570.81	1.15
268082.43	599573.30	1.3
268087.26	599578.72	1.35
268092.33	599574.67	1.15
268102.24	599576.60	1.1
268112.55	599577.60	1.85
268122.13	599579.17	1.65
268132.35	599580.53	1.85
268130.74	599590.79	1
268133.76	599571.02	0.3
268123.96	599569.46	0.94
268115.03	599568.24	0.9
268104.06	599566.53	0.75
268094.47	599564.77	0.9
268084.38	599563.96	1.15
268074.56	599561.65	1.55
268064.67	599560.46	0.75
268054.76	599558.53	0.3
268045.17	599556.78	0.2
268042.72	599566.87	0.4
268033.70	599569.92	0.3
268054.64	599547.40	0.3
268066.19	599550.95	0.6
268075.95	599551.40	0.45
268085.24	599553.54	1.25
268095.64	599554.34	0.9
268105.35	599556.47	0.6
268114.72	599557.86	0.5
268126.09	599559.19	0.55
268126.76	599549.52	0.45
268117.08	599548.32	0.55
268106.97	599546.95	0.5
268097.40	599545.75	0.8
268087.48	599543.45	0.9
268077.89	599541.70	0.65
268067.05	599540.72	0.5
268057.68	599539.14	0.15
268079.09	599532.19	0.94
268088.90	599534.13	0.94
268098.68	599535.32	0.45

Easting	Northing	Peat Depth (m)
268108.46	599536.33	0.3
268095.44	599625.62	1.9
268084.50	599624.65	1.7
268075.17	599621.21	1.7
268064.03	599620.62	1.6
267924.20	599582.84	1.94
267923.01	599571.19	1.65
267874.61	599565.21	1
267873.34	599575.64	1.6
267872.75	599605.54	1.65
267866.35	599615.01	1.85
267860.33	599622.61	1.7
267911.04	599642.26	1.9
267903.81	599648.60	1.8
267896.08	599656.07	2.5
267930.32	599691.79	3.2
267938.58	599684.68	3.7
267946.68	599679.05	3
267969.15	599725.53	3.6
267960.32	599728.02	3.7
267951.70	599733.66	3.8
267919.57	599764.87	2.9
267923.32	599773.48	2.6
267927.21	599783.01	2.8
267967.33	599778.10	2.7
267977.33	599775.95	2.4
267986.52	599771.41	1.4
267977.43	599825.32	1.5
267987.07	599825.40	1.5
267996.64	599822.89	1.65
267979.83	599874.06	0.8
267989.80	599874.31	0.55
268000.73	599874.73	0.9
267999.55	599923.95	0.8
267989.72	599924.99	0.85
268060.86	600537.38	0.9
268058.74	600526.67	0.85
268057.20	600517.63	1
268054.89	600507.67	0.7
268041.63	600489.32	0.6
268041.73	600499.53	0.8
268044.69	600510.02	0.75
268048.23	600529.22	0.88
268038.57	600532.29	1.15
268036.36	600522.15	0.4
268034.49	600512.55	0.82
268032.69	600502.02	0.9
268030.71	600492.43	0.78
268030.44	600483.53	0.5

Easting	Northing	Peat Depth (m)
268028.66	600473.38	0.45
268027.33	600464.32	0.35
268025.02	600454.37	0.58
268023.66	600444.39	0.45
268021.15	600434.81	0.45
268020.12	600425.01	0.7
268017.38	600414.88	0.85
268015.92	600405.27	0.5
268014.25	600395.49	1.25
268011.84	600385.54	0.6
268007.12	600422.61	0.42
267996.95	600426.07	0.9
268015.91	600472.27	0.88
268018.51	600484.82	0.85
268022.35	600503.45	1.1
268024.57	600513.96	1.55
268026.45	600523.56	1.6
268029.38	600533.12	1.15
268031.28	600543.64	1.8
268033.05	600553.05	1.5
268035.55	600562.26	1.1
268037.76	600572.40	0.8
268045.79	600561.21	1
268055.37	600559.25	1
268053.16	600549.11	1.35
268050.85	600539.16	0.96
268040.96	600541.31	0.98
268042.51	600550.73	1.05
268025.13	600564.61	1.15
268023.69	600555.56	1.45
268018.65	600535.67	0.8
268013.04	600532.31	0.8
268017.19	600525.87	1.7
268015.47	600517.94	1.55
268013.23	600506.69	1.25
268011.22	600496.17	1.85
268008.61	600486.78	0.98
268006.02	600474.61	0.96
267998.94	600489.48	1.35
268000.69	600498.34	1.85
268003.43	600508.28	1.6
268004.35	600517.90	1.25
268007.40	600527.84	1.94
268009.29	600537.99	0.8
268011.49	600547.76	0.95
268013.47	600557.16	1.35
268016.00	600567.48	0.94
268017.76	600576.90	0.88
268028.29	600574.54	1.35

Easting	Northing	Peat Depth (m)
268008.30	600579.22	1.45
268006.22	600569.82	1
268004.66	600560.21	1.02
268002.02	600550.08	1.25
267999.51	600540.32	0.8
267997.63	600530.73	0.35
267993.31	600510.07	1.6
267990.93	600501.23	1.94
267988.62	600491.46	2.5
267981.44	600503.00	2.1
267983.32	600512.59	1.85
267985.20	600522.19	1.65
267987.49	600531.58	1.55
267989.82	600542.09	1.88
267992.22	600551.67	1.25
267993.98	600560.90	1.35
267987.06	600573.91	2.1
267985.16	600563.76	1.94
267982.77	600554.55	1.8
267980.25	600544.61	1.94
267978.26	600534.64	1.85
267975.64	600524.89	1.7
267973.21	600514.57	1.92
267971.44	600505.15	1.96
267966.49	600527.39	0.52
267968.68	600536.79	0.96
267972.64	600555.97	1.15
267987.42	600376.61	0.75
267997.18	600373.72	1.92
268006.67	600372.14	1.25
267978.93	600326.38	0.92
267988.83	600324.42	0.92
267998.45	600323.76	0.94
267978.00	600174.78	1.4
267987.63	600174.31	1.65
267997.79	600174.00	1.7
267998.30	600123.50	1.92
267988.37	600124.54	1.75
267977.99	600124.67	1.7
267979.35	600074.33	0.3
267988.58	600074.80	0.92
267998.39	600073.39	0.85
267999.47	600024.17	0.7
267989.10	600024.67	0.45
267979.56	600024.77	0.35
267965.10	600022.79	0.35
267955.26	600019.74	0.32
267947.97	600013.28	1.92
267979.45	599974.85	0.75

Easting	Northing	Peat Depth (m)
267989.20	599974.74	0.62
267999.34	599973.88	0.65
267976.00	599951.56	0.9
267926.56	600059.39	0.9
267934.59	600065.64	1.3
267944.84	600068.12	0.87
267922.90	600114.25	3.1
267913.27	600111.01	1.8
267904.75	600106.07	1.65
267877.92	600144.17	1.6
267884.61	600151.77	1.65
267893.97	600156.32	1.35
267855.51	600195.51	1.38
267849.95	600186.77	1.07
267843.80	600179.34	0.96
267801.41	600193.05	1.32
267802.89	600203.58	1.08
267805.07	600212.98	1.28
267753.08	600217.50	0.52
267753.01	600208.04	0.3
267753.86	600197.44	0.5
267706.69	600193.09	0.85
267703.68	600202.28	1.05
267701.14	600212.93	0.85
267653.33	600187.27	0.88
267659.69	600180.21	0.87
267667.00	600173.31	0.62
267754.59	600147.30	0.6
267638.58	600137.04	0.3
267629.37	600140.66	0.35
267619.61	600143.73	0.4
267619.22	600091.96	0.92
267628.73	600091.12	0.45
267607.15	600074.32	0.6
267605.59	600054.14	0.88
267603.51	600034.15	0.22
267601.13	600014.74	1.75
267599.13	599994.20	1.98
267614.35	600042.37	0.07
267624.39	600041.51	0.28
267619.08	599991.56	1.9
267608.73	599992.61	1.85
267625.00	599984.14	1.65
267644.56	599964.81	0.55
267641.75	599945.41	0.55
267638.60	599925.27	0.75
267658.76	599922.44	0.8
267656.17	599903.40	1.1
267633.39	599885.71	0.95

Easting	Northing	Peat Depth (m)
267636.63	599905.29	1.38
267618.98	599927.90	0.89
267621.69	599947.68	0.8
267624.63	599968.19	1.05
267604.87	599969.90	1.78
267602.40	599951.04	1.22
267599.56	599930.52	0.68
267596.86	599911.30	0.23
267616.38	599908.49	1.32
267613.57	599888.90	0.62
267593.62	599891.35	0.48
267576.68	599913.20	0.18
267579.30	599933.17	0.48
267581.91	599953.32	1.42
267727.82	599719.93	0.35
267730.51	599710.57	0.46
267734.36	599700.99	0.8
267754.28	599747.16	0.25
267775.81	599740.77	0.72
267778.17	599731.23	1.07
267781.71	599722.03	0.62
267828.73	599742.53	0.23
267824.97	599751.18	0.42
267822.61	599760.90	0.48
267870.06	599781.75	0.32
267873.06	599772.20	0.17
267876.50	599763.00	0.85
267854.74	599846.80	0.75
267908.29	599844.83	0.8
267910.71	599854.96	0.94
267913.43	599864.53	0.92
267915.95	599874.11	0.92
267917.94	599884.07	1.05
267920.78	599894.01	0.62
267923.37	599902.65	0.88
267926.43	599912.96	0.84
267927.99	599922.75	0.96
267931.34	599931.93	0.68
267933.24	599942.45	0.89
267942.90	599939.56	0.82
267952.67	599936.49	0.83
267962.57	599934.70	0.48
267972.34	599931.81	0.64
267981.69	599929.12	0.33
267979.92	599919.52	0.45
267977.09	599909.96	0.32
267974.57	599900.01	0.18
267969.56	599881.23	0.27
267967.15	599871.65	0.18

Easting	Northing	Peat Depth (m)
267964.33	599862.08	0.06
267959.19	599842.75	0.89
267956.57	599832.99	0.55
267947.42	599835.31	0.76
267937.00	599837.47	0.38
267939.74	599847.60	0.41
267942.87	599856.78	0.31
267952.44	599854.46	0.22
267955.16	599863.84	0.34
267959.03	599883.40	0.42
267962.60	599893.13	0.43
267964.69	599902.72	0.32
267967.20	599912.11	0.27
267969.71	599921.87	0.18
267959.84	599924.76	0.21
267949.32	599927.49	0.89
267940.80	599929.42	0.8
267937.68	599920.60	0.88
267947.88	599918.07	0.71
267957.22	599915.19	0.32
267954.71	599905.43	0.34
267945.56	599907.74	0.68
267935.89	599910.45	0.83
267933.28	599901.06	0.87
267943.17	599898.72	0.87
267952.62	599896.03	0.45
267950.00	599886.08	0.48
267940.42	599888.41	0.62
267930.11	599890.76	0.89
267928.35	599881.35	0.86
267947.59	599876.32	0.54
267944.44	599866.76	0.82
267935.18	599868.89	0.9
267925.20	599871.79	1.06
267923.00	599862.02	0.91
267932.80	599860.06	0.9
267930.05	599849.74	0.74
267920.69	599852.06	0.76
267917.77	599842.87	0.7
267927.86	599840.34	0.31
267854.16	599947.96	0.14
267690.55	599515.40	0.12
267642.53	599500.50	0.18
267595.36	599485.77	0.22
267576.36	599470.56	0.05
267590.12	599466.62	0.09
267607.56	599475.75	0.14
267625.44	599485.24	0.08
267640.43	599479.78	0.01

Easting	Northing	Peat Depth (m)
267658.19	599489.09	0.31
267653.97	599475.48	0
267662.67	599458.14	0.06
267658.43	599443.98	0.17
267654.39	599447.25	0.17
267645.42	599448.27	0.35
267631.77	599452.39	0.22
267649.94	599461.31	0
267654.32	599430.74	0.48
267640.88	599434.67	0.16
267627.65	599438.77	0.18
267613.90	599443.27	0.09
267618.01	599456.70	0.69
267635.69	599466.56	0.08
267622.46	599470.67	0.07
267605.11	599461.16	0.39
267600.48	599447.94	0.18
267595.83	599434.34	0.06
267582.62	599438.82	0.07
267569.16	599442.38	0.21
267553.50	599446.75	0.12
267547.76	599470.86	0.03
267666.98	599471.38	0.52
267671.21	599484.98	0.06
267676.16	599498.20	0.23
267688.85	599493.92	0.16
267693.06	599507.16	0.33
264217.40	602050.95	0.11
264236.82	602058.89	0.28
264254.52	602066.52	0.1
264280.80	602056.43	0.11
264262.63	602047.52	0.13
264244.07	602039.92	0.22
264225.94	602032.50	0.09
264207.70	602024.71	0.25
264214.98	602006.48	0.45
264223.09	601987.86	0.35
264247.45	601967.06	0.88
264249.67	601977.39	0.84
264241.22	601995.47	0.3
264233.53	602014.08	0.25
264251.68	602022.24	0.42
264260.01	602003.61	0.45
264268.23	601984.99	0.36
264275.20	601970.85	0.42
264286.26	601992.78	0.12
264278.35	602011.22	0.32
264270.13	602029.66	0.34
264289.12	602037.80	0.16

Easting	Northing	Peat Depth (m)
264296.50	602019.38	0.18
264263.24	601932.98	0.4
264279.45	601926.36	0.28
264272.00	601914.71	0.13
264280.02	601896.46	0.3
264289.10	601878.55	0.74
264301.02	601880.23	0.6
264322.30	601835.21	0.22
264360.05	601805.47	0.16
264353.23	601797.14	0.28
264349.97	601787.59	0.27
264396.84	601768.71	0.88
264399.89	601778.45	0.78
264404.74	601788.14	0.76
264447.42	601763.63	0.4
264495.41	601750.46	0.52
264545.25	601745.41	0.45
264595.02	601748.34	0.32
263644.26	601073.56	0.17
263664.49	601076.65	0.03
263683.96	601079.39	0.22
263706.54	601062.73	0.25
263687.26	601059.43	0.22
263667.05	601056.71	0.12
263647.04	601053.80	0.17
263627.58	601051.25	0.17
263630.67	601031.29	0.07
263633.25	601011.91	0.11
263650.45	601033.84	0.03
263650.15	601034.22	0.11
263670.05	601037.31	0.18
263690.56	601039.28	0.12
263710.06	601043.13	0.64
263692.61	601019.91	0.22
263673.25	601017.36	0.28
263653.45	601014.07	0.07
263655.92	600994.69	0.04
263676.11	600996.67	0.07
263695.51	601000.52	0.09
263712.40	601022.83	0.28
263726.41	601044.30	0.16
263744.50	601064.16	0.11
263730.35	601072.21	0.6
263749.94	601075.50	0.13
263769.61	601078.05	0.09
263789.12	601081.90	0.04
263793.90	601071.92	0.06
263809.32	601084.25	0.7
263842.89	601080.43	0.96

Easting	Northing	Peat Depth (m)
263894.09	601092.03	0.11
263887.98	601099.83	0.12
263882.74	601108.53	0.04
263929.03	601129.19	0.88
263968.83	601159.15	0.16
263994.90	601201.04	0.7
264011.91	601247.84	0.13
264029.77	601294.44	0.22
264053.29	601339.37	0.15
264083.93	601378.15	0.42
264110.50	601422.62	0.48
264117.27	601415.36	0.42
264124.53	601406.97	0.33
264169.03	601386.67	0.34
264172.82	601396.02	0.17
264176.48	601405.00	0.82
264206.21	601393.51	0.35
264215.20	601389.52	0.06
264224.62	601385.89	0.9
264233.82	601382.08	0.62
264242.82	601378.28	0.9
264252.54	601374.27	0.9
264261.54	601370.65	0.32
264270.21	601366.67	0.76
264280.05	601362.85	0.84
264288.82	601358.49	0.08
264298.44	601354.67	0.6
264308.05	601350.29	1.25
264311.75	601360.39	0.92
264320.64	601356.40	1.18
264330.78	601352.19	0.62
264339.36	601348.59	1.08
264334.14	601361.56	1.3
264343.03	601357.94	1.12
264361.76	601350.32	0.94
264348.77	601344.77	0.78
264358.51	601340.95	1.02
264367.39	601337.15	0.9
264376.70	601333.34	0.9
264372.83	601324.55	0.8
264363.61	601327.62	0.12
264354.21	601331.99	0.91
264345.19	601335.05	0.89
264336.10	601339.04	1.45
264326.68	601342.67	1.22
264317.26	601346.67	1.15
264313.40	601338.07	1.19
264310.13	601328.14	0.83
264306.35	601318.98	0.67

Easting	Northing	Peat Depth (m)
264302.15	601309.64	0.81
264298.47	601300.29	0.72
264294.59	601291.31	0.89
264300.02	601278.34	0.61
264309.44	601274.71	0.45
264318.32	601270.54	0.38
264327.64	601267.10	0.07
264349.93	601268.46	0.28
264340.94	601272.44	0.32
264331.84	601276.25	0.11
264322.63	601279.87	0.46
264313.32	601283.69	0.58
264304.11	601287.49	0.35
264307.78	601296.48	0.78
264316.99	601292.85	0.8
264325.98	601289.05	0.45
264335.82	601285.22	0.32
264344.60	601281.43	0.27
264354.13	601277.79	0.22
264366.70	601283.53	0.28
264357.81	601287.15	0.16
264348.40	601291.15	0.52
264339.39	601294.58	0.61
264329.76	601298.21	0.3
264320.87	601302.01	0.69
264311.04	601306.21	0.32
264315.44	601314.99	0.7
264324.33	601311.19	0.54
264333.55	601307.75	0.95
264342.96	601303.75	0.94
264352.16	601299.75	0.78
264361.37	601296.13	0.63
264370.57	601292.32	0.6
264374.46	601301.48	0.62
264365.47	601305.66	0.55
264356.26	601309.28	1.5
264346.75	601313.28	0.92
264337.33	601317.10	0.93
264330.67	601314.15	0.8
264328.54	601320.71	0.72
264318.92	601324.72	0.84
264323.02	601333.87	0.44
264332.21	601329.69	0.87
264341.54	601326.44	1.15
264350.52	601322.45	0.52
264359.72	601318.45	0.89
264368.95	601315.39	0.78
264378.45	601310.83	0.33
264285.26	601294.57	1.12

Easting	Northing	Peat Depth (m)
264289.28	601304.47	0.9
264292.94	601313.45	0.78
264283.31	601317.09	0.72
264287.40	601326.24	0.48
264296.41	601322.81	0.62
264300.51	601332.15	0.78
264290.98	601335.78	0.73
264304.39	601341.31	0.92
264294.77	601345.32	1.11
264265.37	601357.17	0.34
264261.39	601348.39	0.32
264214.95	601367.63	0.6
264219.05	601376.97	0.2
264157.89	601444.74	0.77
264145.47	601460.90	0.34
264194.23	601475.73	1.12
264189.10	601484.80	0.94
264182.29	601497.44	0.52
263644.78	601368.47	0.06
263635.02	601368.03	0.62
263624.66	601368.72	0.32
263614.79	601368.10	1.82
263604.74	601368.41	0.45
263594.25	601368.55	1.54
263584.71	601368.10	1.3
263574.65	601368.22	0.87
263564.58	601368.16	0.91
263554.64	601368.66	1.71
263544.36	601368.42	0.72
263534.60	601367.97	0.31
263524.76	601368.28	1.08
263514.48	601368.22	1.15
263504.75	601368.52	0.25
263495.22	601368.63	0.18
263484.51	601368.41	0.32
263474.66	601368.34	1.07
263454.75	601368.40	1
263435.25	601368.07	0.58
263414.59	601367.97	1.65
263404.72	601377.74	1.07
263424.54	601378.05	1.38
263444.47	601378.55	0.32
263464.79	601378.11	0.7
263485.13	601378.04	0.68
263504.09	601378.20	0.96
263525.29	601378.47	0.7
263544.34	601378.07	0.42
263564.79	601378.18	1.1
263584.60	601378.31	1.85

Easting	Northing	Peat Depth (m)
263604.84	601378.61	0.4
263624.66	601378.93	0.3
263644.76	601378.31	1.48
263654.29	601388.22	0.18
263635.01	601388.26	0.1
263614.15	601388.53	1.9
263594.98	601388.57	0.72
263575.27	601388.25	0.22
263554.61	601388.33	0.96
263534.68	601387.83	0.36
263514.98	601387.70	1.88
263495.08	601388.31	0.2
263474.52	601387.83	1
263454.85	601388.81	0.7
263434.93	601388.68	1.1
263414.46	601387.83	1.9
263395.21	601388.80	1.18
263404.72	601398.34	1.78
263424.74	601398.28	1.35
263444.97	601398.21	1
263465.00	601398.52	0.75
263485.00	601398.09	2
263504.39	601398.05	0.5
263524.53	601398.54	0.4
263544.56	601399.03	0.3
263564.35	601398.24	0.4
263584.69	601398.54	1
263604.81	601398.10	0.78
263624.94	601398.41	0.6
263644.32	601398.37	0.33
263664.98	601398.29	0.63
263654.69	601408.26	0.58
263634.77	601408.13	1
263614.87	601408.37	0.12
263595.16	601408.05	0.14
263574.61	601408.32	0.45
263554.70	601408.19	0.25
263534.79	601408.43	0.32
263515.08	601408.30	0.76
263494.84	601407.81	0.73
263474.31	601408.63	0.82
263454.91	601408.11	0.2
263435.34	601408.72	1
268769.62	599152.90	0.31
268758.54	599147.47	0.31
268755.24	599146.83	0.36
268750.91	599143.99	0.29
268742.21	599139.79	0.33
268719.61	599138.98	0.45

Easting	Northing	Peat Depth (m)
268727.61	599144.31	0.33
268737.17	599148.66	0.34
268745.86	599152.12	0.38
268755.64	599156.65	0.33
268764.91	599161.95	0.29
268774.14	599166.13	0.33
268781.71	599171.10	0.31
268778.35	599179.18	0.29
268768.60	599175.76	0.28
268760.09	599171.00	0.36
268750.32	599166.65	0.41
268741.80	599161.70	0.32
268733.52	599157.87	0.43
268723.21	599152.98	0.25
268715.46	599149.12	0.25
268701.03	599151.96	0.47
268711.28	599158.34	0.18
268719.67	599162.36	0.33
268728.71	599167.10	0.26
268737.10	599171.12	0.14
268745.69	599174.95	0.29
268755.35	599179.12	0.39
268763.66	599184.26	0.28
268772.98	599187.69	0.37
268782.87	599192.41	0.37
268778.29	599202.38	0.31
268768.61	599197.47	0.36
268759.02	599192.19	0.22
268751.48	599188.14	0.27
268742.88	599183.76	0.33
268733.24	599180.33	0.38
268723.96	599174.67	0.32
268714.41	599170.68	0.32
268706.76	599166.46	0.42
268698.03	599161.70	0.43
268687.94	599160.89	0.2
268673.55	599161.69	0.26
268692.28	599171.34	0.29
268702.15	599175.50	0.3
268710.42	599179.34	0.38
268719.16	599184.65	0.43
268729.04	599188.81	0.51
268734.94	599187.71	0.3
268737.85	599193.00	0.29
268746.35	599197.39	0.22
268755.92	599201.93	0.27
268763.99	599206.15	0.27
268773.56	599210.69	0.4
268768.33	599220.12	0.22

Easting	Northing	Peat Depth (m)
268759.69	599214.63	0.42
268751.74	599210.96	0.23
268741.32	599206.45	0.24
268733.16	599202.61	0.23
268723.49	599198.25	0.53
268715.38	599192.74	0.5
268706.59	599189.29	0.27
268697.66	599184.73	0.37
268688.19	599180.00	0.37
268594.68	599142.69	0.51
268603.20	599147.82	0.38
268612.11	599151.63	0.75
268621.07	599157.12	0.35
268629.99	599161.50	0.22
268637.88	599166.46	0.34
268647.32	599170.45	0.17
268655.84	599175.58	0.49
268668.83	599170.37	0.39
268665.08	599179.57	0.64
268673.57	599183.77	0.71
268683.17	599189.24	0.46
268693.23	599192.66	0.48
268701.13	599198.17	0.39
268710.44	599201.24	0.75
268719.27	599206.17	0.76
268729.27	599211.07	0.4
268737.68	599215.65	0.32
268746.62	599220.58	0.18
268756.39	599225.12	0.38
268751.32	599232.51	0.42
268741.99	599228.88	0.33
268732.93	599223.59	0.49
268725.08	599219.55	0.37
268714.58	599215.96	0.6
268706.49	599211.19	0.48
268696.61	599206.48	0.36
268688.84	599201.88	0.38
268702.73	599220.03	0.55
268711.04	599225.16	0.72
268719.86	599229.54	0.85
268728.90	599234.28	0.77
268752.52	599633.73	0.54
268744.50	599627.84	0.51
268737.75	599621.73	1.74
268730.03	599614.91	0.56
268707.87	599610.93	0.48
268715.68	599617.19	0.54
268723.47	599622.34	0.24
268731.51	599629.15	0.29

Easting	Northing	Peat Depth (m)
268738.40	599636.56	0.67
268746.52	599642.26	0.92
268762.36	599654.78	0.62
268755.40	599662.97	1.21
268747.15	599656.53	0.68
268740.59	599649.49	0.5
268732.34	599642.86	0.37
268724.21	599636.61	0.28
268717.67	599630.49	0.35
268709.14	599625.18	0.96
268701.41	599618.36	0.66
268693.78	599611.16	0.8
268685.89	599606.01	0.71
268677.24	599600.14	0.36
268669.91	599592.38	1.1
268662.85	599586.46	0.44
268654.17	599579.67	0.9
268646.70	599574.32	0.95
268638.48	599568.44	0.96
268631.07	599561.80	0.59
268622.81	599554.80	0.94
268616.07	599549.06	1.36
268669.68	599605.75	1.26
268687.24	599619.33	0.69
268695.08	599626.15	1.25
268702.54	599631.31	1.06
268709.62	599637.78	0.28
268718.62	599644.76	0.3
268725.27	599651.05	0.48
268733.96	599658.22	0.78
268740.94	599664.88	0.79
268748.43	599670.78	1.8
268756.64	599676.29	2.1
268751.37	599684.43	2
268744.73	599692.61	1.96
268737.52	599699.69	1.93
268718.17	599708.06	2
268722.96	599701.61	1.94
268729.71	599693.42	1.8
268736.15	599685.62	2.1
268743.21	599677.25	2.2
268734.78	599671.56	2
268728.74	599678.79	1.68
268722.19	599686.41	1.9
268715.88	599695.13	2.07
268709.73	599702.18	1.9
268695.68	599703.71	1.9
268702.25	599696.47	1.94
268708.15	599688.31	1.78

Easting	Northing	Peat Depth (m)
268715.01	599680.31	1.82
268720.73	599672.90	1.7
268726.87	599665.67	0.61
268719.88	599658.64	0.46
268711.31	599651.84	0.27
268704.67	599645.91	0.3
268695.90	599639.68	0.94
268689.14	599633.38	1.2
268681.65	599627.11	0.39
268663.79	599614.65	0.87
268668.64	599624.52	0.5
268673.28	599634.22	0.44
268682.17	599641.20	1
268689.99	599647.46	0.63
268697.68	599653.36	0.58
268704.87	599660.01	1.02
268713.97	599666.42	0.5
268712.70	599659.41	0.9
268707.22	599674.79	0.32
268699.06	599667.61	1.1
268691.88	599661.14	0.74
268683.95	599654.69	0.37
268675.50	599648.63	0.14
268668.63	599641.97	0.41
268701.74	599682.93	0.57
268692.85	599675.96	0.62
268684.59	599668.97	0.17
268676.47	599663.27	0.63
268669.28	599656.61	1.44
268662.59	599663.31	0.45
268671.41	599671.40	0.41
268678.80	599677.67	1
268685.34	599683.61	0.25
268694.54	599690.20	1
268687.41	599696.35	0.74
268679.63	599691.38	0.55
268671.73	599685.68	1.36
268845.61	600196.66	0.9
268850.86	600205.97	0.55
268854.10	600214.97	0.7
268859.05	600246.19	1
268853.81	600237.44	0.34
268849.85	600229.02	1
268845.76	600219.86	0.67
268840.85	600211.28	0.54
268836.13	600202.14	0.42
268832.89	600193.14	0.35
268827.53	600183.84	0.4
268819.30	600188.35	0.6

Easting	Northing	Peat Depth (m)
268823.14	600196.59	0.4
268827.22	600205.56	0.53
268831.52	600214.53	0.63
268836.99	600224.20	0.82
268840.54	600233.00	1.18
268845.35	600241.59	0.94
268855.25	600246.86	0.94
268849.97	600250.91	0.93
268840.01	600254.55	1.26
268836.62	600247.23	1.25
268832.01	600238.27	1
268827.68	600228.19	0.76
268823.09	600219.79	0.83
268818.36	600210.28	0.43
268814.17	600201.31	0.7
268809.45	600191.98	0.78
268804.41	600183.04	0.89
268789.97	600181.80	1.08
268797.15	600188.26	0.87
268800.68	600196.51	0.67
268805.93	600205.45	0.8
268809.80	600214.61	0.56
268814.33	600224.32	0.42
268818.80	600232.35	0.84
268823.43	600242.05	0.98
268827.06	600250.11	0.83
268831.80	600259.99	1.01
268835.96	600268.03	1.24
268827.53	600273.11	0.95
268823.25	600264.33	0.56
268819.26	600254.79	1
268814.47	600246.96	0.94
268809.64	600237.63	0.94
268812.47	600229.75	0.62
268805.66	600228.47	0.71
268800.96	600220.26	0.79
268796.24	600211.12	0.82
268791.49	600201.05	0.63
268788.10	600193.73	0.82
268778.12	600175.28	0.57
268771.42	600181.42	1
268778.98	600196.97	0.5
268783.15	600205.57	0.7
268786.90	600214.18	0.94
268791.01	600224.08	0.95
268796.14	600232.84	0.76
268801.42	600242.70	0.71
268805.46	600250.38	1
268809.00	600259.18	1.05

Easting	Northing	Peat Depth (m)
268814.40	600269.60	1
268818.68	600278.38	1.15
268805.81	600273.01	1.14
268800.68	600264.25	0.9
268796.81	600255.27	0.72
268791.14	600246.16	0.84
268787.62	600238.29	0.88
268782.87	600228.22	0.88
268776.89	600219.49	0.59
268774.49	600209.91	0.95
268769.87	600200.77	0.62
268765.91	600192.16	0.44
268761.05	600181.91	0.88
268757.10	600173.68	0.89
268751.77	600165.48	0.96
268747.08	600157.46	0.88
268742.87	600147.56	1
268737.96	600139.35	0.98
268732.38	600129.87	0.74
268729.96	600119.73	0.75
268725.18	600112.08	0.65
268756.60	600131.93	0.77
268748.37	600136.63	1.05
268764.88	600214.65	0.47
268768.75	600223.63	0.54
268773.46	600232.40	0.94
268778.36	600240.60	0.8
268782.88	600250.12	1.14
268786.75	600258.91	1.13
268791.14	600267.88	0.65
268796.71	600276.99	0.8
268778.31	600263.80	1.02
268773.47	600254.11	1.26
268769.95	600246.23	1
268765.35	600237.65	0.94
268733.65	600086.96	0.85
268725.54	600092.02	0.3
268717.01	600097.47	0.84
268693.07	600054.57	0.26
268700.85	600048.96	1.02
268709.04	600042.96	0.77
268679.79	599999.84	0.67
268672.48	600007.11	1.57
268665.35	600013.26	1.3
268625.18	600016.12	1.04
268618.73	600009.63	1.45
268611.82	600001.67	1.3
268583.50	600047.06	0.68
268593.68	600050.84	0.39

Easting	Northing	Peat Depth (m)
268602.04	600057.46	0.35
268572.64	600098.61	1.58
268582.48	600101.84	1.34
268592.18	600100.07	0.96
268598.24	600147.21	1.5
268587.92	600149.19	0.96
268578.81	600152.80	1.25
268590.57	600202.75	0.9
268600.91	600197.99	1.3
268610.59	600195.47	0.83
268621.43	600243.03	1.36
268613.07	600246.99	1.15
268602.43	600248.98	1.17
268614.55	600296.69	0.4
268624.87	600294.71	0.44
268634.35	600292.76	0.6
268646.68	600340.65	0.7
268637.03	600343.91	0.85
268626.26	600348.68	1.24
268637.30	600392.34	0.93
268647.57	600391.85	0.44
268656.93	600389.53	0.7
268645.54	600444.80	0.65
268653.78	600447.53	0.46
268655.33	600442.84	0.35
268665.72	600442.91	0.49
268668.23	600491.83	1.5
268648.23	600492.79	1
268648.97	600520.98	1.45
268648.57	600532.69	1.8
268658.04	600541.13	1.1
268667.60	600541.96	1.7
268647.45	600552.02	0.5
268648.18	600562.39	0.94
268647.19	600571.89	1
268647.49	600581.90	1.51
268647.58	600591.92	1.76
268656.38	600592.22	1.6
268667.49	600591.89	1.4
268647.46	600602.32	1.66
268647.53	600611.78	1.26
268717.25	600651.66	0.7
268716.60	600661.88	1
268716.61	600672.65	0.94
268717.00	600682.29	1.3
268707.42	600702.24	1.5
268707.65	600692.03	1.05
268707.68	600682.38	1.33
268708.00	600671.79	1.17

Easting	Northing	Peat Depth (m)
268706.88	600662.73	0.94
268706.88	600651.78	0.8
268706.59	600642.14	1.12
268707.87	600631.70	0.94
268697.60	600631.82	1
268697.03	600641.12	0.96
268696.49	600651.53	1
268696.16	600661.75	0.94
268697.08	600671.37	1
268697.35	600680.64	0.77
268697.38	600692.33	1
268697.56	600701.79	1.23
268688.03	600702.08	0.89
268687.23	600693.01	0.7
268687.65	600682.04	0.7
268687.78	600672.39	1.16
268687.77	600661.25	1.47
268687.27	600651.43	1.04
268687.73	600642.14	0.92
268687.63	600631.56	0.81
268687.46	600622.29	1
268673.61	600612.49	1.22
268677.05	600621.11	1.35
268676.92	600631.14	1.67
268677.34	600641.71	1.65
268676.47	600651.57	1.25
268672.88	600666.34	0.76
268676.97	600671.97	0.51
268677.69	600682.15	0.47
268677.01	600701.85	0.54
268666.42	600702.16	1.25
268667.41	600692.48	0.89
268667.83	600681.89	0.88
268667.53	600671.51	0.94
268671.43	600667.31	0.83
268667.63	600660.92	1.65
268666.64	600652.23	1.37
268667.79	600641.25	1.43
268667.73	600632.15	1.75
268667.09	600621.22	1.8
268657.45	600621.14	1.53
268657.02	600631.54	1.55
268657.00	600641.75	1.5
268656.66	600651.78	0.98
268657.30	600662.34	1.3
268656.63	600672.02	0.6
268657.27	600682.76	0.75
268656.56	600691.13	0.5
268657.01	600702.81	0.94

Easting	Northing	Peat Depth (m)
268647.87	600701.60	1.2
268647.90	600692.13	0.83
268646.46	600682.71	0.39
268647.49	600671.17	0.67
268647.55	600662.45	1.35
268647.15	600652.44	1.31
268647.46	600641.48	1.16
268647.60	600632.01	1.38
268648.15	600621.97	1.6
268636.04	600631.61	1.4
268637.64	600642.51	1.33
268637.93	600652.34	1.1
268636.44	600662.78	1
268636.90	600671.30	0.6
268636.57	600681.33	0.58
268637.32	600692.45	0.96
268628.00	600681.77	0.54
268627.05	600671.04	0.4
268627.61	600661.37	0.87
268628.38	600651.88	1
268546.90	601110.87	0.96
268544.81	601101.10	0.5
268541.48	601092.47	0.5
268537.92	601083.11	0.46
268521.65	601066.89	1.52
268524.80	601076.64	1
268527.72	601085.64	0.9
268532.12	601094.79	0.46
268533.91	601105.13	0.7
268538.18	601113.36	0.86
268541.45	601123.47	0.94
268544.73	601133.95	0.96
268535.78	601135.89	0.74
268532.13	601127.09	0.98
268529.31	601117.71	0.74
268524.62	601109.68	0.61
268521.45	601099.38	0.54
268519.55	601088.86	0.67
268515.38	601080.44	1.05
268511.60	601070.90	0.83
268500.18	601064.38	1
268501.84	601073.79	0.94
268505.37	601082.23	1.05
268508.01	601092.36	0.55
268512.12	601102.44	0.48
268515.76	601110.87	0.74
268519.67	601121.15	0.81
268522.26	601129.98	0.88
268525.93	601139.34	0.75

Easting	Northing	Peat Depth (m)
268528.23	601149.10	0.7
268519.40	601151.41	0.82
268517.14	601142.94	0.76
268511.48	601134.38	1.33
268509.50	601124.79	1
268507.09	601114.84	0.57
268503.07	601104.57	0.66
268499.85	601095.94	0.36
268496.59	601086.01	0.56
268494.01	601077.55	0.53
268490.23	601068.20	1.18
268483.38	601062.28	1.33
268480.87	601070.52	0.8
268483.28	601080.10	0.54
268487.16	601089.45	0.37
268489.97	601098.46	0.8
268493.02	601108.58	0.6
268500.54	601112.06	0.4
268497.33	601117.91	0.82
268500.17	601128.22	0.85
268503.16	601136.11	0.93
268507.28	601146.20	1.2
268510.44	601156.31	1.6
268502.15	601159.16	1.18
268497.66	601150.57	1.29
268493.77	601140.66	1.15
268491.16	601131.27	0.95
268488.01	601121.72	1.12
268484.56	601112.54	0.55
268481.29	601102.43	0.44
268477.83	601092.88	0.54
268474.49	601083.89	1
268471.14	601074.52	0.94
268459.50	601078.21	0.83
268465.68	601086.75	0.82
268467.76	601095.97	0.44
268471.95	601105.12	0.32
268474.97	601114.31	0.36
268478.15	601124.98	0.57
268481.37	601133.42	0.9
268484.41	601143.17	0.86
268488.23	601154.00	1.37
268478.22	601155.60	0.58
268475.01	601147.53	0.83
268472.09	601138.34	0.92
268462.60	601139.73	0.5
268459.93	601131.83	0.3
268468.60	601128.05	0.27
268465.70	601119.41	0.32

Easting	Northing	Peat Depth (m)
268455.70	601121.56	0.25
268451.93	601112.40	0.27
268462.43	601109.30	0.45
268458.78	601100.32	0.4
268455.74	601090.75	0.41
268455.62	601068.86	0.77
268452.38	601059.67	1.5
268463.69	601058.97	0.98
268472.38	601055.74	0.82
268449.43	601049.55	1
268445.79	601041.31	1.05
268441.67	601031.04	0.43
268438.78	601022.77	0.82
268436.16	601013.20	0.53
268447.57	601012.12	1.88
268456.27	601009.08	1.46
268432.28	601003.67	1.27
268428.37	600993.39	1.26
268425.45	600984.20	1.6
268421.98	600967.41	1.7
268430.06	600964.57	2
268440.11	600960.56	1.46
268436.28	600917.43	1.64
268426.54	600914.19	2.1
268416.81	600911.14	2.2
268435.55	600864.56	1.48
268445.43	600869.09	1.5
268453.96	600874.22	0.6
268454.72	600846.54	0.5
268457.50	600818.80	0.9
268466.12	600823.93	0.8
268474.41	600828.14	0.21
268495.09	600782.79	0.37
268486.91	600778.40	0.36
268477.14	600773.86	0.31
268496.42	600727.82	1
268505.04	600732.76	0.85
268513.98	600734.16	0.47
268532.11	600688.34	0.88
268523.21	600684.70	0.75
268513.55	600680.54	1.19
268528.64	600635.73	0.65
268538.23	600637.67	0.58
268547.37	600642.04	0.65
268562.18	600591.49	0.76
268552.55	600588.43	1.36
268542.71	600585.02	0.92
268556.43	600536.91	1.75
268564.08	600541.32	1.55

Easting	Northing	Peat Depth (m)
268574.44	600544.35	1.44
268589.04	600497.34	0.64
268579.81	600493.34	0.4
268570.81	600489.71	0.63
268590.81	600442.72	1.8
268599.18	600446.37	0.82
268609.67	600449.95	1
268628.63	600406.89	1
268619.89	600401.77	1.48
268611.95	600394.58	1.73
268595.48	600257.72	1
268587.10	600253.52	1.3
268577.99	600250.26	0.6
268556.39	600289.70	1.5
268562.58	600298.42	1.42
268569.95	600303.95	1.27
268575.07	600308.81	1
268581.63	600315.49	1
268589.05	600322.69	1.4
268544.49	600366.89	2.2
268540.43	600358.66	2.26
268529.49	600340.05	1.6
268526.35	600330.49	1
268520.40	600322.87	1.24
268475.26	600340.55	0.44
268480.30	600349.49	1.77
268482.06	600358.91	0.78
268484.98	600367.91	0.65
268488.85	600377.08	1.26
268491.61	600387.95	2.07
268442.93	600400.16	0.7
268440.35	600392.07	0.5
268437.51	600381.95	0.47
268425.80	600358.72	0.53
268431.14	600349.47	0.64
268434.89	600340.08	0.4
268388.93	600323.07	2.5
268379.64	600327.80	1.23
268351.36	600363.54	0.92
268343.48	600369.34	1.67
268336.58	600375.86	2.2
268387.15	600405.53	1
268388.34	600395.84	1.35
268391.22	600385.74	1.8
268340.45	600281.64	2.86
268334.80	600273.46	2.83
268329.52	600263.22	2.75
268323.39	600256.54	2.63
268323.07	600256.73	2.63

Easting	Northing	Peat Depth (m)
268318.36	600247.96	2
268312.72	600239.97	1.64
268307.27	600231.22	1.58
268301.72	600222.66	1.4
268296.39	600214.47	1.6
268291.05	600206.09	1.52
268253.34	600177.70	0.63
268248.41	600168.76	0.46
268244.38	600161.45	0.7
268239.35	600152.51	0.3
268238.34	600129.52	0.25
268242.77	600139.60	0.22
268247.66	600147.25	0.32
268251.75	600156.22	0.6
268257.62	600164.96	0.55
268262.72	600172.41	0.41
268267.77	600182.10	0.5
268272.36	600190.13	0.63
268285.81	600197.15	1
268281.57	600186.33	1
268276.83	600176.82	0.96
268270.88	600169.02	0.9
268266.05	600159.69	0.92
268261.95	600150.16	0.75
268256.63	600142.34	0.6
268251.62	600134.33	0.7
268246.99	600124.63	0.34
268250.29	600110.98	0.59
268255.65	600120.10	1.6
268260.69	600129.42	1
268265.57	600136.69	0.96
268269.68	600146.41	0.68
268275.23	600155.15	1
268280.35	600163.35	1.17
268285.26	600171.56	1.7
268290.26	600179.57	1.6
268295.20	600188.71	1.7
268302.73	600199.80	1.7
268311.47	600194.35	1.6
268303.45	600184.75	1.52
268299.14	600175.23	1.55
268292.98	600167.61	0.53
268289.19	600157.89	1.82
268284.19	600150.06	1.44
268278.75	600141.50	1.38
268274.58	600133.08	0.7
268269.33	600123.96	1.3
268258.95	600106.27	1.5
268268.66	600101.52	1.44

Easting	Northing	Peat Depth (m)
268272.54	600110.87	1.74
268277.14	600119.46	2.56
268281.61	600127.49	2.54
268288.54	600136.01	2.64
268284.62	600142.99	0.8
268292.61	600144.61	2.39
268297.79	600154.67	1.94
268302.12	600161.59	1.74
268307.08	600171.46	1.45
268312.62	600179.46	1.47
268320.12	600175.16	1.38
268315.29	600166.02	1.63
268311.84	600156.85	1.45
268305.35	600148.87	1.8
268300.95	600140.09	2.4
268296.36	600131.69	2.72
268292.05	600122.17	2.94
268285.75	600113.26	1.12
268281.38	600105.23	1.86
268276.20	600095.17	2.3
268289.28	600100.35	2.4
268294.96	600109.46	3
268299.78	600118.41	2.8
268305.10	600126.24	2.55
268309.60	600135.20	2
268315.04	600143.39	1.72
268320.28	600152.32	1.82
268325.44	600162.01	1.52
268333.85	600156.00	2
268328.08	600147.27	0.92
268324.02	600139.04	1.05
268318.43	600129.18	1.67
268313.11	600121.36	2.41
268308.51	600112.59	2.8
268303.47	600103.64	2.94
268299.27	600094.12	3
268316.84	600107.70	2.55
268322.94	600116.98	1.4
268328.47	600124.98	1.7
268333.07	600133.57	1.35
267362.57	599447.46	0.2
267371.71	599430.66	0.32
267366.12	599417.28	0.3
267380.60	599412.40	0.26
267376.04	599398.24	0.1
267371.50	599384.83	0.27
267380.00	599367.68	0.27
267385.31	599382.37	0.32
267389.39	599394.50	0.2

Easting	Northing	Peat Depth (m)
267393.60	599407.92	0.2
267398.02	599420.97	0.27
267384.26	599424.91	0.25
267388.38	599438.89	0.3
267375.34	599442.06	0.25
267401.65	599435.89	0.2
267415.69	599430.65	0.05
267411.90	599417.21	0.2
267408.11	599404.15	0.27
267403.26	599390.74	0.28
267399.27	599377.87	0.39
267394.88	599365.75	0.2
267408.48	599359.96	0.6
267411.41	599372.68	0.18
267415.94	599385.91	0.5
267421.32	599399.30	0.05
267424.46	599412.19	0.2
267428.58	599425.99	0.3
267432.38	599439.61	0.18
267419.25	599443.53	0.2
267446.28	599436.78	0.1
267443.59	599421.27	0.55
267438.66	599408.80	0.15
267434.66	599395.56	0.22
267430.22	599381.77	0.21
267426.62	599367.59	0.15
267423.78	599354.12	0.28
267440.95	599364.74	0.34
267443.88	599377.83	0.3
267447.01	599390.36	0.2
267450.91	599403.79	0.2
267455.35	599417.58	0.24
267460.87	599431.89	0.16
267464.96	599444.57	0.2
267481.48	599454.84	0.25
267477.66	599440.48	0.15
267473.66	599427.42	0.1
267469.98	599414.36	0.15
267466.49	599400.17	0.1
267462.28	599386.93	0.2
267458.27	599373.50	0.2
267454.17	599360.45	0.15
267475.16	599382.09	0.1
267470.76	599369.60	0.12
267479.72	599396.06	0.15
267483.59	599408.75	0.14
267488.02	599422.17	0.22
267491.19	599435.99	0.1
267495.41	599449.60	0.12

Easting	Northing	Peat Depth (m)
267499.20	599459.32	0.05
267512.57	599459.85	0.1
267509.40	599446.21	0.25
267505.90	599431.66	0
267501.14	599418.06	0.2
267498.34	599405.90	0.2
267494.01	599392.11	0.22
267488.76	599378.82	0.2
267502.04	599373.98	0.18
267506.51	599388.58	0.16
267509.97	599401.47	0.1
267514.41	599415.07	0.15
267518.60	599427.75	0.3
267522.75	599442.47	0.18
267527.47	599454.95	0.15
267541.44	599451.01	0.22
267515.80	599369.55	0.12
267519.94	599384.09	0.14
267524.42	599395.65	0.17
267529.75	599410.90	0.18
267533.48	599423.99	0.26
267535.83	599436.88	0.15
267547.25	599471.62	0.17
267558.84	599462.36	0.17
267554.99	599447.07	0.3
267551.89	599433.71	0.23
267547.35	599418.35	0.2
267543.81	599406.21	0.16
267539.59	599392.78	0
267533.75	599378.11	0.05
267548.10	599376.20	0.2
267551.75	599388.34	0.15
267556.32	599402.37	0.22
267560.44	599416.47	0.3
267564.87	599430.07	0.28
267568.22	599442.97	0.23
267571.31	599457.54	0.1
267566.26	599384.56	0.18
267569.67	599397.82	0.24
267574.40	599411.97	0.22
267578.81	599425.02	0.15
267583.23	599438.06	0.05
267587.35	599451.86	0.27
267600.32	599446.27	0.26
267595.95	599434.53	0.2
267591.91	599420.17	0.12
264837.08	602200.12	0.4
264831.96	602191.92	0.37
264828.14	602181.46	0.4

Easting	Northing	Peat Depth (m)
264824.27	602172.67	0.23
264826.68	602150.88	0.27
264829.73	602160.62	0.21
264833.17	602169.24	0.25
264837.27	602178.77	0.35
264841.27	602188.30	0.39
264845.13	602196.72	0.42
264848.38	602206.08	0.25
264853.12	602215.59	0.22
264862.42	602211.59	0.32
264858.32	602202.25	0.26
264854.46	602193.65	0.35
264850.15	602184.31	0.3
264847.19	602174.01	0.34
264843.14	602166.34	0.34
264839.89	602157.16	0.24
264835.87	602146.89	0.27
264841.11	602134.48	0.26
264844.42	602142.54	0.2
264848.21	602151.89	0.28
264852.45	602162.71	0.23
264856.42	602171.13	0.28
264859.66	602180.12	0.35
264863.13	602189.85	0.64
264866.69	602198.65	0.28
264871.66	602208.90	0.31
264874.65	602216.79	0.48
264883.58	602214.29	0.65
264879.88	602204.00	0.45
264877.38	602195.17	0.61
264873.30	602186.39	0.52
264869.72	602176.66	0.46
264864.98	602167.15	0.47
264861.08	602157.44	0.42
264858.38	602148.80	0.22
264854.70	602139.07	0.22
264851.01	602129.35	0.34
264853.88	602119.24	0.39
264859.51	602126.86	0.45
264863.32	602136.95	0.29
264867.46	602144.25	0.23
264870.85	602154.72	0.15
264874.40	602163.52	0.29
264871.30	602169.56	0.42
264878.78	602171.56	0.39
264882.05	602181.67	0.4
264886.06	602191.57	0.56
264890.04	602200.35	0.78
264894.77	602209.67	0.9

Easting	Northing	Peat Depth (m)
264902.26	602205.36	0.82
264899.36	602196.91	0.59
264895.02	602186.65	0.6
264891.17	602178.42	0.4
264887.93	602169.61	0.34
264883.50	602159.72	0.29
264879.94	602150.55	0.24
264875.83	602140.84	0.26
264873.09	602130.90	0.3
264869.65	602122.47	0.38
264881.81	602128.59	0.35
264885.04	602137.40	0.31
264889.37	602147.48	0.36
264893.58	602157.00	0.36
264896.27	602165.08	0.32
264900.65	602173.49	0.2
264904.47	602184.14	0.78
264908.98	602192.91	0.39
264916.25	602188.23	0.62
264914.73	602180.11	0.3
264909.76	602169.87	0.38
264906.97	602161.97	0.47
264902.53	602151.90	0.55
264899.18	602142.54	0.4
264896.14	602133.35	0.6
264891.82	602123.64	0.5
264908.60	602139.09	1
264911.51	602147.54	0.36
264915.60	602156.70	0.4
264919.53	602167.34	0.54
263410.11	602320.08	0
263401.15	602321.29	0
263390.00	602323.86	0
263382.33	602274.54	0.39
263391.48	602272.40	0.9
263403.27	602270.00	0.26
263395.43	602221.79	0.83
263385.08	602222.86	0.63
263374.23	602224.86	0.8
263367.82	602175.13	0.59
263376.26	602173.94	1.2
263386.79	602171.95	0.54
263380.19	602122.78	1.2
263369.46	602125.15	1.15
263360.05	602125.63	1.1
263350.90	602076.54	0.92
263361.43	602074.36	1.07
263370.00	602074.28	0.56
263361.15	602024.25	1.32

Easting	Northing	Peat Depth (m)
263350.08	602026.08	0.65
263340.68	602026.93	0.67
263329.58	601979.57	0.52
263338.44	601978.37	0.84
263348.14	601976.77	0.8
263335.95	601928.52	1.1
263324.77	601929.98	1.45
263315.61	601931.75	1.35
263302.12	601882.79	0.7
263312.11	601880.25	0.45
263321.41	601879.60	0.77
263307.99	601832.68	1.16
263298.25	601832.80	1
263289.81	601833.80	0.87
263282.09	601782.81	1.28
263292.09	601784.36	0.94
263302.35	601784.04	1
263305.13	601733.28	1.8
263294.47	601734.73	2
263285.74	601733.14	1.36
263288.64	601683.12	0.92
263298.19	601683.76	1.6
263309.14	601685.09	1.5
263312.51	601636.35	1.5
263305.22	601633.43	0.88
263291.95	601632.54	1.92
263311.83	601583.66	2.4
263321.24	601589.87	3.3
263329.39	601593.14	3.45
263365.69	601568.08	2.26
263361.89	601558.17	2.53
263408.18	601565.09	0.3
263409.80	601555.95	0.2
263459.48	601566.11	0.55
263457.04	601576.58	0.26
263506.16	601585.83	0.8
263508.82	601575.91	0.7
263556.99	601585.56	0.58
263554.59	601593.43	0.48
263608.06	601596.23	0.27
263608.36	601585.46	0.41
263654.46	601572.53	0.37
263658.23	601581.50	0.5
263705.66	601560.00	0.32
263701.06	601551.79	0.1
263697.39	601542.62	0.15
263746.06	601530.35	0.12
263792.99	601510.16	0.41
263839.83	601510.95	0.5

Easting	Northing	Peat Depth (m)
263841.14	601501.63	0.6
263840.52	601491.81	0.92
263890.82	601494.90	1
263890.45	601503.63	1.2
263888.58	601515.01	0.62
263937.03	601520.02	0.58
263940.66	601510.44	1.15
263941.29	601500.03	0.72
263990.85	601506.67	0.63
263989.83	601514.68	0.65
263988.99	601525.47	0.43
264039.59	601527.63	1.1
264039.91	601517.41	0.86
264089.04	601527.22	0.47
264090.17	601508.81	0.46
264139.39	601518.25	0.57
264140.74	601507.07	0.54
264191.72	601514.79	0.84
264188.26	601505.61	0.75
264183.17	601498.53	0.84
264231.79	601515.78	1.1
264236.26	601495.78	1
264284.25	601506.38	0.63
264283.04	601515.32	0.4
264280.81	601525.41	0.75
264330.56	601534.84	0.27
264332.70	601525.12	0.3
264334.41	601515.23	0.3
264394.75	601586.69	0.15
264405.24	601583.22	0.1
264413.40	601580.18	0.1
264417.46	601588.22	0.5
264407.75	601592.60	0.38
264398.96	601596.21	0.15
264403.06	601605.55	0.64
264412.36	601601.56	0.66
264421.59	601598.49	0.35
264416.77	601641.70	0.48
264437.86	601686.90	0.29
264458.74	601732.29	0.29
264494.45	601750.12	0.5
264544.96	601746.16	0.46
264545.46	601745.40	0.46
264594.93	601748.90	0.34
264643.14	601760.04	0.4
264689.88	601778.47	0.24
264738.61	601796.10	0.28
264733.03	601804.06	0.55
264728.53	601812.55	0.4

Easting	Northing	Peat Depth (m)
264781.28	601861.24	0.33
264772.48	601864.29	0.34
264761.63	601866.48	0.2
264780.97	601913.59	0.23
264790.20	601910.52	0.1
264799.30	601906.72	0.1
264882.22	602118.00	0.45
264878.03	602108.85	0.33
264875.26	602098.17	0.55
264853.01	602101.26	0.36
264862.87	602098.17	0.33
264871.63	602090.30	0.36
264867.81	602079.46	0.38
264864.38	602071.40	0.54
264860.46	602060.94	0.54
264834.73	602053.93	0.35
264844.56	602050.11	0.27
264853.11	602042.23	0.3
264849.67	602033.43	0.27
264846.07	602023.33	0.22
264835.30	601999.90	0.38
264825.58	602004.10	0.2
264817.31	602007.51	0.44
264799.04	601960.74	1.15
264807.97	601958.24	0.73
264817.28	601954.43	0.89
264775.41	601832.28	0.38
264781.08	601823.75	0.35
264819.65	601858.95	0.48
264811.79	601865.13	0.38
264804.28	601872.23	0.3
264836.94	601911.69	0.27
264843.58	601903.51	0.25
264852.06	601896.94	0.24
264879.90	601941.37	0.58
264870.91	601945.36	1
264861.74	601950.28	1.3
264888.33	601992.16	1.23
264897.92	601987.04	1
264906.83	601984.17	1.2
264933.74	602025.85	1.34
264925.28	602029.82	1.3
264915.36	602034.39	0.96
264942.07	602076.64	1
264953.09	602073.33	0.51
264960.10	602067.18	0.94
263384.84	601498.81	0.9
263404.66	601499.13	0.6
263424.66	601498.51	0.65

Easting	Northing	Peat Depth (m)
263444.86	601497.51	1.4
263465.03	601499.12	2
263494.59	601499.13	0.8
263514.91	601498.69	0.6
263534.60	601498.27	1
263555.17	601499.12	0.46
263575.42	601499.61	0.3
263594.34	601498.28	0.4
263615.23	601498.94	0.38
263634.39	601498.72	0.32
263655.15	601498.63	0.4
263674.10	601498.24	0.33
263664.34	601508.19	0.45
263645.39	601508.40	0.41
263625.48	601508.46	0.5
263605.87	601508.14	0.42
263584.88	601507.67	0.2
263565.29	601507.90	0.45
263545.18	601508.15	0.34
263524.95	601508.22	1.3
263505.15	601508.64	0.62
263484.46	601507.43	0.85
263454.60	601507.61	1
263434.37	601507.68	0.74
263415.86	601508.62	1
263395.41	601508.32	0.43
263385.32	601528.12	0.47
263405.68	601528.79	0.4
263425.04	601528.19	1.4
263444.66	601528.89	1.53
263464.13	601528.29	0.76
263484.80	601528.58	0.55
263503.70	601530.03	0.43
263524.61	601528.28	0.5
263544.43	601528.59	0.5
263564.04	601529.10	0.75
263584.98	601528.08	0.73
263605.21	601528.02	1
263624.40	601528.54	0.4
263645.18	601529.01	0.45
263664.54	601528.41	0.38
263665.15	601548.07	0.38
263645.12	601547.94	0.45
263614.38	601547.22	0.5
263596.08	601547.79	0.44
263574.45	601547.15	0.35
263544.09	601548.28	0.93
263525.00	601547.57	0.44
263504.76	601547.45	0.5

Easting	Northing	Peat Depth (m)
263484.67	601548.44	0.62
263444.52	601548.20	1
263424.81	601548.06	0.6
263411.08	601545.89	0.3
263434.36	601558.90	1.48
263460.22	601555.88	0.47
263474.16	601558.05	0.53
263494.59	601557.60	2.1
263514.34	601559.03	0.51
263534.22	601558.23	0.8
263555.11	601558.89	1
263574.70	601568.86	0.75
263594.52	601569.36	0.5
263625.52	601568.22	0.2
263643.75	601568.77	0.15
263653.10	601562.55	0.27
263607.65	601576.01	0.26
263560.56	601574.12	0.7
266702.85	599767.96	0.1
266671.19	599673.70	0.2
266691.61	599581.40	0.35
266755.75	599547.17	0.25
266756.92	599505.19	0.4
266801.90	599485.83	0.3
266851.36	599474.32	0.75
266854.46	599447.13	1.5
266754.27	599346.95	0.3
266754.24	599247.29	0.25
266854.18	599247.62	0.5
266953.78	599247.41	0.15
267056.06	599247.86	0.15
267155.87	599243.93	0.15
267254.95	599247.27	0.15
267353.59	599246.91	0.7
267554.41	599247.02	0.4
267454.60	599247.41	0.25
267555.10	599347.96	0.1
267454.56	599348.75	0.2
267355.75	599350.59	0.05
267254.33	599346.77	0.2
267055.51	599346.06	0.1
266954.34	599346.87	0.2
266854.12	599347.84	0.75
266898.89	599465.84	0.2
266853.79	599547.93	0.7
266854.98	599647.56	0.15
266854.29	599747.81	0.75
266949.68	599459.86	0.3
266999.88	599458.90	0.2

Easting	Northing	Peat Depth (m)
267050.04	599456.65	0.45
267099.11	599456.85	0.1
267149.56	599457.19	0.8
267199.00	599455.70	0.65
267249.54	599455.67	0.75
267298.89	599454.56	0.45
267349.27	599452.68	0.25
267242.97	599557.76	0.3
267053.92	599546.92	0.4
266953.02	599546.24	0.25
266953.76	599648.12	0.45
267155.18	599648.00	0.6
267255.10	599647.97	0.05
267254.42	599748.77	0.3
267153.30	599747.54	0.05
267054.02	599744.21	0.5
266954.01	599744.81	0.45
266956.29	599855.73	0.3
267054.80	599854.81	0.2
267059.01	599948.96	0.1
267151.24	599954.36	0.1
267261.92	599952.71	1
267249.27	599856.02	0.05
267354.48	599947.89	0.4
267455.74	599946.89	0.35
267554.20	600046.77	0.3
267455.56	600046.75	0.25
267351.25	600048.58	0.3
267254.17	600047.59	0.4
267154.86	600050.02	0.3
267153.31	600146.58	0.55
267255.83	600247.62	0.6
267255.77	600146.84	0.35
267354.10	600147.05	0.15
267455.43	600148.46	1.6
267554.68	600147.90	0.2
268055.41	600645.74	1.1
268155.85	600646.27	0.45
268254.86	600744.47	1.2
268155.12	600746.15	0.65
268053.37	600747.70	0.6
268056.84	600846.33	0.8
267957.77	600845.58	0.65
267854.09	600849.97	0.25
267954.53	600946.08	0.6
267955.41	601046.65	0.45
268255.08	600847.66	0.1
268256.48	600944.50	0.35
268154.92	600949.01	0.95

Easting	Northing	Peat Depth (m)
268055.87	600948.81	0.55
268054.50	601048.14	0.5
268054.87	601145.94	0.7
268154.69	601246.71	0.45
268153.74	601147.45	0.95
268154.88	601047.01	0.85
268256.55	601046.39	0.2
268255.11	601147.40	0.25
268256.99	601245.89	0.05
268254.31	601347.87	0.4
268553.57	601445.68	0.9
268556.04	601346.87	0.4
268452.68	601247.86	0.9
268453.70	601346.20	0.85
268354.35	601246.52	0.35
268354.24	601147.04	0.3
268354.96	601046.61	1.4
268855.49	599247.05	0.2
268854.46	599148.16	0.35
268854.77	599047.74	0.25
268853.96	598948.66	0.3
268754.71	598946.77	0.25
268654.57	598947.15	0.75
268555.02	598945.83	1.05
268454.27	598946.79	1.3
268354.13	598946.98	0.9
268254.33	598947.91	1.35
268155.00	598946.79	0.55
268155.20	598847.11	0.3
268054.94	598843.24	0.6
268054.66	598947.55	0.4
267954.79	598946.26	0.25
267857.40	598946.38	0.15
267854.05	599046.89	0.55
267754.45	599047.45	0.4
267754.05	599147.50	0.25
267654.83	599146.57	0.9
267653.33	599245.17	0.25
267754.99	599246.40	0.95
267755.41	599345.50	0.25
267853.17	599446.88	0.15
267854.02	599347.56	0.8
267954.38	599347.72	0.15
267953.84	599248.25	0.2
267854.85	599247.68	0.15
267854.70	599146.91	0.2
267954.46	599148.20	0.6
268553.90	599047.02	0.35
268653.87	599048.50	0.35

Easting	Northing	Peat Depth (m)
268754.31	599047.56	0.55
268953.87	599749.14	0.45
268953.27	599847.15	0.6
268854.85	599947.51	0.2
268953.55	599945.88	0.95
268953.54	600045.73	0.95
268854.29	600046.44	0.5
268954.52	600146.85	0.8
267922.81	599582.33	1.6
267922.84	599572.68	1.45
267925.53	599563.50	0.75
267875.47	599554.79	0.45
267876.21	599565.35	0.95
267873.55	599575.63	1.7
267854.58	599547.06	1.05
267836.33	599549.83	0.9
267833.53	599559.20	0.9
267832.57	599569.43	0.7
267828.06	599578.11	0.65
267822.15	599586.08	0.8
267789.79	599535.08	0.75
267786.48	599544.83	0.45
267783.26	599554.02	0.25
267738.28	599531.05	0.6
267724.68	599512.15	0.25
267721.30	599498.33	0.2
267714.67	599485.73	0.4
267729.43	599479.72	0.3
267711.72	599471.90	0.15
267727.28	599467.90	0.15
267722.22	599454.69	0.1
267734.38	599450.06	0.05
267729.33	599433.69	0.1
267724.93	599421.20	0.15
267708.86	599411.66	0.1
267712.97	599425.27	0.2
267699.77	599430.31	0.1
267717.30	599439.06	0.2
267704.00	599444.10	0.1
267709.93	599458.21	0.3
267699.56	599476.34	0.1
267702.44	599487.58	0.05
267687.99	599493.58	0.05
267684.96	599480.68	0.25
267694.82	599463.31	0.15
267688.65	599448.09	0.25
267687.43	599435.87	0.55
267694.33	599415.07	0.2
267690.74	599401.07	0.15

Easting	Northing	Peat Depth (m)
267676.82	599406.87	0.15
267682.38	599422.66	0.15
267667.97	599426.43	0.1
267673.16	599440.57	0.15
267677.60	599454.36	0.2
267658.88	599398.68	0.2
267645.77	599403.34	0.3
267628.70	599392.53	0.4
267613.82	599397.99	0.2
267609.88	599386.60	0.25
267597.37	599389.94	0.1
267583.49	599393.70	0.05
267565.49	599383.66	0.55
267570.59	599397.98	0.3
267587.82	599407.30	0.15
267600.86	599404.13	0.25
267619.04	599413.23	0.2
267632.91	599409.29	0.15
267664.51	599413.36	0.35
267649.14	599416.79	0.35
267625.56	599425.66	0.25
267642.46	599434.25	0.4
267655.56	599429.40	0.4
267636.36	599421.62	0.35
267606.47	599417.88	0.3
267609.83	599427.62	0.25
267627.42	599438.22	0.25
267614.72	599442.32	0.05
267632.01	599453.31	0.05
267645.73	599448.07	0.3
267654.78	599446.13	0.4
267659.19	599444.51	0.15
267592.40	599422.20	0.1
267597.14	599432.08	0.2
267600.89	599447.56	0.1
264668.77	602548.45	0.25
264687.14	602543.43	0.15
264692.72	602562.94	0.2
264711.89	602559.56	0.3
264730.89	602554.16	0.2
264746.28	602531.04	0.35
264728.45	602536.79	0.15
264708.00	602539.64	0.3
264663.60	602528.56	0.15
264683.68	602523.68	0.2
264703.28	602520.67	0.15
264722.61	602515.43	0.25
264742.64	602512.59	0.15
264738.04	602490.09	0.1

Easting	Northing	Peat Depth (m)
264718.00	602496.46	0.25
264697.59	602500.79	0.15
264678.87	602504.89	0.15
264660.55	602508.42	0.3
264674.02	602484.81	0.1
264693.46	602483.29	0.35
264714.63	602476.14	0.15
264690.16	602465.57	0.1
264663.58	602465.46	0.25
264667.77	602433.03	0.35
264653.80	602426.41	0.1
264647.93	602407.66	0.2
264644.91	602388.45	0.2
264654.63	602384.07	0.1
264642.99	602335.98	0.35
264631.93	602337.99	0.25
264629.87	602288.12	0.3
264615.37	602239.94	0.1
264598.16	602193.32	0.35
264575.53	602149.47	0.1
264543.02	602111.49	0.45
264498.25	602088.18	0.75
264448.98	602077.07	0.45
264400.50	602088.21	0.35
264358.08	602114.01	0.3
264313.92	602138.38	0.3
264263.85	602138.99	0.3
264226.61	602112.85	0.35
266769.25	600997.78	0.3
266781.10	601095.79	0.1
266768.97	601195.64	0.25
266732.92	601286.00	0.05
266666.46	601358.35	0.45
266592.64	601424.98	0.25
266503.51	601465.35	0.05
266406.08	601500.95	0.05
266311.67	601524.41	0.05
266213.22	601550.59	0.1
266121.33	601590.68	0.05
266052.10	601661.82	0.1
265893.85	602027.80	0.35
265883.32	602078.79	0.6
265873.66	602074.62	0.2
265864.12	602070.83	0.45
265844.65	602116.71	1.75
265856.08	602119.89	0.35
265864.10	602122.61	0.35
265844.81	602170.90	0.4
265835.78	602166.53	0.9

Easting	Northing	Peat Depth (m)
265825.25	602161.47	0.75
265806.25	602208.82	0.1
265817.27	602212.57	0.1
265826.39	602216.37	0.2
265807.32	602261.68	0.2
265797.81	602258.63	0.65
265785.85	602255.47	0.75
265769.27	602302.19	0.35
265778.34	602304.51	0.95
265787.46	602308.50	0.85
265768.23	602355.11	0.1
265759.33	602351.49	1
265749.90	602344.35	0.65
265739.55	602397.56	0.8
265719.50	602441.97	0.55
265682.94	602475.75	0.35
265634.61	602491.88	0.4
265586.30	602497.99	0.2
265538.15	602485.35	0.35
265505.47	602448.48	0.6
265475.25	602408.94	0.25
265436.66	602376.15	0.25
265445.38	602370.31	0.45
265453.66	602363.94	0.35
265408.40	602331.54	0.35
265418.35	602327.71	0.15
265426.19	602324.50	0.2
265391.72	602284.34	1.55
265399.40	602279.28	1.6
265409.31	602274.34	1.55
265375.58	602237.69	0.25
265386.16	602233.84	0.1
265395.08	602227.82	0.45
265379.30	602182.64	0.6
265370.27	602185.33	0.2
265360.53	602188.78	0.1
265339.94	602145.42	0.45
265350.07	602141.03	0.7
265358.91	602135.56	0.8
265311.66	602103.78	0.35
265309.99	602111.44	0.55
265306.92	602121.93	0.5
265261.07	602118.87	0.3
265259.58	602108.15	0.7
265256.58	602099.89	0.85
265212.21	602121.10	0.15
265161.60	602131.92	0.95
265111.97	602143.46	0.55
265063.88	602153.47	0.85

Easting	Northing	Peat Depth (m)
265066.31	602163.79	0.75
265019.56	602138.12	0.95
265017.32	602148.02	0.9
265012.78	602155.40	0.95
264987.64	602109.02	1.6
264978.86	602112.82	1
264969.80	602121.08	0.4
263396.12	601486.77	0.9
263405.31	601489.46	0.6
263417.43	601487.41	1.25
263435.58	601488.71	0.55
263454.96	601488.66	2.1
263475.61	601488.21	1.8
263506.32	601488.01	0.7
263523.81	601488.58	0.95
263546.50	601489.36	0.4
263563.95	601488.27	0.35
263585.00	601487.43	0.3
263604.49	601487.39	0.45
263625.28	601488.42	0.25
263644.64	601487.64	0.95
263663.88	601486.49	0.35
263674.77	601468.52	0.45
263654.72	601467.65	0.4
263633.68	601468.67	0.3
263614.60	601468.52	0.3
263595.41	601467.81	0.15
263573.84	601469.03	0.45
263554.52	601467.77	0.25
263535.70	601468.72	0.9
263514.39	601468.27	0.6
263495.43	601468.11	0.2
263475.63	601468.54	1.05
263454.11	601467.72	1.95
263434.52	601468.14	0.85
263414.62	601468.38	0.75
263395.09	601467.31	1.5
263383.47	601447.63	1.1
263405.83	601447.86	1.55
263426.06	601447.98	1.45
263446.81	601447.53	2.3
263464.66	601449.20	1.55
263486.20	601447.24	0.3
263502.87	601448.39	1.2
263524.80	601448.64	0.25
263545.85	601447.62	0.45
263565.47	601448.50	0.55
263584.57	601449.58	0.4
263605.43	601449.13	0.8

Easting	Northing	Peat Depth (m)
263624.28	601449.10	0.7
263645.37	601449.38	0.35
263674.99	601448.09	0.4
263675.55	601428.59	0.75
263653.93	601428.14	0.8
263634.13	601428.38	0.65
263614.02	601428.82	0.3
263594.82	601427.92	1
263574.42	601429.48	0.85
263554.95	601426.74	0.2
263535.24	601429.76	1.05
263514.01	601428.38	0.35
263495.87	601427.64	1.05
263473.83	601427.20	0.15
263453.94	601428.19	1.1
263433.98	601429.92	1.45
263415.19	601428.64	1.35
263393.81	601429.30	1.55
263394.66	601408.67	1.2
263414.92	601409.53	2.2
268677.00	599161.00	0.22
268667.00	599168.00	0.37
268632.00	599134.00	0.54
268628.00	599144.00	0.31
268587.00	599112.00	0.64
268583.00	599121.00	0.64
268578.00	599129.00	0.5
268546.00	599088.00	0.26
268539.00	599096.00	0.34
268537.00	599104.00	0.48
268500.00	599061.00	0.6
268497.00	599070.00	0.64
268491.00	599080.00	0.84
268458.00	599037.00	0.9
268454.00	599046.00	1.12
268449.00	599054.00	0.8
268416.00	599010.00	0.76
268411.00	599020.00	1.04
268405.00	599030.00	1.22
268368.00	598992.00	0.94
268365.00	599001.00	0.96
268360.00	599010.00	1.06
268321.00	598976.00	0.7
268319.00	598984.00	0.8
268314.00	598992.00	0.8
268272.00	598958.00	0.84
268269.00	598969.00	0.84
268268.00	598977.00	0.84
268217.00	598964.00	0.48

Easting	Northing	Peat Depth (m)
268221.00	598972.00	0.49
268224.00	598984.00	0.84
268171.00	598983.00	0.43
268175.00	598993.00	0.38
268123.00	599002.00	1.17
268128.00	599013.00	0.79
268350.00	599024.00	0.79
268343.00	599030.00	1.28
268333.00	599034.00	0.94
268371.00	599068.00	1.6
268364.00	599074.00	1
268355.00	599079.00	1.52
268392.00	599114.00	0.87
268384.00	599119.00	0.57
268374.00	599124.00	0.59
268404.00	599163.00	1.63
268395.00	599167.00	0.94
268386.00	599169.00	1.08
268391.00	599216.00	1.15
268399.00	599217.00	1.34
268411.00	599218.00	0.94
268413.00	599265.00	0.94
268403.00	599266.00	1.17
268394.00	599269.00	1.09
268394.00	599316.00	0.94
268404.00	599317.00	1.48
268415.00	599319.00	1.51
268415.00	599369.00	1.88
268403.00	599363.00	1.48
268393.00	599365.00	1.09
268412.00	599417.00	1.34
268402.00	599419.00	0.96
268391.00	599416.00	1.04
268391.00	599467.00	1.29
268400.00	599466.00	1.27
268412.00	599466.00	1.58
268463.00	599481.00	0.71
268465.00	599467.00	1
268467.00	599459.00	1.14
268519.00	599476.00	1.24
268511.00	599484.00	1.27
268504.00	599492.00	1.19
268548.00	599517.00	0.8
268556.00	599508.00	0.7
268560.00	599502.00	0.92
268601.00	599532.00	1.18
268593.00	599541.00	1.24
268587.00	599549.00	1.18
268625.00	599580.00	1.24

Easting	Northing	Peat Depth (m)
268633.00	599572.00	1.04
268660.00	599609.00	1.24
268407.00	599516.00	1.82
268399.00	599516.00	2.08
268390.00	599517.00	1.24
268389.00	599568.00	1.58
268400.00	599568.00	1.88
268410.00	599570.00	2.32
268412.00	599619.00	2.82
268399.00	599619.00	2.56
268389.00	599617.00	2.22
268402.00	599704.00	1.24
268401.00	599716.00	1.58
268397.00	599725.00	2.76
268429.00	599754.00	1.9
268437.00	599747.00	1.88
268446.00	599739.00	1.85
268478.00	599778.00	2.22
268472.00	599784.00	2.21
268464.00	599789.00	2.24
268498.00	599825.00	2.24
268513.00	599812.00	1.88
268648.00	599960.00	1.24
268643.00	599967.00	1
268675.21	600006.03	1.44
268666.54	600009.25	1.48
268682.00	599996.00	0.62
268711.00	600039.00	0.8
268705.00	600046.00	0.9
268694.00	600052.00	0.98
268719.00	600095.00	0.74
268728.00	600088.00	0.74
268736.00	600082.00	0.8
268758.00	600127.00	0.63
268751.00	600134.00	0.98
268782.00	600173.00	0.38
268774.00	600179.00	0.94
268854.00	600048.00	0.2
268854.46	599947.21	0.2
268953.00	599928.00	0.4
268951.00	600030.00	0.94
268941.00	600127.00	0.84

Easting	Northing	Peat Depth (m)